

MODIFIED N.R.C. VERSION
OF THE U.S.G.S. SOLUTE TRANSPORT MODEL,
VOLUME 1: MODIFICATIONS

by

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PREFACE

The N.R.C. version of the U.S.G.S. Solute Transport Model (Tracy, 1982) has been modified in this study to incorporate options to (a) solve the ground-water flow equation using the Strongly Implicit Procedure, (b) simulate only the head distributions, (c) simulate a water-table aquifer, (d) input either transmissivity or hydraulic conductivity, and (e) output for use with SAS graphics programs. Stability, accuracy, and efficiency of the modified model are checked by applying the model to a number of test problems and comparing the results with those from the original model. In all cases, the modified model is found to be stable, efficient, and capable of producing reliable results. For most of these problems, the Strongly Implicit Procedure requires only about half the number of iterations than the Alternating-Direction Implicit Procedure to converge to a desired solution. Thus, using the SIP algorithm, it is possible to save a considerable amount of computer time and, therefore, computer cost.

The modifications lend themselves to a preprocessor program described in Volume 2 of this report (Kent, et al, 1986) which is an interactive program to be used in conjunction with this modified N.R.C. version of the U.S.G.S. Solute Transport Model. This preprocessor enables users to input data sets with a minimum degree of effort and confusion and provides maximum flexibility in managing the data.

The final report represents the completion of the contract with the Environmental Protection Agency entitled, "Mathematical Models for Transport and Transformation of Chemical Substances in Subsurface Environments", cooperative agreement number CR811142-01-0. The principal investigators are Dr. Douglas C. Kent and Dr. Jan Wagner. Ms. Lorraine LeMaster is the principal programmer. The cooperation and assistance of

Chi-Chung Chang, for his help in validating the modifications described in this report, and M. M. Hoque, for his work in the application of the SIP algorithm for this project, is gratefully acknowledged. Appreciation is also extended to the project officer, Carl G. Enfield, and to the entire staff of the Robert S. Kerr Environmental Research Center.

The methods described herein can be used to estimate or predict the concentrations in a contaminant plume. The value or accuracy of the prediction can be no better than the estimate of the hydrogeological and chemical parameters that are used in the simulation. Because these parameters can range within wide limits, so also can the prediction. Furthermore, the prediction must conform to fundamental hydrogeologic principles and common sense. The results of these predictive techniques must not be allowed to take precedence over sound field investigation, data collection, and interpretation at the study sites.

The information contained in this manual is believed to be correct at the time of publication. However, the authors assume no liability resulting from the use of the methods described in this publication.

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MODIFIED N.R.C. VERSION
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VOLUME 1: MODIFICATIONS

1.0 INTRODUCTION

The purpose of this report is to describe modifications made to the N.R.C. version (Tracy, 1982) of the U.S.G.S. Solute Transport Model (Konikov and Bredehoeft, 1978).

The program modifications described in this manual are intended as a companion to the manual titled "Modified N.R.C. Version of the U.S.G.S. Solute Transport Model Volume 2: Interactive Preprocessor" (Kent, et al, 1986), prepared for the U.S. Environmental Protection Agency under a contract entitled "Mathematical Models for Subsurface Transport and Fate Predictions."

The project is providing a well documented set of transport and fate models ranging from relatively simple analytical models to complex numerical models. These models will be available on the EPA computer network in a format which would enable users to access the code, enter the required data, run the model, and receive the model results without extensive technical system support.

1.1 Objectives

The broad objective of this project is to develop and/or modify mathematical models in order to provide easier access to models which are capable of predicting the probable concentrations of chemical substances in ground-water systems resulting from the release of these substances onto the ground surface or into the subsurface.

More specifically, the objectives of this project report are to describe the modifications made to the N.R.C. version of the U.S.G.S.

Solute Transport Model. The modifications were made to improve its flexibility and increase its capabilities.

This report contains the following:

- (1) Program Documentation and
- (2) User's Manual

Documentation of the program is developed to include (a) the motivation for and limitations (assumptions) of the program modifications, (b) a description of the numerical methods used in the modifications, (c) listings of the source code or modifications, (d) one or more sets of test data, and (e) guidelines for further modifications which might be required to enable the use of the model on a variety of computer systems. A master copy of all source codes are prepared on magnetic tape in a format which is system independent. This type of program documentation has been written for those who have some background in mathematics and/or computer systems and languages. These documents are intended to serve as reference manuals for individuals who may be responsible for maintaining, modifying, or transferring computer codes; as well as users who are also interested in the details of the computer codes.

The User's Manual includes (a) practical implications of assumptions and restrictions which are incorporated in the mathematical model, (b) the type of computer resources which may be required (for example computer memory, execution time, and input and output devices), (c) input data requirements and formats, and (d) detailed, step-by-step examples of practical problems. The user's manual is written in layman terms for those who may not have a background or experience in numerical methods or computer programming.

The modifications described in this report were developed and tested on an IBM 3081D computer. The modified model has also been tested on an IBM-PC microcomputer. With 20x20 matrices, 512K random access memory is necessary to execute the modified model. The modified model is a batch program, as are previous versions.

A "user-friendly" preprocessor has also been developed to simplify the creation of the data set necessary to run the modified version of the N.R.C. version of the U.S.G.S. Solute Transport Model. The preprocessor is interactive; that is, data is actively requested by the computer and entered by the modeler, while the preprocessor is running. The preprocessor is described in the companion volume entitled "Modified N.R.C. Version of the U.S.G.S. Solute Transport Model Volume 2: Interactive Preprocessor" (Kent, et al, 1986).

1.2 History

The ground-water flow equation is coupled with the solute-transport equation in the U.S.G.S. Solute Transport Model. The computer program uses an Alternating-Direction Implicit Procedure (ADIP) to solve a system of algebraic equations generated from a finite-difference approximation to the ground-water flow equation. The method of characteristics is used to solve the solute-transport equation. The method of characteristics uses a particle tracking procedure to represent convective transport and a two-step explicit procedure to solve a finite-difference equation that describes the effects of hydrodynamic dispersion, fluid sources and sinks and divergence of velocity.

Radioactive decay and equilibrium adsorption are incorporated for the U.S. Nuclear Regulatory Commission (Tracy, 1982). Procedures for radioactive decay, linear isotherm, Langmuir isotherm, and the Freundlich

isotherm are added to the Solute Transport Model developed by Konikov and Bredehoeft (1978). The N.R.C. version of the Solute Transport Model is used in this project.

It is assumed that users will have some background in hydrogeology, soil science, or a similar field; and will have a basic understanding of the physical, chemical, and/or biological processes involved in a specific problem to be addressed. With this background, the report (Volumes 1 and 2) is intended to introduce the user to the model or model adaptation and areas of application and to provide tutorials on data requirements, model access and execution, and the management and interpretation of model output.

1.3 Applications

The modifications will enable various groups within federal and state regulatory agencies, as well as the private sector, to apply a more flexible version of the N.R.C. version of this model to the analysis of study sites such as those involving landfill or groundwater pollution related to conservative and non conservative elements (eg. brine pollution and hazardous elements). This model can also evaluate the effects of pumping and injection wells, recharge, constant head, nonhomogeneities in the aquifer, dispersive coefficients, and no flow boundaries in the vicinity of the site.

1.4 Modifications

The U.S.G.S. Solute Transport Model was selected since it is well-documented and maintained. The modifications by Tracy (1982) which include adsorption and first-order reactions were incorporated. Additional modifications were made to the N.R.C. version of the U.S.G.S. Solute

Transport Model; the modifications include options for selecting (1) only the potentiometric head calculations or the potentiometric head and solute transport calculations, (2) water-table or confined-aquifer conditions, (3) adjustment of transmissivities after each time step to accommodate unconfined flow, (4) calculation of the initial saturated thickness from the bottom elevation and potentiometric head in an unconfined system, (5) incorporation of the SIP iterative technique which is an option for solving the fluid-flow equations, and (6) modification of model output for use with SAS graphics programs. Previous versions use the ADIP technique to solve the fluid-flow equations. Detailed descriptions of the modifications listed above can be found in the following chapter.

2.0 TECHNICAL INFORMATION

2.1 Introduction

The computer program of the N.R.C. version of the U.S.G.S. Solute Transport Model has been modified to incorporate the Strongly Implicit Procedure (SIP), introduce an option to run only the flow model, simulate either a confined or an unconfined aquifer, update the transmissivity for an unconfined aquifer, provide an option for the input of either transmissivity or hydraulic conductivity, provide an option for the input of either saturated thickness or bottom elevation in an unconfined system, and restructure the mass balance output for the flow model. The significance of these modifications will be discussed in the following sections. The implementations of the modifications are discussed in Section 2.3. Variables used for the modifications are defined in Appendix III. Additional information regarding previous implementations and modifications to the model may be found in documents by Konikow and Bredehoeft (1978) and Tracy (1982).

2.1.1 Strongly Implicit Procedure (SIP)

The N.R.C. version of the U.S.G.S. Solute Transport Model solves the ground-water flow equation, using the Alternating-Direction Implicit Procedure (ADIP) developed by Peaceman and Rachford (1955), to obtain head distributions. The seepage velocities are determined from the head distributions. These seepage velocities are used in solving the advective dispersive mass transport equation with adsorption and decay by the method of characteristics (MOC).

Some techniques have proven to be more capable and faster than ADIP in solving the flow equation for aquifers with irregular boundaries,

nonhomogeneous properties, and water table-aquifers. One of these techniques, the Strongly Implicit Procedure (SIP), was developed by Stone (1968) and used by Trescott, et al (1976). The present report documents the development and implementation of the SIP algorithm as an alternative to the ADIP algorithm for solving the flow equation in the N.R.C. version of the U.S.G.S. Solute Transport Model. This algorithm is mathematically more complex and relatively difficult to program, but it facilitates the simulation of problems which cannot be efficiently solved by the ADIP algorithm. For details of the development of the SIP algorithm refer to Remson, et al (1971), Stone (1968), and Trescott, et al (1976).

A sensitivity analysis regarding the performance of the SIP and ADIP flow equations is discussed in Section 3.0.

2.1.2 Transmissivity

Transmissivity is a function of the saturated thickness and hydraulic conductivity of an aquifer. In an unconfined aquifer the saturated thickness changes along with the water table. These changes are caused by stresses such as pumpage, recharge, etc. It is necessary, therefore, to update the transmissivity with time. A modification has been made in the main program to perform this updating at the end of every time step of simulation. In the input section, a provision has been included to allow the input of either transmissivity or hydraulic conductivity data, according to necessity.

It should be noted that the hydraulic conductivity is considered uniform with regard to depth for this application. When dealing with a non-uniform situation, the model may be applied to a representative cross section of the study site. Examples of cross sectional applications may be found in the Master's Thesis by Chang (1985).

2.1.3 Hydraulic Head Simulation

It has been mentioned that the N.R.C. version of the U.S.G.S. Solute Transport Model has a flow portion and solute transport portion. Using the results of head distributions from the flow portion, the solute transport portion predicts the concentration distributions of contaminants. Sometimes, it may be desirable to apply the model to predict only the head distributions in an aquifer where there is no contamination problem or during early stages of calibration. In these situations, it is useful to use only the flow portion of the model to save the computer time and cost of running the solute transport part of the model.

2.1.4 Mass Balance (Hydraulic)

The format used in the mass balance for the flow portion of the model did not distinguish between recharge and injection. In the present modification, recharge and injection are printed separately in the output. Evapotranspiration has been dropped from the titles in the mass balance because there is no provision for estimating transient evapotranspiration from aquifers in the model. Leakage has been modified so that the direction of flow is indicated uniformly throughout the mass balance (negative for inflow, positive for outflow). These modifications clarify the components of the mass balance output.

2.1.5 Saturated Thickness

Saturated thickness is a function of the bottom elevation and potentiometric head in an unconfined aquifer. To aid the user in preparing data, a provision has been made to allow the input of either the bottom elevation or the saturated thickness for an unconfined aquifer. The

initial input section has been modified to calculate the saturated thickness if the bottom elevation is input.

2.2 Solute Transport Flow of Control

The flow of operations in the modified N.R.C. version of the U.S.G.S. Solute Transport Model has been modified in the present study to provide options such as (a) head only simulation, (b) unconfined aquifer simulation, and (c) incorporation of the SIP algorithm to solve the flow equation. These additions are shown in the flow chart (Figures 1 and 2). Modifications made for this report are indicated by shaded boxes in Figures 1 and 2.

2.3 Specific Program Modifications

The FORTRAN source code for the modified N.R.C. version of the U.S.G.S. Solute Transport Model is reproduced in Appendix I. For reference purposes, columns 73-80 of each line contain a sequentially numbered label within each subroutine. Modifications to each subroutine are itemized by these label numbers in Appendix II and are described in the following sections.

2.3.1 Named Common Blocks

The following changes to the common blocks have been made in all the subroutines and in the main program. The integer variables FCON, IHEAD, and ISOLV have been added to the common block PRMI. The functions of these variables are described in Appendix IV. The two-dimensional array THICK has been added to the common block HEDA. This array is used to update the aquifer thickness after each time step when simulating unconfined conditions. The new thickness is then used to update the transmissivities and the related harmonic means. Another two-dimensional array HJ was added

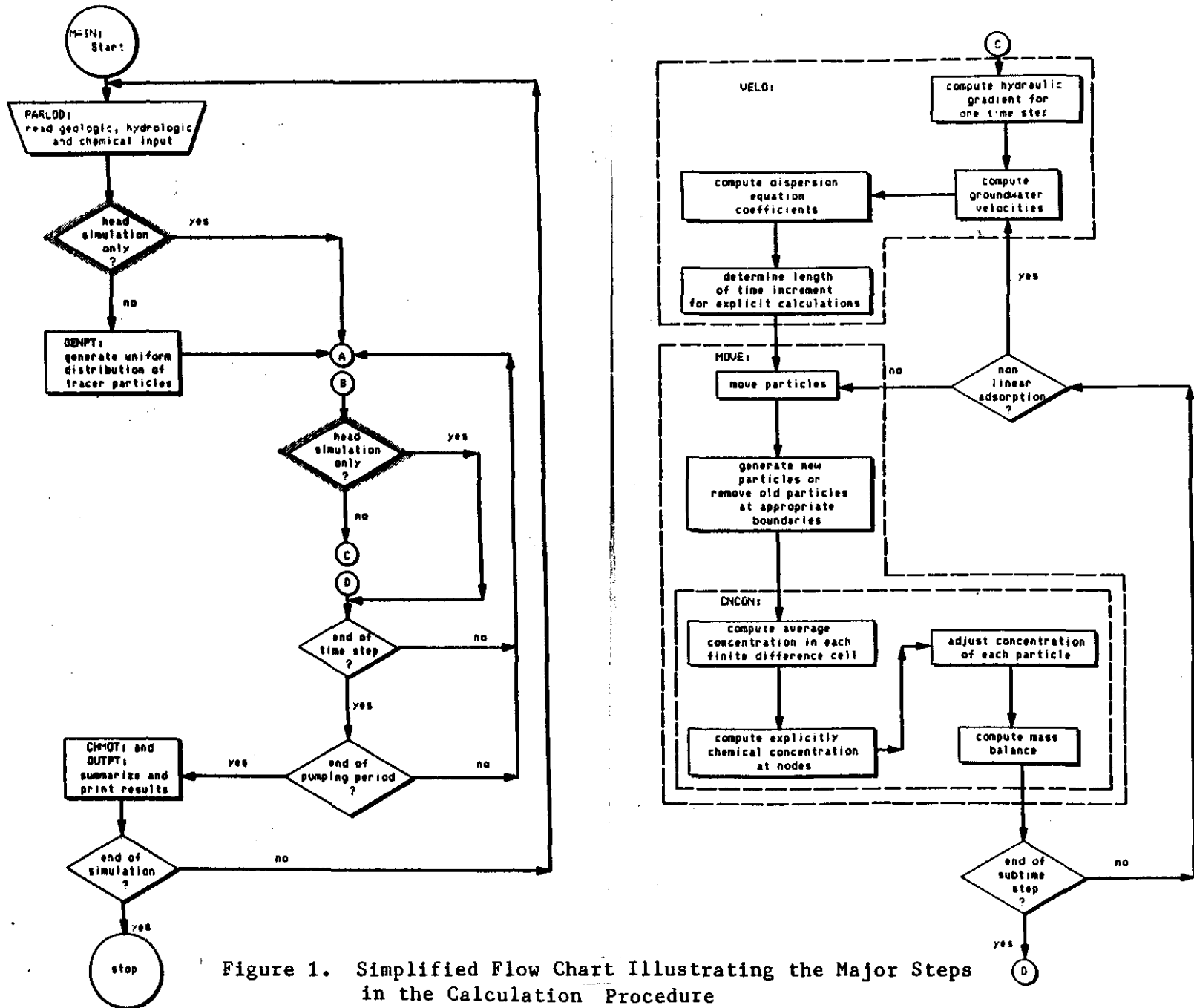


Figure 1. Simplified Flow Chart Illustrating the Major Steps in the Calculation Procedure

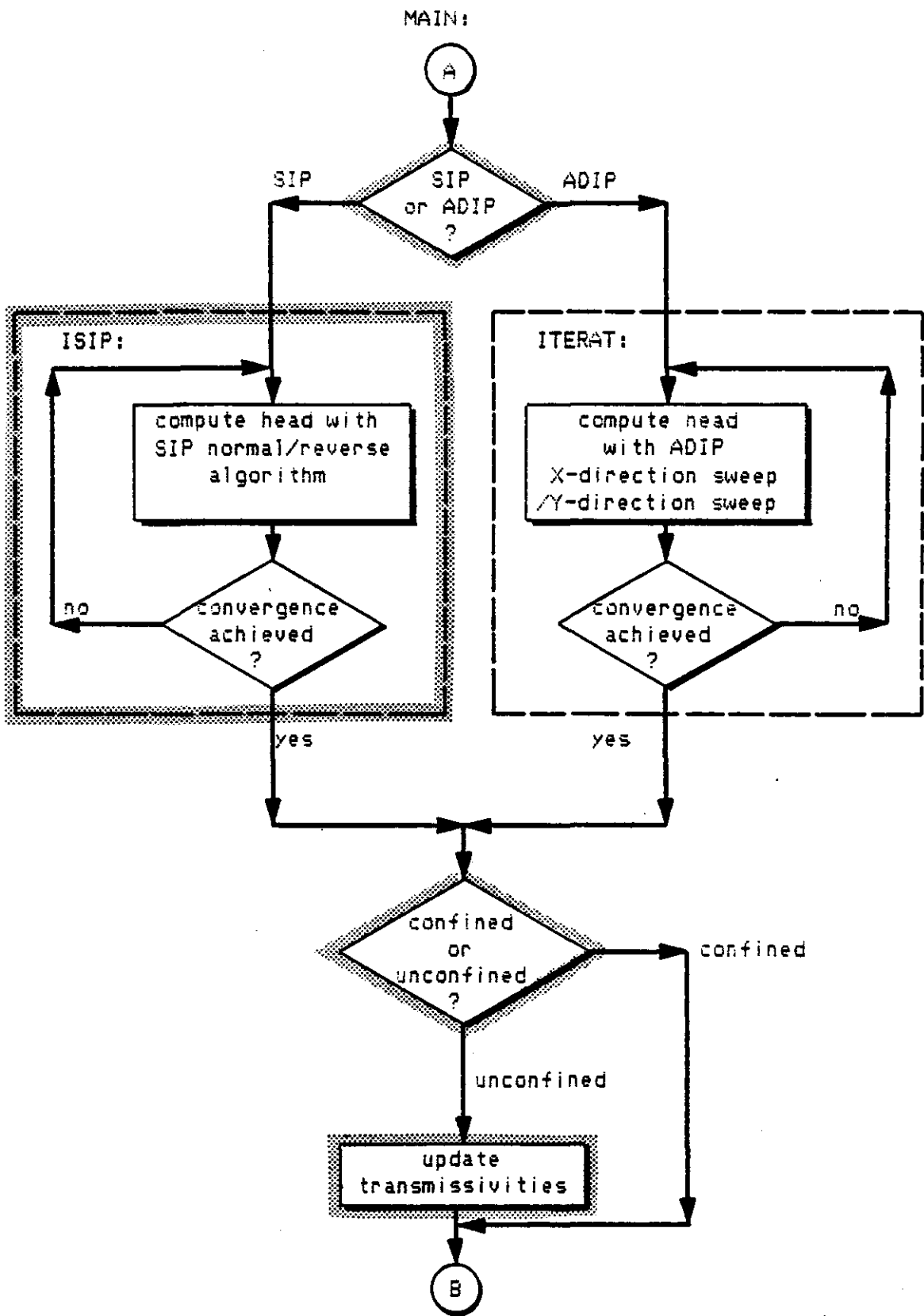


Figure 2. Simplified Flow Chart Illustrating the Major Steps in the Calculation of the Head Distributions

to the common block HEDB. HJ is used as a temporary array for storing the predicted head distributions of the aquifer in the subroutine ISIP. HJ is a double precision variable and is declared as such in a REAL*8 declaration of each affected subroutine. In the common block BALM one real variable, TPQR, is added. This variable represents the total amount of recharge to the aquifer from distributed sources (injection excluded) during the simulation period. The modified lines are listed in Appendix II-A.

2.3.2 Strongly Implicit Procedure (SIP)

To implement the SIP algorithm in the N.R.C. version of the U.S.G.S. Solute Transport Model, a new subroutine, ISIP, has been added to the program. To incorporate ISIP into the program, some modifications were made to other subroutines. The flag used to incorporate this option is ISOLV. The routines affected are the Main program and the subroutine PARLOD. The changes to these routines are listed in Appendix II-B.

The acceleration parameter is set to unity in the implementation as recommended by Stone (1968). It is indicated in the article that the use of iteration parameters between 0.0 and 1.0 (as in this implementation) caused a relatively dense cluster of decay factors near unity. Therefore, no adjustment (acceleration parameter other than unity) is necessary. This may be altered, if desired, in the subroutines PARLOD (for input) and ISIP.

2.3.3 Transmissivity

To update the transmissivity for simulating an unconfined aquifer and to provide an option to input either transmissivity or hydraulic conductivity, the variables FCON and THICK are added as described in Section 2.3.1. The flag TP is added to PARLOD to determine which matrix is input. THICK is used for temporary storage of aquifer thickness during

transmissivity updating in an unconfined aquifer. The routines that have been modified are the Main program and subroutines PARLOD and OUTPT. The lines modified are described in Appendix II-C.

2.3.4 Hydraulic Head Simulation

To include an option to simulate only the head distributions in an aquifer system, flag IHEAD is added to the common block PRMI. The modifications that have been made to the routines MAIN and PARLOD to simulate the head only distributions are listed in Appendix II-D.

2.3.5 Mass Balance

To add the mass balance modifications to the program, variable TPQR which represents the recharge to the aquifer, is included in the common block BALM. All modifications required to the subroutines PARLOD, ITERAT, and OUTPT are listed in Appendix II-E.

The mass balance calculations, performed in OUTPT, are as follows. Injection and pumping are totaled in lines H562-H568. Diffuse recharge and discharge are calculated in lines H572-H578. The leakage rates are calculated in lines H582-H640 and H745. The cumulative and rate net pumping are summed in lines H730 and H740. The mass balance residual and error are calculated between lines H757 and H805 as follows. The sources are the water released from storage minus the recharge, injection, and leakage into the aquifer. The sinks are the sum of the pumping and leakage out of the aquifer. The mass balance residual is the difference of the sources and sinks. The error is the residual times 100 and divided by one half of the total sum of the water through the system (sum of the sources and sinks).

2.3.6 Saturated Thickness

The option of entering either saturated thickness or bottom elevation for an unconfined aquifer is provided by adding the integer flag BTM to PARLOD. PARLOD is the only routine that has been modified. The changes are listed in Appendix II-F.

2.3.7 Additional Modifications

To facilitate the future use of model results with a graphics program, the changes noted in Appendix II-G were made to subroutines PARLOD, OUTPT, and CHMOT. The routine, GRPH, was added to write data to a data set that can be used with languages designed for graphical analysis such as SAS (1982). A description of procedures and graphic products are described in a companion volume entitled "Modified N.R.C. Version of the U.S.G.S. Solute Transport Model Volume 2: Interactive Preprocessor" (Kent, et al, 1986).

3.0 MODEL PERFORMANCE

3.1 Comparison of SIP and ADIP Iterative Techniques

To demonstrate and compare the performance of the modified model (SIP option) with the original model (ADIP option) several test problems were run. Two of the problems are taken from the original manual for the U.S.G.S. Solute Transport Model (Konikow and Bredehoeft, 1978), the third is taken from the manual for the N.R.C. version of the model (Tracy, 1982). A fourth test problem was run to demonstrate the applications of the model with both SIP and ADIP options to an unconfined aquifer system. The results for this problem are reported in the "Modified N.R.C. Version of the U.S.G.S. Solute Transport Model Volume 2: Interactive Preprocessor" (Kent, et al, 1986). An error criteria (TOL) of 0.01 was used in both SIP and ADIP runs for all test problems. Other values can be used to reflect the accuracy of the field data. Larger values for TOL (eg. 0.1) can be used to reduce the number of iterations which results in lower computer costs. All simulations were performed on an IBM 3081D computer.

3.1.1 Test Problem 1

This is the second problem from the manual for the original version of the U.S.G.S. Solute Transport Model (Konikow and Bredehoeft, 1978). This problem was designed to demonstrate the performance of the model on an aquifer where the flow field is strongly influenced by wells. The problem consists of one injection well and one pumping well. The effects of these wells are superimposed on a regional flow field which is controlled by two constant head boundaries. The injection well is a source of constant concentration of 100 parts per million. The initial concentration in the flow field is zero. This is a confined, homogeneous aquifer with a uniform

thickness of 20 feet and hydraulic conductivity of 0.005 ft/sec. The potentiometric surface varies uniformly from 80 to 100 feet. This example was run for both steady state and transient flow simulations to demonstrate the performances of the SIP and ADIP options. A single time step was used in the steady state simulation for a pumping period of 2.5 years and in the case of the transient flow simulation, 10 equal time steps for this pumping period were used. To control the constant head boundaries, the NODEID matrix is used. For this problem the NODEID (ICODE) is designated as 2. Figure 3 shows the NODEID matrix. The CPU time required for each case, and the mass balance error resulting from each, are presented in Table 1 for steady state simulation and in Table 2 for transient simulation.

Table 1 indicates that the SIP algorithm requires fewer iterations, less CPU time, and is more accurate than the ADIP algorithm for steady state simulation of the site. Similar results are indicated in Table 2 for the transient flow simulation.

3.1.2 Test Problem 2

This is the third test problem from the manual for the original version of the U.S.G.S. Solute Transport Model (Konikov and Bredehoeft, 1978). This problem was selected to demonstrate the application of the model with the SIP and ADIP options in a flow field where a patch source of contamination exists and where the flow field is moderately influenced by wells. The problem consists of one withdrawal well located in a regional flow field (confined and homogeneous) that is controlled by two constant head boundaries. The constant contaminant sources are three central nodes (see Figure 4) along the upgradient constant head boundaries. All the parameters for this flow field are the same as Test Problem 1 (section 3.1.1) except the potentiometric head. The potentiometric head uniformly

0	0	0	0	0	0	0	0	0
0	2	2	2	2	2	2	2	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	2	2	2	2	2	2	2	0
0	0	0	0	0	0	0	0	0

Figure 3. - Nodeid Matrix For Test Problem 1

NODEID CODES

ICODE# 1
 ICODE 2
 FCTR1 1.0
 FCTR2 0
 FCTR3 0
 OVERRD 0

Table 1. - Computational Efficiency For Steady-State Problems

Test Problem	Iterations and CPU Time				Mass Balance Error (%)			
	SIP		ADIP		SIP		ADIP	
	No. of Iterations	Total CPU Time (sec)	No. of Iterations	Total CPU Time (sec)	Hydraulic Mass balance error	Chemical Mass balance error	Hydraulic Mass balance error	Chemical Mass balance error
1	7	1.45	13	1.48	1.53883E-02	-7.95201E+00	1.31100E-01	-6.86250E+00
2	6	1.43	13	1.48	8.80971E-03	-3.06842E+00	1.18518E-01	-3.05039E+00
3	2	4.03	1	3.95	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00

Table 2. - Computational Efficiency For TransientTest Problem 1

Time Step	Iterations and CPU Time				Mass Balance Error (%)			
	SIP		ADIP		SIP		ADIP	
	No. of Iterations	Total CPU Time (sec)	No. of Iterations	Total CPU Time (sec)	Hydraulic Mass balance error	Chemical Mass balance error	Hydraulic Mass balance error	Chemical Mass balance error
1	7	1.90	13	2.02	2.16500E-02	-2.26953E+1	1.57759E-01	-2.26953E+01
2	3		6		3.22388E-02	-2.44461E+01	1.267004E-01	-2.44459E+01
3	2		3		2.50258E-02	-7.74837E+0	7.17186E-02	-1.92833E+01
4	1		3		1.96135E-02	-1.13217E+01	5.67972E-02	-1.31429E+01
5	1		2		1.53982E-02	-5.06631E+00	4.74312E-02	-6.48212E+00
6	1		1		1.26792E-02	-2.30856E+00	4.08725E-02	-4.43758E+00
7	1		1		1.07680E-02	-3.97417E+00	3.32994E-02	-5.89064E+00
8	1		1		9.35754E-03	-3.36166E+00	3.00519E-02	-6.00104E+00
9	1		1		8.27377E-03	-3.11102E+00	2.56867E-02	-5.72208E+00
10	1		1		7.42532E-03	-2.52546E+00	2.37322E-02	-4.11345E+00

0	0	0	0	0	0	0	0	0
0	2	2	1	1	1	2	2	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	2	2	2	2	2	2	2	0
0	0	0	0	0	0	0	0	0

Figure 4. - Nodeid Matrix For Test Problem 2.

ICODE#	NODEID CODES	
	1	2
ICODE	2	1
FCTR1	1.0	1.0
FCTR2	0	100
FCTR3	0	0
OVERRD	0	0

varies from 75 to 100 feet. In this example, to control the constant head boundaries, 2 ICODEs are used for the NODEID matrix. ICODE 2 is used to represent the constant head boundaries except the three central nodes along the upgradient where the contaminant source patch exists. These three nodes are controlled with ICODE 1 (see Figure 4).

The results from the steady state simulation of this problem were reported in the U.S.G.S. Solute Transport manual (Konikow and Bredehoeft, 1978). In the present study this problem was run for both steady state and transient flow simulations using the same pumping period setup as Test Problem 1 (section 3.1.1). The CPU time required for and the mass balance error resulting from each option (SIP and ADIP) for both steady state and transient flow simulations are presented in Tables 1 and 3, respectively. Input data and the selected output for this test problem are presented in Appendix VII.

Table 1 indicates that the SIP algorithm requires fewer iterations, less CPU time, and is more accurate than the ADIP algorithm for steady state simulation of the site. Similar results are indicated in Table 3 for the transient flow simulation.

3.1.3 Test Problem 3

This problem is presented in the manual for the N.R.C. version of the U.S.G.S. Solute Transport Model (Tracy, 1982). In the present study this problem was selected to demonstrate the performance of the SIP and ADIP options in a solute transport problem where radioactive decay and sorption phenomena exist. This is considered a one-dimensional simulation. The flow field is influenced by one injection well and one withdrawal well and controlled by two constant head boundaries. The injection well is the

Table 3_r - Computational Efficiency For Transient

Test Problem 2

Time Step	Iterations and CPU Time				Mass Balance Error (%)			
	SIP		ADIP		SIP		ADIP	
	No. of Iterations	Total CPU Time (sec)	No. of Iterations	Total CPU Time (sec)	Hydraulic Mass balance error	Chemical Mass balance error	Hydraulic Mass balance error	Chemical Mass balance error
1	6	1.90	13	2.01	8.58178E-03	-1.13870E+01	1.33714E-01	-1.13756E+01
2	3		6		2.59461E-02	6.32174E+00	1.10818E-01	6.3452E+00
3	2		3		2.03862E-02	-7.09691E-01	6.32410E-01	-6.97257E-01
4	1		3		1.61486E-02	-3.16578E+00	5.03580E-02	-3.15459E+00
5	1		2		1.27278E-02	1.74106E+00	4.21897E-02	-1.75011E+00
6	1		1		1.04736E-02	-2.05990E+00	3.64501E-02	-2.06982E+00
7	1		1		8.89435E-03	-8.19606E+00	2.97079E-02	-8.24349E+00
8	1		1		7.71704E-03	-1.11926E+00	2.68048E-02	-1.12535E+00
9	1		1		6.81105E-03	-1.47943E+00	2.39371E-02	-1.48265E+00
10	1		1		6.12330E-03	-1.56466E+00	2.12051E-02	-1.56501E+00

contaminant source in this flow field and has a concentration of 500 parts per million. In the NODEID matrix, the constant head boundaries are controlled by ICODE 2 (see Figure 5). This flow field is also considered to be a confined, homogeneous aquifer. Simulations were made for both steady state and transient flow. The CPU time required to run these test problems and the resulting mass balance error are presented in Table 1 for steady state and in Table 4 for transient flow simulations. Input data and the selected output for time steps 1 and 10 are presented in Appendix VIII.

Table 1 indicates that the ADIP algorithm requires less time and fewer iterations than the SIP algorithm for this one-dimensional, steady state simulation. Results of the transient flow simulation, in Table 4, also indicate the ADIP algorithm is slightly more efficient than the SIP algorithm. There are no significant differences in the accuracy of the algorithms for either transient flow or steady state simulations.

3.1.4 Conclusions: SIP vs. ADIP

For Test Problems 1 and 2, which are relatively complex in nature, the SIP algorithm requires (for steady state simulation) only about half of the number of iterations as the ADIP algorithm to converge to the desired solution. For a less complex problem, such as Test Problem 3 (one-dimensional), the SIP algorithm provides a rate of convergence similar to that of the ADIP algorithm. In the case of transient flow simulation, the SIP algorithm provides a significantly faster convergence rate (fewer iterations) than the ADIP algorithm for the first few time steps of Test Problems 1 and 2. However, as the simulation proceeds, the number of iterations required by each algorithm, and the difference between the number of iterations for each algorithm, becomes insignificant. The results are shown in Tables 1, 2, 3, and 4. These results indicate that

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Figure 5. - Nodeid Matrix For Test Problem 3

NODEID CODES

ICODE#	1
ICODE	2
FCTR1	0.3
FCTR2	0
FCTR3	0
OVERRD	0

Table 4. - Computational Efficiency For Transient

Test Problem 3

Time Step	Iterations and CPU Time				Mass Balance Error (%)			
	SIP		ADIP		SIP		ADIP	
	No. of Iterations	Total CPU Time (sec)	No. of Iterations	Total CPU Time (sec)	Hydraulic Mass balance error	Chemical Mass balance error	Hydraulic Mass balance error	Chemical Mass balance error
1	2	4.095	1	4.025	0.00000E+00	3.78286E+00	0.00000E+00	3.78286E+00
2	1		1		0.00000E+00	-1.53608E+01	0.00000E+00	-1.53608E+01
3	1		1		0.00000E+00	-6.28198E+00	0.00000E+00	-5.58985E+00
4	1		1		0.00000E+00	-6.28198E+00	0.00000E+00	-6.28198E+00
5	1		1		0.00000E+00	-1.03799E+00	0.00000E+00	-6.28198E+00
6	1		1		-9.55977E-06	-7.16792E+00	-9.55977E-06	-7.16792E+00
7	1		1		-7.16972E-06	-2.42799E+00	-7.16972E-06	-7.16792E+00
8	1		1		0.00000E+00	-6.90429E+00	0.00000E+00	-6.90429E+00
9	1		1		0.00000E+00	-2.82789E+00	0.00000E+00	-6.90429E+00
10	1		1		0.00000E+00	-2.03537E+00	0.00000E+00	-2.03537E+00

SIP is, overall, a more powerful iterative algorithm than ADIP. Because SIP generally requires fewer iterations for a given simulation than ADIP, computer time and cost should be less when the SIP technique is used.

3.2 Sensitivity to Grid Orientation

A word should be said with regard to the relationship of the SIP and ADIP iterative techniques to the physical setup of the data for a simulation. This setup is in regard to the gradient and the X-Y grid system. The two setups are with the flow along the columns (X axis) and the flow along the rows (Y axis). For an isotropic, homogeneous site with uniform gradient, no significant differences (differences of less than or equal to 1%) were found between the results of either iterative technique or flow setup. With an anisotropic site, however, significant differences, related to the direction of flow, were found. The anisotropic characteristics were accurately represented in the results when the flow was along the columns. However, when the flow was simulated along the rows, the anisotropy was apparently ignored. Those results matched the isotropic simulations. No apparent explanation was found for this in the program code and further analysis is beyond the scope of this study.

3.3 Model Sensitivity to Particle Movement

The previous sections discussed the performance of the Solute Transport Model in relation to different iterative techniques used to determine potentiometric head. This section presents the results of a sensitivity analysis of the parameters affecting particle movement.

The maximum cell distance per particle move (CELDIS) and the initial number of particles per node (NPTPND) are the two execution parameters that must be specified by the users to simulate the transport of solute in an

aquifer system with the modified N.R.C. version of the U.S.G.S. Solute Transport Model. These two parameters influence the accuracy, precision, and efficiency (computational time and cost) of the solution to a particular problem.

Konikov and Bredehoeft (1978) performed sensitivity analyses on a Honeywell 60/68 computer using the ADIP algorithm to solve the flow equation. For this study, the SIP algorithm is used to solve the flow equation for all the test problems and the program is executed on an IBM 3081D computer. The results of this analysis may be useful to users in the developmental stages of simulations especially in relation to CELDIS and NPTPND.

Before discussing the sensitivity of particle movement, it is important to discuss briefly how the stability criteria controls the size and number of subtime steps (automatically generated in the program and used in the solute transport equation) and how the subtime steps may vary according to the value of CELDIS.

3.3.1 Relation of Stability Criteria with Particle Movement

For an explicit finite difference solution of dispersion terms of the solute transport equation, stability checks may be given as:

$$\Delta t \leq \text{Min} \left(\text{over grid} \right) \left[\frac{0.5}{D_{xx} / (\Delta X)^2 + D_{yy} / (\Delta Y)^2} \right] \dots\dots (1)$$

where

Δt = time increment (T),

D_{xx} = dispersion coefficient in the X direction (L^2/T),

D_{yy} = dispersion coefficient in the Y direction (L^2/T),

ΔX = grid size in the X direction, XDEL, (L),
 and ΔY = grid size in the Y direction, YDEL, (L).

This equation gives the maximum permissible time increment which is the minimum of all the time steps (Δt) computed for each individual node in the entire grid.

The second stability criteria relates the effects of mixing groundwater of one concentration with injected or recharged water of different concentration represented by the source terms. This relationship is given as:

$$\Delta t \leq \text{Min}_{(\text{over grid})} \left[\frac{\epsilon b}{W} \right] \dots \dots \dots (2)$$

where

- ϵ = effective porosity, POROS, (dimensionless),
- b = thickness of the aquifer, THCK, (L),
- and W = volume flux per unit area (L/T).

A third type of stability check involves the movement of points computed for convective transport terms of the solute transport equation. This relationship is developed as follows:

$$dx = \Delta t V_x \dots \dots \dots (3a)$$

$$dy = \Delta t V_y \dots \dots \dots (3b)$$

where

- dx = distance traveled in the X direction (L),
- dy = distance traveled in the Y direction (L),
- V_x = maximum velocity in the X direction, VMAX, (L/T),
- and V_y = maximum velocity in the Y direction, VMAY, (L/T).

If dx is greater than ΔX or dy is greater than ΔY , it might be possible for particles to move beyond the boundaries of the grid during one time

increment. Thus, for a given velocity field and grid, some restrictions must be placed on the size of the time increment to assure that neither dx nor dy exceed some critical distances (dx^* and dy^*). These critical distances relate the dimension of the grid by:

$$dx^* = \gamma \Delta X \dots\dots\dots(4a)$$

$$dy^* = \gamma \Delta Y \dots\dots\dots(4b)$$

where

γ = is the fraction of the grid dimensions that a particle will be allowed to move, CELDIS, ($0 \leq \gamma \leq 1$).

From equations 3 and 4 stability relationships may be obtained as:

$$\Delta t \leq \frac{\gamma \Delta X}{V_x} \dots\dots\dots(5a)$$

$$\Delta t \leq \frac{\gamma \Delta Y}{V_y} \dots\dots\dots(5b)$$

If the time steps used to solve the flow equation exceeds the smallest of the time steps calculated by equations 1, 2, and 5, then the time step will be subdivided into the appropriate number of smaller time increments which will be used to solve the solute transport equation. Therefore, in every time step (used to solve flow equation) each particle moves a maximum distance which is equal to the number of subtime steps times γ (represented as CELDIS in the model).

In equation 5, the optimum size of the time step is dependent on the value of γ (ΔX , ΔY , V_x , and V_y are the parameters of the flow equation). If CELDIS is smaller, the total number of time steps needed to solve the solute transport equation increases and hence the efficiency of the model decreases. This relationship can be observed from the results in the following sections.

3.3.2 Methods for Particle Movement Sensitivity Analysis

The sensitivity of the model to the number of (density) tracer particles may be evaluated by varying the value of NPTPND and keeping CELDIS constant. From the study by Konikov and Bredehoeft (1978), it was determined that the accuracy (chemical mass balance error) of the solution is directly proportional to the density (number of particles per node), while the efficiency is inversely proportional to the density.

The influence of the maximum cell distance per particle move may be evaluated by keeping NPTPND constant and running the model with several possible values of CELDIS. Konikov and Bredehoeft (1978) reported that the relationship between CELDIS and chemical mass balance error is not as simple and straightforward as for NPTPND. The effect of CELDIS on the chemical mass balance error seems to be completely problem dependent. To demonstrate the effects of CELDIS and NPTPND for different problems, the sensitivity of the modified model to these parameters has been analyzed for Test Problems 1, 2, and 3. The results of the sensitivity analysis are presented in the following sections.

3.3.3 Test Problem 1

Table 5 shows trends for Test Problem 1 and indicates that the efficiency increases with the increase of CELDIS. On the other hand the efficiency decreases with the increase of NPTPND. With respect to accuracy, the table shows no regular trend relating to either the CELDIS or the NPTPND.

3.3.4 Test Problem 2

For Test Problem 2, the trends of efficiency and accuracy are similar (see Table 6) to that of Test Problem 1 (Table 5). However, for Test

TABLE 5. Effect of CELDIS and NPTPND on Efficiency (CPU time) and Accuracy (Chemical Mass Balance Error) of Solution to Test Problem 1.

NPTPND	4		5		8		9	
	CPU	Chemical Mass Balance Error %	CPU	Chemical Mass Balance Error %	CPU	Chemical Mass Balance Error %	CPU	Chemical Mass Balance Error %
0.25	1.63	-4.10944E-01	1.97	-9.46637E-01	2.15	-2.02629E-00	2.47	-2.63050E-00
0.5	0.95	-3.83740E-00	1.05	-2.06772E-00	1.19	7.93923E-00	1.42	-2.85956E-00
0.75	0.88	-4.42353E-00	1.0	3.38968E-00	1.11	1.16942E+01	1.28	1.47898E-01
1.0	0.87	-4.42353E-00	1.0	3.38968E-00	1.13	1.16942E+01	1.28	1.47898E-01

TABLE 6. Effect of CELDIS and NPTPND on Efficiency (CPU time) and Accuracy (Chemical Mass Balance Error) of Solution to Test Problem 2.

NPTPND CELDIS	4		5		8		9	
	CPU	Chemical Mass Balance Error %	CPU	Chemical Mass Balance Error %	CPU	Chemical Mass Balance Error %	GPU	Chemical Mass Balance Error %
0.25	1.82	-3.07111E-00	2.00	-3.96768E-00	2.24	-4.58213E-00	2.46	-3.94209E-00
0.5	1.09	-1.79805E-00	1.18	-2.70483E-00	1.40	-2.45453E-00	1.41	-3.06842E-00
0.75	0.78	-2.87525E-01	0.85	4.70031E-01	0.93	-8.00412E-02	0.99	-2.08099E-01
1.0	0.68	9.28112E-01	0.73	-1.22564E-00	0.80	-2.83650E-00	0.84	-7.57554E-00

Problem 1, efficiency increases more rapidly with the increase of CELDIS than does Test Problem 2. The major difference between Test Problems 1 and 2 is the introduction of the contaminant source. In Test Problem 1, an injection source is used, and in Test Problem 2 a patch source of contamination is used. The injection source of contamination may be responsible for the relatively greater increase in efficiency.

3.3.5 Test Problem 3

For Test Problem 3, it is found (see Table 7) that the efficiency of the model does not vary significantly with the CELDIS, but it does with the NPTPND. Similarly, the accuracy varies with the NPTPND more than that of with the CELDIS. No trend could be found with regard to the variation in accuracy.

3.3.6 Conclusions

A comparison between the variation of efficiency for Test Problems 2 and 3 are shown in Figure 6. The variation of efficiency for Test Problem 1 is not shown in Figure 6 because it has a trend similar to Test Problem 1. Test Problem 3 is a one-dimensional problem and a radioactive decay term is considered in this problem. These two factors may be responsible for the differences observed (see Figure 6) between the results of Test Problems 2 and 3.

It is clear from the results of the analysis that the effects of CELDIS and NPTPND differ from problem to problem. However, the effects of CELDIS and NPTPND on the efficiency of the model follow a regular trend, though the effects of these two parameters on the accuracy of the results does not have any regular relationship.

TABLE 7. Effect of CELDIS and NPTPND on Efficiency (CPU time) and Accuracy (Chemical Mass Balance Error) of Solution to Test Problem 3.

NPTPND		4		5		8		9	
CELDIS	CPU	Chemical Mass Balance Error %	CPU	Chemical Mass Balance Error %	CPU	Chemical Mass Balance Error %	CPU	Chemical Mass Balance Error %	
0.25	2.87	-2.78318E-00	2.89	3.08818E-00	3.58	-2.65033E-00	3.94	-2.17975E-00	
0.5	2.88	-2.78318E-00	2.90	-3.08818E-00	3.57	-2.65033E-00	3.94	-2.17975E-00	
0.75	2.86	-2.78318E-00	3.22	-3.08818E-00	3.57	-2.65033E-00	3.94	-2.17975E-00	
1.00	2.86	-2.78318E-00	3.21	-3.08818E-00	3.56	-2.65033E-00	3.93	-2.17975E-00	

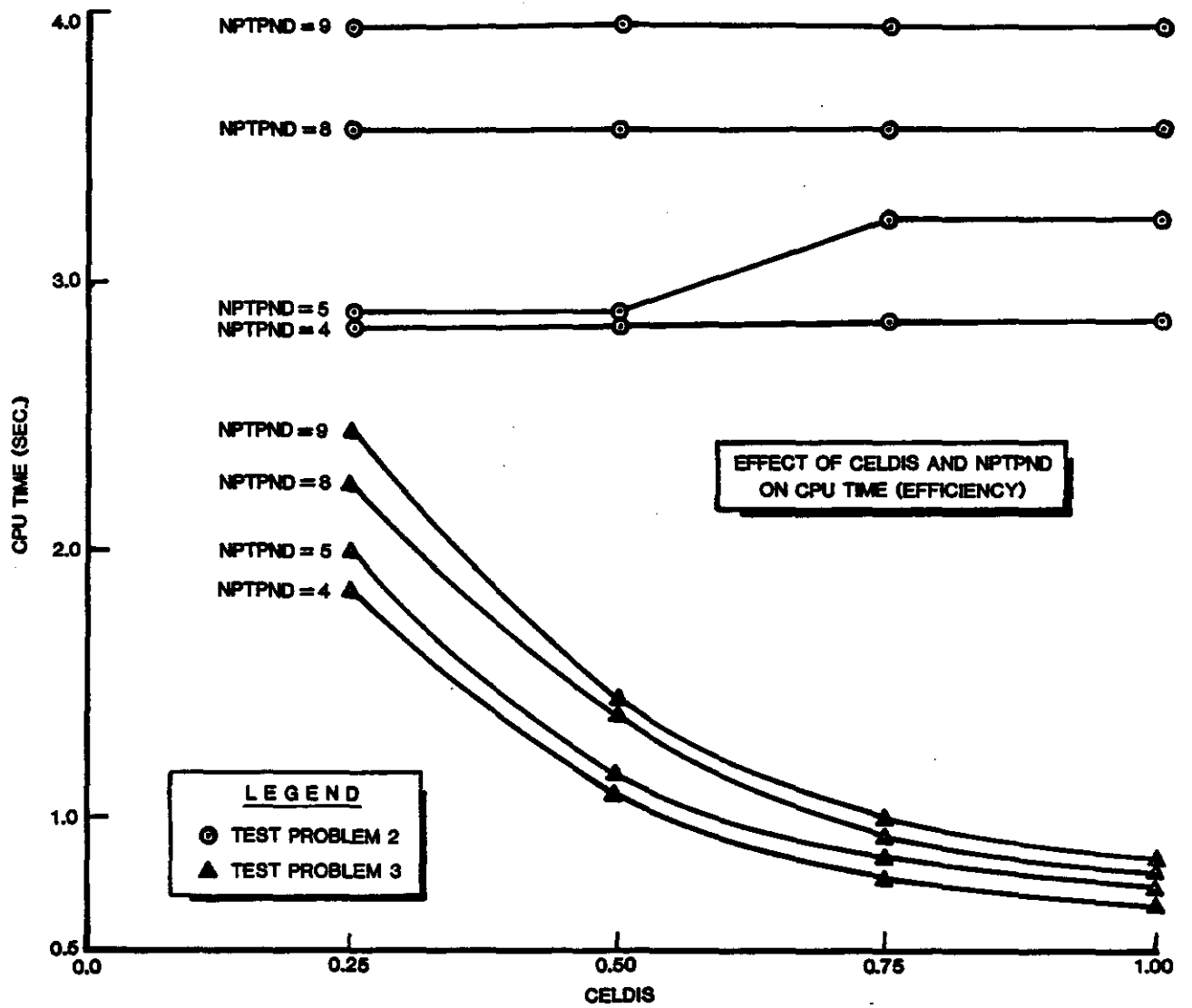


Figure 6. Effect of CELDIS and NPTPND on CPU Time (Efficiency)

Model users are assumed to be able to relate their problem to the problems used in this analysis and choose the approximate values of CELDIS and NPTPND that would result in an efficient and accurate solution. If a problem is not comparable to any one of the test problems, the modeler may want to perform a sensitivity analysis in an attempt to determine the appropriate values of CELDIS and NPTPND for the problem being considered. However, because of the possible trade off between accuracy and efficiency it is recommended that the modeler start with NPTPND as 4 or 5 and CELDIS as 0.75 to 1.0 for maximum efficiency (see Figure 6).

4.0 REFERENCES

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APPENDIX I
FORTRAN IV PROGRAM LISTING

**** TSO FOREGROUND HARDCOPY ****
DSNAME=U11236C.KONIMOD.CNTL

(MAIN)

```
C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER
C $NOFLOATCALLS
C $STORAGE:2
C DISTRIBUTED BY LOW-LEVEL WASTE LICENSING BRANCH, NRC
C LOGICAL UNIT "5" IS INPUT
C LOGICAL UNIT "6" IS OUTPUT
C LOGICAL UNIT "7" IS OPTIONAL
C *****
C * A 10
C * A 20
C * SOLUTE TRANSPORT AND DISPERSION IN A POROUS MEDIUM * A 30
C * NUMERICAL SOLUTION --- METHOD OF CHARACTERISTICS * A 40
C * PROGRAMMED BY J. D. BREDEHOEFT AND L. F. KONIKOW * A 50
C * REVISED APRIL 1979, MARCH 1980 * A 55
C * REVISED DECEMBER 1980 * A 56
C * REVISED AUGUST 1981 * A 57
C * REVISED OCTOBER 1983 * A 58
C * RADIONUCIDE DECAY AND NONLINEAR SORPTION MODIFICATIONS * USNRC
C * DEVELOPED AND IMPLEMENTED FOR US NRC BY J. TRACY * USNRC
C * AUGUST-SEPTEMBER 1981 * USNRC
C * MODIFIED NRC VERSION * OSU
C * OF THE USGS SOLUTE TRANSPORT MODEL, * OSU
C * VOLUME 1: MODIFICATIONS * OSU
C * BY * OSU
C * D.C. KENT, L. LEMASTER, AND J. WAGNER * OSU
C * FOR * OSU
C * U.S. ENVIRONMENTAL PROTECTION AGENCY * OSU
C * JANUARY, 1986 * OSU
C * A 60
C *****
C CHARACTER*8 TITLE A 70
C REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT A 90
C REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR A 100
C REAL*8 TINT,ALPHA1,ANITP A 110
C REAL*8 TMSUM,ANTIM,TDEL A 116
C REAL*8 HJ A 117
C INTEGER FCON A 118
C COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO A 120
C 1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IIPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N A 130
C 2PNCHV,NPDEL,ICLK,FCON,IHEAD,ISOLV A 142
C COMMON /PRMC/ NODEID(20,20),NPOLD(20,20),LIMBO(500), A 145
C 1IXOBS(5),IYOBS(5) A 146
C 2,NDECAY,NSORB USNRC
C COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR A 170
C 1,THICK(20,20) A 171
C COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20, A 180
C 120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T A 190
C 2ITITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR A 200
C 3,HJ(20,20) A 205
C COMMON /CHMA/ PART(3,3200),CONC(20,20),TMCN(5,50),VX(20,20),VY(20, A 210
C 120),CONINT(20,20),CNRECH(20,20),POROS,SUMTCH,BETA,TIMV,STORM,STORM A 220
C 2I,CMSIN,CMSOUT,FLMIN,FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM A 230
C 3,DCYLAM,BLKDEN,SRBRAT,SRBSAT,SRBALF,VOLDYCY,VOLSRB,SRBCY USNRC
C ***** A 240
C ---LOAD DATA--- A 250
C INT=0 A 260
C TMSUM = 0.0 A 265
C N = 0 A 266
C CALL PARLOD A 270
C IF (IHEAD.EQ.0) CALL GENPT A 281
C ***** A 290
C ---START COMPUTATIONS--- A 300
C ---COMPUTE ONE PUMPING PERIOD--- A 310
```

	DO 150 INT=1,NPMP	A 320
	N = 0	A 321
	IF (INT.GT.1) TMSUM = TMSUM + PYR	A 325
	IF (INT.GT.1) CALL PARLOD	A 330
	IPCK=0	A 336
C	---COMPUTE ONE TIME STEP---	A 340
	DO 130 N=1,NTIM	A 350
	IPRNT=0	A 360
C	---LOAD NEW DELTA T---	A 370
	TINT=SUMT-TMSUM	A 381
	TDEL=DMIN1(TIM(N),PYR-TINT)	A 390
	SUMT=SUMT+TDEL	A 400
	IF (TDEL.EQ.(PYR-TINT)) IPCK=1	A 406
	TIM(N)=TDEL	A 410
	REMN=MOD(N,NPNT)	A 420
C	*****	A 430
C	IF (S.EQ.O.O.AND.ICHK.EQ.O.O.AND.(N.GT.1.OR.INT.GT.1)) GO TO 101	A 435
	IF (ISOLV.EQ.O) GO TO 117	A 436
	CALL ISIP	A 437
	GO TO 125	A 438
117	CONTINUE	A 439
	CALL ITERAT	A 440
C	---UPDATE THCK,TMRX---	A 441A
125	IF (FCON.EQ.O) GO TO 119	A 441B
	DO 111 IY=1,NY	A 442A
	DO 111 IX=1,NX	A 442B
	IF (THICK(IX,IY).EQ.O.O) GO TO 111	A 443A
	THCK(IX,IY) = THICK(IX,IY) - HI(IX,IY) + HK(IX,IY)	A 443B
111	CONTINUE	A 444A
	NNX = NX - 1	A 444B
	NNY = NY - 1	A 445A
	DO 115 IY=2,NNY	A 445B
	DO 115 IX=2,NNX	A 446A
	IF (PERM(IX,IY).EQ.O.O) GO TO 115	A 446B
	TMRX(IX,IY,1)=2.*PERM(IX,IY)*THCK(IX,IY)*PERM(IX+1,IY)*THCK(IX+1,I	A 447A
	Y)/(PERM(IX,IY)*THCK(IX,IY)*XDEL+PERM(IX+1,IY)*THCK(IX+1,IY)*XDEL)	A 447B
	TMRX(IX,IY,2)=2.*PERM(IX,IY)*THCK(IX,IY)*PERM(IX,IY+1)*THCK(IX,IY+	A 448A
	11)/(PERM(IX,IY)*THCK(IX,IY)*YDEL+PERM(IX,IY+1)*THCK(IX,IY+1)*YDEL)	A 448B
C	---ADJUST COEFFICIENT FOR ANISOTROPY---	A 449A
	TMRX(IX,IY,2)=TMRX(IX,IY,2)*ANFCTR	A 449B
115	CONTINUE	A 450A
119	CONTINUE	A 450B
C		A 450C
	IF (REMN.EQ.O.O.OR.N.EQ.NTIM.OR.IPCK.EQ.1) CALL OUTPT	A 451
	IF (IHEAD.NE.O) GO TO 126	A 452
	CALL VELO	A 460
101	CALL MOVE	A 471
C	*****	A 480
C	---STORE OBS. WELL DATA FOR TRANSIENT FLOW PROBLEMS---	A 490
	IF (S.EQ.O.O) GO TO 120	A 500
	IF (NUMOBS.LE.O) GO TO 120	A 510
	J=MOD(N,50)	A 520
	IF (J.EQ.O) J=50	A 530
	TMOBS(J)=SUMT	A 540
	DO 110 I=1,NUMOBS	A 550
	TMWL(I,J)=HK(IXOBS(I),IYOBS(I))	A 560
	TMCN(I,J)=CONC(IXOBS(I),IYOBS(I))	A 570
110	CONTINUE	A 580
C	*****	A 590
C	---OUTPUT ROUTINES---	A 600
120	IF (REMN.EQ.O.O.OR.N.EQ.NTIM.OR.MOD(N,50).EQ.O.OR.IPCK.EQ.1)	A 611
	1 CALL CHMGT	A 612
126	CONTINUE	A 615
	IF (REMN.EQ.O.O.OR.N.EQ.NTIM.OR.IPCK.EQ.1) CALL GRPH	A 620
	IF (SUMT.GE.(PYR+TMSUM)) GO TO 140	A 621
130	CONTINUE	A 630

C	*****	A 640
C	---SUMMARY OUTPUT---	A 650
140	CONTINUE	A 660
	NND = -1	A 662
	WRITE (10,200) NND,NND	A 664
	IPRNT=1	A 670
	IF (IHEAD .EQ. 0) CALL CHMOT	A 681
150	CONTINUE	A 690
C	*****	A 700
C	ENDFILE(6)	A 702
C	IF (NPNCHV.EQ.0) GO TO 155	A 703
C	ENDFILE(7)	A 704
C 155	CONTINUE	A 705
	STOP	A 710
C	*****	A 720
200	FORMAT (1H ,2I4)	A 725
	END	A 730-

**** TSD FOREGROUND HARDCOPY ****
DSNAME=U11236C.KONIMOD.CNTL

(PARLOD)

C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER
C \$NOFLOATCALLS
C \$STORAGE:2

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SUBROUTINE PARLOD
DOUBLE PRECISION DMIN1,DEXP,DLOG,DABS
CHARACTER*8 TITLE
REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT
REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
REAL*8 FCTR,TIMX,TINIT,PIES,YNS,XNS,RAT,HMX,HMY
REAL*8 TMSUM,ANTIM,TDEL
REAL*8 DXINV,DYINV,ARINV,PORINV
REAL*8 TINT,ALPHA1,ANITP
REAL*8 HJ
INTEGER OVERRD,TP,BTM
INTEGER FCON
COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO
1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N
2PNCHV,NPDEL,ICLK,FCON,IHEAD,ISOLV
COMMON /PRMC/ NODEID(20,20),NPOLD(20,20),LIMBO(500),
1IXOBS(5),IYOBS(5)
2,NDECAY,NSORB
COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR
1,THICK(20,20)
COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20,
120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T
2TITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
3,HJ(20,20)
COMMON /CHMA/ PART(3,3200),CONC(20,20),TMCN(5,50),VX(20,20),VY(20,
120),CONINT(20,20),CNRECH(20,20),POROS,SUMTCH,BETA,TIMV,STORM,STORM
2I,CMSIN,CMSOUT,FLMIN,FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM
3,DCYLAM,BLKDEN,SRBRAT,SRBSAT,SRBALF,VOLDCY,VOLSRB,SRBDCY
COMMON /BALM/ TOTLQ,TOTLQI,TPIN,TPOUT,TPQR
COMMON /XINV/ DXINV,DYINV,ARINV,PORINV
COMMON /CHMC/ SUMC(20,20),VXBDY(20,20),VYBDY(20,20)
DIMENSION TEMP(5),IORDER(10)
DIMENSION TRANS(20,20),BOT(20,20)
DATA IORDER/5,5,4,4,3,3,2,2,1,1/
*****
C IF (INT.GT.1) GO TO 10
WRITE (6,750)
READ (5,720) TITLE
WRITE (6,730) TITLE
WRITE (10,735) INT,N,TITLE
*****
C ---INITIALIZE TEST AND CONTROL VARIABLES---
STORMI=0.0
TEST=0.0
TPQR=0.0
TOTLQ=0.0
TOTLQI=0.0
TPIN = 0.0
TPOUT = 0.0
SUMT=0.0
SUMTCH=0.0
INT=0
IPRNT=0
NCA=0
N=0
IMOV=0
NMOV=0
ICLK = 0
VOLDCY=0.0

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	VOLSRB=0.0	USNRC
	SRBDCY = 0.0	USNRC
C	*****	B 400
C	---LOAD CONTROL PARAMETERS---	B 410
	READ (5,740) NTIM, NPMP, NX, NY, NPMAX, NPNT, NITP, NUMOBS, ITMAX, NREC, NPT	B 420
	1PND, NCODES, NPNTMV, NPNTVL, NPNTD, NPDEL, NPNCHV	B 430
	READ (5,800) PINT, TOL, POROS, BETA, S, TIMX, TINIT, XDEL, YDEL, DLTRAT, CEL	B 440
	1DIS, ANFCTR	B 450
	READ (5,805) NDECAY, NSORB, DCYTIM, DENROC, SORBQR, SORBST, SORBAL	USNRC
	READ (5,740) ISOLV, IHEAD, FCON, TP, BTM	B 465
	NNX=NX-1	B 470
	NNY=NY-1	B 480
	NP=NPMAX	B 490
	DXINV=1.0/XDEL	B 500
	DYINV=1.0/YDEL	B 510
	ARINV=DXINV*DYINV	B 520
	PORINV=1.0/POROS	B 530
	DCYLAM = 0.0	USNRC
	BLKDEN = 0.0	USNRC
	SRBRAT = 0.0	USNRC
	SRBSAT = 0.0	USNRC
	SRBALF = 0.0	USNRC
	IF (NDECAY.GT.0.AND.DCYTIM.GT.0.0)	USNRC
1	DCYLAM = ALOG(2.0)/(365.25*86400.0*DCYTIM)	USNRC
	IF (NSORB.GT.0) BLKDEN = DENROC*(1.0-POROS)/POROS	USNRC
	IF (NSORB.GT.0) SRBRAT = SORBQR	USNRC
	IF (NSORB.EQ.2) SRBSAT = SORBST	USNRC
	IF (NSORB.EQ.3) SRBALF = SORBAL	USNRC
C	---PRINT CONTROL PARAMETERS---	B 540
	WRITE (6,760)	B 550
	WRITE (6,770) NX, NY, XDEL, YDEL	B 560
	WRITE (10,785) NX, NY, NTIM, NPMP, ISOLV, IHEAD, FCON, TP, BTM,	B 564
1	XDEL, YDEL, PINT	B 565
	WRITE (6,780) NTIM, NPMP, PINT, TIMX, TINIT	B 570
	WRITE (6,790) S, POROS, BETA, DLTRAT, ANFCTR	B 580
	IF (NDECAY.LT.1) WRITE (6,791)	USNRC
	IF (NDECAY.GT.0) WRITE (6,792) DCYTIM, DCYLAM	USNRC
	IF (NSORB.LT.1) WRITE (6,793)	USNRC
	IF (NSORB.GT.0) WRITE (6,794) DENROC, BLKDEN	USNRC
	IF (NSORB.EQ.1) WRITE (6,795) SRBRAT	USNRC
	IF (NSORB.EQ.2) WRITE (6,796) SRBRAT, SRBSAT	USNRC
	IF (NSORB.EQ.3) WRITE (6,797) SRBRAT, SRBALF	USNRC
	IF (ISOLV.EQ.0) WRITE (6,811)	B 585
	IF (ISOLV.NE.0) WRITE (6,812)	B 586
	IF (IHEAD.NE.0) WRITE (6,813)	B 587
	IF (FCON.EQ.0) WRITE (6,814)	B 588
	IF (FCON.NE.0) WRITE (6,815)	B 589
	IF (BTM.NE.0) WRITE (6,816)	B 589A
	WRITE (6,870) NITP, TOL, ITMAX, CELDIS, NPMAX, NPTPND	B 590
	IF (NPTPND.LT.4.OR.NPTPND.GT.9.OR.NPTPND.EQ.6.OR.NPTPND.EQ.7) WRIT	B 600
	1E (6,880)	B 610
	IF (NITP.LT.1) WRITE (6,885)	B 615
	WRITE (6,890) NPNT, NPNTMV, NPNTVL, NPNTD, NUMOBS, NREC, NCODES, NPNCHV, N	B 620
	1PDEL	B 630
	WRITE (10,895) TOL, NUMOBS, NREC, NCODES	B 640
	GO TO 20	B 650
C	*****	B 660
C	---READ DATA TO REVISE TIME STEPS AND STRESSES FOR SUBSEQUENT	B 670
C	PUMPING PERIODS---	B 680
10	READ (5,1060) ICHK	B 690
	IF (ICHK.LT.1) WRITE (6,1110) INT	B 695
	IF (ICHK.LT.1) WRITE (10,1095) INT, N, ICHK, ICHK, ICHK	B 700
	IF (ICHK.LT.1) GO TO 20	B 701
	READ (5,1070) NTIM, NPNT, NITP, ITMAX, NREC, NPNTMV, NPNTVL, NPNTD, NPDEL	B 710
	1, NPNCHV, PINT, TIMX, TINIT	B 720
	WRITE (6,1080) INT	B 730

	WRITE (6,1090) NTIM, NPNT, NITP, ITMAX, NREC, NPNTMV, NPNTVL, NPNTD, NPDEL	B 740
	1C, NPNCHV, PINT, TIMX, TINIT	B 750
	WRITE (10,1095) INT, N, NTIM, NREC, PINT	B 755
C	*****	B 760
C	---LIST TIME INCREMENTS---	B 770
	20 DO 30 J=1,100	B 780
	TIM(J)=0.0	B 790
	30 CONTINUE	B 800
	PYR = PINT*86400.0*365.25	B 805
	TIM(1)=TINIT	B 810
	IF (NPNTMV.EQ.0) NPNTMV = 999	B 815
	IF (S.EQ.0.0) GO TO 50	B 820
	DO 40 K=2,NTIM	B 830
	40 TIM(K)=TIMX*TIM(K-1)	B 840
	WRITE (6,470)	B 850
	WRITE (6,490) TIM	B 860
	IF (TINIT.GT.PYR) WRITE (6,475)	B 865
	GO TO 60	B 870
	50 ANTIM = NTIM	B 882
	DO 55 K=1,NTIM	B 884
	55 TIM(K)=PYR/ANTIM	B 886
	WRITE (6,480) TIM(1)	B 890
C	*****	B 900
C	---INITIALIZE MATRICES---	B 910
	60 IF (INT.GT.1) GO TO 100	B 920
	DO 70 IY=1,NY	B 930
	DO 70 IX=1,NX	B 940
	VPRM(IX,IY)=0.0	B 950
	PERM(IX,IY)=0.0	B 960
	TRANS(IX,IY)=0.0	B 962
	BOT(IX,IY)=0.0	B 964
	THCK(IX,IY)=0.0	B 970
	THICK(IX,IY)=0.0	B 971
	RECH(IX,IY)=0.0	B 980
	CNRECH(IX,IY)=0.0	B 990
	REC(IX,IY)=0.0	B1000
	NODEID(IX,IY)=0	B1010
	TMRX(IX,IY,1)=0.0	B1020
	TMRX(IX,IY,2)=0.0	B1030
	HI(IX,IY)=0.0	B1040
	HR(IX,IY)=0.0	B1050
	HC(IX,IY)=0.0	B1060
	HK(IX,IY)=0.0	B1070
	WT(IX,IY)=0.0	B1080
	VX(IX,IY)=0.0	B1090
	VY(IX,IY)=0.0	B1100
	VXBDY(IX,IY)=0.0	B1110
	VYBDY(IX,IY)=0.0	B1120
	CONC(IX,IY)=0.0	B1130
	CONINT(IX,IY)=0.0	B1140
	SUMC(IX,IY)=0.0	B1150
	70 CONTINUE	B1160
C	*****	B1170
C	---READ OBSERVATION WELL LOCATIONS---	B1180
	IF (NUMOBS.LE.0) GO TO 100	B1190
	WRITE (6,900)	B1200
	DO 80 J=1,NUMOBS	B1210
	READ (5,700) IX,IY	B1220
	WRITE (6,810) J,IX,IY	B1230
	WRITE (10,1095) INT,N,IX,IY	B1235
	IXOBS(J)=IX	B1240
	80 IYOBS(J)=IY	B1250
	DO 90 I=1,NUMOBS	B1260
	DO 90 J=1,50	B1270
	TMWL(I,J)=0.0	B1280
	90 TMCN(I,J)=0.0	B1290

C	*****	B1300
C	---READ PUMPAGE DATA -- (X-Y COORDINATES AND RATE IN CFS)---	B1310
C	---SIGNS : WITHDRAWAL = POS.; INJECTION = NEG.---	B1320
C	---IF INJ. WELL, ALSO READ CONCENTRATION OF INJECTED WATER---	B1330
100	IF (NREC.LE.O) GO TO 120	B1340
	IF (INT.GT.1.AND.ICHK.LE.O) RETURN	B1345
	WRITE (6,910)	B1350
	DO 110 I=1,NREC	B1360
	READ (5,710) IX,IY,FCTR,CNREC	B1370
	IF (FCTR.LE.O.O) CNRECH(IX,IY)=CNREC	B1380
	REC(IX,IY)=FCTR	B1390
	WRITE (10,825) INT,N,IX,IY,REC(IX,IY),CNRECH(IX,IY)	B1395
110	WRITE (6,820) IX,IY,REC(IX,IY),CNRECH(IX,IY)	B1400
C	*****	B1410
120	IF (INT.GT.1) RETURN	B1420
	AREA=XDEL*YDEL	B1430
	WRITE (6,690) AREA	B1440
	WRITE (6,600)	B1450
	WRITE (6,610) XDEL	B1460
	WRITE (6,610) YDEL	B1470
C	*****	B1480
C	---READ TRANS(FT**2/SEC) OR PERM(FT/SEC) INTO VPRM ARRAY---	B1490
C	---DEPENDING ON VALUE OF TP---	B1491
C	---FCTR = TRANS (OR PERM) MULTIPLIER ---> FT**2/SEC---	B1500
C	WRITE (6,530)	B1510
	READ (5,550) INPUT,FCTR	B1520
	DO 160 IY=1,NY	B1530
	IF (INPUT.EQ.1) READ (5,560) (VPRM(IX,IY),IX=1,NX)	B1540
	DO 150 IX=1,NX	B1550
	IF (INPUT.NE.1) GO TO 130	B1560
	VPRM(IX,IY)=VPRM(IX,IY)*FCTR	B1570
	GO TO 140	B1580
130	VPRM(IX,IY)=FCTR	B1590
140	IF (IX.EQ.1.OR.IX.EQ.NX) VPRM(IX,IY)=O.O	B1600
	IF (IY.EQ.1.OR.IY.EQ.NY) VPRM(IX,IY)=O.O	B1610
	IF (TP.NE.O) PERM(IX,IY)=VPRM(IX,IY)	B1611
150	CONTINUE	B1620
160	CONTINUE	B1632
C	*****	B1920
C	---READ AQUIFER THICKNESS---	B1930
	IF (BTM.EQ.O) WRITE (6,510)	B1942
	IF (BTM.NE.O) WRITE (6,520)	B1944
	READ (5,550) INPUT,FCTR	B1950
	DO 210 IY=1,NY	B1960
	IF (INPUT.EQ.1) READ (5,540) (THCK(IX,IY),IX=1,NX)	B1970
	DO 200 IX=1,NX	B1980
	IF (INPUT.NE.1) GO TO 190	B1990
	THCK(IX,IY)=THCK(IX,IY)*FCTR	B2000
	GO TO 195	B2011
190	IF (VPRM(IX,IY).NE.O.O) THCK(IX,IY)=FCTR	B2020
195	THCK(IX,IY)=THCK(IX,IY)	B2021
	IF (BTM.NE.O) BOT(IX,IY)=THCK(IX,IY)	B2022
200	CONTINUE	B2030
210	WRITE (6,500) (THCK(IX,IY),IX=1,NX)	B2040
C	*****	B2041
C	---READ WATER-TABLE ELEVATION---	B2046
	WRITE (6,670)	B2051
	READ (5,550) INPUT,FCTR	B2056
	DO 350 IY=1,NY	B2061
	IF (INPUT.EQ.1) READ (5,660) (WT(IX,IY),IX=1,NX)	B2066
	DO 340 IX=1,NX	B2071
	IF (INPUT.NE.1) GO TO 330	B2076
	WT(IX,IY)=WT(IX,IY)*FCTR	B2081
	GO TO 340	B2086
330	IF (VPRM(IX,IY).NE.O.O) WT(IX,IY)=FCTR	B2091
340	CONTINUE	B2096

350	WRITE (6,680) (WT(IX,IY),IX=1,NX)	B2101
C	---CALCULATE SATURATED THICKNESS---	B2103
	IF (BTM.EQ.O) GO TO 356	B2106
	WRITE (6,510)	B2111
	DO 354 IY=1,NY	B2116
	DO 352 IX=1,NX	B2121
	THCK(IX,IY)=WT(IX,IY)-THCK(IX,IY)	B2126
	THICK(IX,IY)=THCK(IX,IY)	B2131
352	CONTINUE	B2136
354	WRITE (6,500) (THCK(IX,IY),IX=1,NX)	B2141
356	CONTINUE	B2146
C	*****	B2180
C	---COMPUTE PERMEABILITY FROM TRANSMISSIVITY---	B2190
C	---COUNT NO. OF CELLS IN AQUIFER---	B2200
C	---SET NZCRIT = 2(OF THE NO. OF CELLS IN THE AQUIFER---	B2210
	DO 250 IX=1,NX	B2220
	DO 250 IY=1,NY	B2230
	IF (THCK(IX,IY).EQ.O.O) GO TO 250	B2240
	IF (TP .EQ. O) PERM(IX,IY)=VPRM(IX,IY)/THCK(IX,IY)	B2252
	IF (TP .NE. O) VPRM(IX,IY)=PERM(IX,IY)*THCK(IX,IY)	B2254
	TRANS(IX,IY)=VPRM(IX,IY)	B2256
	NCA=NCA+1	B2260
250	CONTINUE	B2271
C		B2272
C	---WRITE TRANSMISSIVITY---	B2273
	WRITE (6,530)	B2274
	DO 255 IY=1,NY	B2275
255	WRITE (6,840) (VPRM(IX,IY),IX=1,NX)	B2276
C		B2280
	AAQ=NCA*AREA	B2290
	NZCRIT=(NCA+25)/50	B2300
	WRITE (6,620)	B2310
	DO 260 IY=1,NY	B2320
260	WRITE (6,840) (PERM(IX,IY),IX=1,NX)	B2331
	WRITE (6,630) NCA,AAQ,NZCRIT	B2340
C	*****	B2350
C	---SET UP COEFFICIENT MATRIX --- BLOCK-CENTERED GRID---	B2351A
C	---AVERAGE TRANSMISSIVITY --- HARMONIC MEAN---	B2351B
C	---MOVED SO THAT PERMEABILTY OR TRANSMISSIVITY MAY---	B2351C
C	---BE INPUT AND CALCULATED PROPERLY---	B2351D
	IF (ANFCTR.NE.O.O) GO TO 170	B2351E
	WRITE (6,1050)	B2352A
	ANFCTR=1.O	B2352B
170	PIES=3.1415927*3.1415927/2.O	B2352C
	YNS=NY*NY	B2352D
	XNS=NX*NX	B2352E
	HMIN=2.O	B2353A
	DO 180 IY=2,NNY	B2353B
	DO 180 IX=2,NNX	B2353C
	IF (VPRM(IX,IY).EQ.O.O) GO TO 180	B2353D
	TMRX(IX,IY,1)=2.O*VPRM(IX,IY)*VPRM(IX+1,IY)/(VPRM(IX,IY)*XDEL+VPRM	B2353E
	1(IX+1,IY)*XDEL)	B2354A
	TMRX(IX,IY,2)=2.O*VPRM(IX,IY)*VPRM(IX,IY+1)/(VPRM(IX,IY)*YDEL+VPRM	B2354B
	1(IX,IY+1)*YDEL)	B2354C
C	---ADJUST COEFFICIENT FOR ANISOTROPY---	B2354D
	TMRX(IX,IY,2)=TMRX(IX,IY,2)*ANFCTR	B2354E
C	---COMPUTE MINIMUM ITERATION PARAMETER (HMIN)---	B2355A
	IF (TMRX(IX,IY,1).EQ.O.O) GO TO 180	B2355B
	IF (TMRX(IX,IY,2).EQ.O.O) GO TO 180	B2355C
	RAT=TMRX(IX,IY,1)*YDEL/(TMRX(IX,IY,2)*XDEL)	B2355D
	HMX=PIES/(XNS*(1.O+RAT))	B2355E
	HMY=PIES/(YNS*(1.O+(1.O/RAT)))	B2356A
	IF (HMX.LT.HMIN) HMIN=HMX	B2356B
	IF (HMY.LT.HMIN) HMIN=HMY	B2356C
180	VPRM(IX,IY)=O.O	B2356D
C	*****	B2356E

C	---READ DIFFUSE RECHARGE AND DISCHARGE---	B2357A
	WRITE (6,830)	B2357B
	READ (5,550) INPUT,FCTR	B2357C
	DO 240 IY=1,NY	B2357D
	IF (INPUT.EQ.1) READ (5,560) (RECH(IX,IY),IX=1,NX)	B2357E
	DO 230 IX=1,NX	B2358A
	IF (INPUT.NE.1) GO TO 220	B2358B
	RECH(IX,IY)=RECH(IX,IY)*FCTR	B2358C
	GO TO 230	B2358D
	220 IF (THCK(IX,IY).NE.O.O) RECH(IX,IY)=FCTR	B2358E
	230 CONTINUE	B2359A
	240 WRITE (6,840) (RECH(IX,IY),IX=1,NX)	B2359B
C	*****	B2359C
C	---READ NODE IDENTIFICATION CARDS---	B2360
C	---SET VERT. PERM., SOURCE CONC., AND DIFFUSE RECHARGE---	B2370
C	---SPECIFY CODES TO FIT YOUR NEEDS---	B2380
	WRITE (6,570)	B2390
	READ (5,550) INPUT,FCTR	B2400
	DO 280 IY=1,NY	B2410
	IF (INPUT.EQ.1) READ (5,640) (NODEID(IX,IY),IX=1,NX)	B2420
	DO 270 IX=1,NX	B2430
	270 IF (INPUT.NE.1.AND.THCK(IX,IY).NE.O.O) NODEID(IX,IY)=FCTR	B2440
	280 WRITE (6,580) (NODEID(IX,IY),IX=1,NX)	B2450
	WRITE (6,920) NCODES	B2460
	IF (NCODES.LE.O) GO TO 310	B2470
	WRITE (6,930)	B2480
	DO 300 IJ=1,NCODES	B2490
	READ (5,850) ICODE,FCTR1,FCTR2,FCTR3,OVERRD	B2500
	DO 290 IX=1,NX	B2510
	DO 290 IY=1,NY	B2520
	IF (NODEID(IX,IY).NE.ICODE) GO TO 290	B2530
	VPRM(IX,IY)=FCTR1	B2540
	CNRECH(IX,IY)=FCTR2	B2550
	IF (OVERRD.NE.O) RECH(IX,IY)=FCTR3	B2560
	290 CONTINUE	B2570
	WRITE (6,860) ICODE,FCTR1,FCTR2	B2580
	WRITE (10,865) INT,N,ICODE,FCTR1,FCTR2,FCTR3	B2585
	300 IF (OVERRD.NE.O) WRITE (6,1100) FCTR3	B2590
	310 WRITE (6,590)	B2600
	DO 320 IY=1,NY	B2610
	320 WRITE (6,840) (VPRM(IX,IY),IX=1,NX)	B2621
C	*****	B2760
C	DO 335 IY=1,NY	B2761
C	DO 335 IX=1,NX	B2762
	335 WRITE (10,845) INT,N,IX,IY,BOT(IX,IY),WT(IX,IY),THCK(IX,IY),	B2763
	1 TRANS(IX,IY),PERM(IX,IY),RECH(IX,IY),NODEID(IX,IY),VPRM(IX,IY)	B2764
C	---SET INITIAL HEADS---	B2770
	DO 360 IX=1,NX	B2780
	DO 360 IY=1,NY	B2790
	HI(IX,IY)=WT(IX,IY)	B2800
	HC(IX,IY)=HI(IX,IY)	B2810
	HR(IX,IY)=HI(IX,IY)	B2820
	360 HK(IX,IY)=HI(IX,IY)	B2830
C		B2840
	CALL OUTPT	B2850
C	*****	B2860
C	---COMPUTE ITERATION PARAMETERS---	B2870
C	---COMPUTE ADIP ITERATION PARAMETERS---	B2872
	DO 370 ID=1,20	B2880
	AOPT(ID)=O.O	B2890
	370 CONTINUE	B2900
	IF (ISOLV.NE.O) GO TO 299	B2902
	ANITP=NITP-1	B2910
	ALPHA1 = 1.O	USNRC
	IF (HMIN.LT.2.O) ALPHA1= DEXP(DLOG(1.O/HMIN)/ANITP)	USNRC
	IF (HMIN.EQ.2.O) HMIN = O.O	USNRC

	AOPT(1)=HMIN	B2930
	DO 380 IP=2,NITP	B2940
380	AOPT(IP)=AOPT(IP-1)*ALPHA1	B2950
	GO TO 401	B2951A
299	CONTINUE	B2951B
C	*****	B2952A
C	---COMPUTE SIP ITERATION PARAMETERS---	B2952B
	I2=NX-2	B2953A
	J2=NY-2	B2953B
	LENGTH=10	B2954A
	W=0.0	B2954B
	PI=0.0	B2955A
	L2=LENGTH/2	B2955B
	PL2=FLOAT(L2)-1.0	B2956A
	WIDTH=FLOAT(I2)	B2956B
	YDIM=FLOAT(J2)	B2957A
	DX=1./WIDTH	B2957B
	DY=1./YDIM	B2958A
C	*****	B2958B
C	---COMPUTE AVERAGE MAXIMUM VALUE OF ITERATION PARAMETER---	B2959A
	DO 11 J=2,NNY	B2959B
	DO 11 I=2,NNX	B2960A
	PI=PI+1.0	B2960B
	W=W+1.0-AMIN1(2.*DX*DX/(1.+ANFCTR*DX*DX/(DY*DY)),	B2961C
	2.*DY*DY/(1.+DY*DY/(ANFCTR*DX*DX)))	B2961D
11	CONTINUE	B2962A
	W=W/PI	B2962B
C	*****	B2963A
C	---COMPUTE ITERATION PARAMETER IN GEOMETRIC SEQUENCE-----	B2963B
	PJ=-1.0	B2964A
	DO 21 I=1,L2	B2964B
	PJ=PJ+1.0	B2965A
21	TEMP(I)=1.0-(1.0-W)**(PJ/PL2)	B2965B
C	*****	B2966A
C	---ORDER SEQUENCE OF PARAMETERS---	B2966B
	DO 31 J=1,LENGTH	B2967A
31	AOPT(J)=TEMP(IORDER(J))	B2967B
401	CONTINUE	B2968A
C	---PRINT ITERATION PARAMETERS---	B2968B
	WRITE (6,450)	B2970
	WRITE (6,460) AOPT	B2980
C	*****	B2990
C	---READ INITIAL CONCENTRATIONS AND COMPUTE INITIAL MASS STORED---	B3000
	READ (5,550) INPUT,FCTR	B3010
	DO 420 IY=1,NY	B3020
	IF (INPUT.EQ.1) READ (5,660) (CONC(IX,IY),IX=1,NX)	B3030
	DO 410 IX=1,NX	B3040
	IF (INPUT.NE.1) GO TO 390	B3050
	CONC(IX,IY)=CONC(IX,IY)*FCTR	B3060
	GO TO 400	B3070
390	IF (THCK(IX,IY).NE.0.0) CONC(IX,IY)=FCTR	B3080
400	CONINT(IX,IY)=CONC(IX,IY)	B3090
410	STORMI=STORMI+CONINT(IX,IY)*THCK(IX,IY)*AREA*POROS	B3100
420	CONTINUE	B3110
C	*****	B3120
C	---CHECK DATA SETS FOR INTERNAL CONSISTENCY---	B3130
	DO 440 IX=1,NX	B3140
	DO 440 IY=1,NY	B3150
	IF (RECH(IX,IY).GT.0.0) WRITE (6,935) IX,IY	B3151
	IF (THCK(IX,IY).GT.0.0) GO TO 430	B3160
	IF (THCK(IX,IY).EQ.0.0) GO TO 434	B3162
	WRITE (6,945) IX,IY	B3164
	GO TO 440	B3166
434	CONTINUE	B3168
	IF (TMRX(IX,IY,1).GT.0.0) WRITE (6,940) IX,IY	B3170
	IF (TMRX(IX,IY,2).GT.0.0) WRITE (6,950) IX,IY	B3180

	IF (NODEID(IX,IY).GT.0) WRITE (6,960) IX,IY	B3190
	IF (WT(IX,IY).NE.0.0) WRITE (6,970) IX,IY	B3200
	IF (RECH(IX,IY).NE.0.0) WRITE (6,980) IX,IY	B3210
	IF (REC(IX,IY).NE.0.0) WRITE (6,990) IX,IY	B3220
430	IF (PERM(IX,IY).GT.0.0) GO TO 440	B3230
	IF (NODEID(IX,IY).GT.0.0) WRITE (6,1000) IX,IY	B3240
	IF (WT(IX,IY).NE.0.0) WRITE (6,1010) IX,IY	B3250
	IF (RECH(IX,IY).NE.0.0) WRITE (6,1020) IX,IY	B3260
	IF (REC(IX,IY).NE.0.0) WRITE (6,1030) IX,IY	B3270
	IF (THCK(IX,IY).GT.0.0) WRITE (6,1040) IX,IY	B3280
440	CONTINUE	B3290
C	*****	B3300
	RETURN	B3310
C	*****	B3320
C		B3330
C		B3340
C		B3350
450	FORMAT (1H1,20HITERATION PARAMETERS)	B3360
460	FORMAT (1H ,/, 1P8E10.3/ 1P8E10.3)	B3370
470	FORMAT (1H1,27HTIME INTERVALS (IN SECONDS))	B3380
475	FORMAT (1H0,5X,65H*** WARNING *** INITIAL TIME STEP IS LONGER TH 1AN PUMPING PERIOD/25X,34H***ADJUST EITHER TINIT OR PINT.***//)	B3384
480	FORMAT (1H1,15X,17HSTEADY-STATE FLOW//5X,57HTIME INTERVAL (IN SEC) 1 FOR SOLUTE-TRANSPORT SIMULATION = ,1P1E12.5)	B3390
490	FORMAT (3H ,10G12.5)	B3400
500	FORMAT (3H ,20F5.1)	B3410
510	FORMAT (1H1,22HAQUIFER THICKNESS (FT))	B3420
520	FORMAT (1H1,19HAQUIFER BOTTOM (FT))	B3430
530	FORMAT (1H1,30HTRANSMISSIVITY MAP (FT*FT/SEC))	B3435
540	FORMAT (26G3.0)	B3450
550	FORMAT (I1,G10.0)	B3461
560	FORMAT (20G4.1)	B3470
570	FORMAT (1H1,23HNODE IDENTIFICATION MAP//)	B3480
580	FORMAT (1H ,20I5)	B3490
590	FORMAT (1H1,45HVERTICAL PERMEABILITY/THICKNESS (FT/(FT*SEC)))	B3500
600	FORMAT (1H0,10X,12HX-Y SPACING:)	B3510
610	FORMAT (1H ,12X,10G12.5)	B3520
620	FORMAT (1H1,24HPERMEABILTY MAP (FT/SEC))	B3530
630	FORMAT (1H0,////10X,44HNO. OF FINITE-DIFFERENCE CELLS IN AQUIFER = 1 ,I4//10X,28HAREA OF AQUIFER IN MODEL = ,1P1E12.5,8H SQ. FT.////1 20X,47HNZCRIT (MAX. NO. OF CELLS THAT CAN BE VOID OF/20X,56HPARTI 3CLES; IF EXCEEDED, PARTICLES ARE REGENERATED) = ,I4//)	B3540
640	FORMAT (80I1)	B3550
660	FORMAT (20G4.0)	B3560
670	FORMAT (1H1,11HWATER TABLE)	B3570
680	FORMAT (1H ,20F5.0)	B3580
690	FORMAT (1H0,10X,19HAREA OF ONE CELL = ,1P1E12.4)	B3591
700	FORMAT (2I2)	B3610
710	FORMAT (2I2,2G8.2)	B3620
720	FORMAT (10A8)	B3630
730	FORMAT (1H0,10A8)	B3640
735	FORMAT (1H ,2I4/10A8)	B3650
740	FORMAT (17I4)	B3660
750	FORMAT (1H1,77HU.S.G.S. METHOD-OF-CHARACTERISTICS MODEL FOR SOLUTE 1 TRANSPORT IN GROUND WATER)	B3670
760	FORMAT (1H0,21X,21HI N P U T D A T A)	B3680
770	FORMAT (1H0,23X,16HGRID DESCRIPTORS//13X,30HNX (NUMBER OF COLUM 1NS) = ,I4/13X,28HNY (NUMBER OF ROWS) = ,I6/13X,29HXDEL (X 2-DISTANCE IN FEET) = ,F7.1/13X,29HYDEL (Y-DISTANCE IN FEET) = ,F7 3.1)	B3700
780	FORMAT (1H0,23X,16HTIME PARAMETERS//13X,40HNTIM (MAX. NO. OF TI 1ME STEPS) = ,I6/13X,40HNPM (NO. OF PUMPING PERIODS) 2 = ,I6/13X,39HPINT (PUMPING PERIOD IN YEARS) = ,F11.3/13X,39 3HTIMX (TIME INCREMENT MULTIPLIER) = ,F10.2/13X,39HTINIT (INIT 4IAL TIME STEP IN SEC.) = ,G10.2)	B3710
785	FORMAT (1H ,9I4,3F11.3)	B3720
		B3730
		B3740
		B3750
		B3760
		B3770
		B3780
		B3791
		B3800
		B3811
		B3815

790	FORMAT (1HO,14X,34H	HYDROLOGIC AND CHEMICAL PARAMETERS//13X,1HS,7X,129H(STORAGE COEFFICIENT) = .5X,F9.6/13X,28H	POROS (EFFECTIVE POROSITY),8X,3H= .F8.2/13X,39HBETA (CHARACTERISTIC LENGTH)	B3820 B3830 B3840 B3850 B3860 B3870
	3	= .F7.1/13X,31HDLTRAT (RATIO OF TRANSVERSE TO/21X,30HLONGITUDINAL DISPERSIVITY) = .F9.2/13X,39HANFCTR (RATIO OF T-YY TO T-XX)		B3880
	5	= .F12.6)		B3890
791	FORMAT (1HO,1X,26H***NON-DECAYING SPECIES***)			USNRC
792	FORMAT (1HO,1X,28HSPECIES HALF LIFE (YEARS) = ,1P1E10.3,			USNRC
	1	30H OR DECAY CONSTANT (1/SECS) = ,1P1E10.3)		USNRC
793	FORMAT (1HO,1X,25H***NON-SORBING SPECIES***)			USNRC
794	FORMAT (1HO,1X,27HROCK DENSITY (GRM/CM**3) = ,1P1E10.3,			USNRC
	1	24HBULK DENSITY/POROSITY = ,1P1E10.3)		USNRC
795	FORMAT (1HO,1X,21H***LINEAR SORPTION***,			USNRC
	1	1X,29HDISTRIBUTION CONSTANT (KD) = ,1P1E10.3)		USNRC
796	FORMAT (1HO,1X,23H***LANGMUIR ISOTHERM***,			USNRC
	1	1X,16HRATE CONSTANT = ,1P1E10.3,		USNRC
	2	1X,22HSATURATION CONSTANT = ,1P1E10.3)		USNRC
797	FORMAT (1HO,1X,25H***FREUNDLICH ISOTHERM***,			USNRC
	1	1X,16HRATE CONSTANT = ,1P1E10.3,		USNRC
	2	1X,19HEXPONENT (ALPHA) = ,1P1E10.3)		USNRC
800	FORMAT (12G5.0)			B3880
805	FORMAT (2I5,5G10.0)			USNRC
810	FORMAT (1H ,16X,12,5X,12,4X,12)			B3890
811	FORMAT (1HO,1X,15H***ADIP USED***)			B3891A
812	FORMAT (1HO,1X,14H***SIP USED***)			B3891B
813	FORMAT (1HO,1X,26H***HEAD ONLY SIMULATION***)			B3891C
814	FORMAT (1HO,1X,22H***CONFINED AQUIFER***)			B3891D
815	FORMAT (1HO,1X,24H***UNCONFINED AQUIFER***)			B3891E
816	FORMAT (1HO,1X,18H***BOTTOM INPUT***)			B3891F
820	FORMAT (1H ,7X,2I4,3X,E9.3,3X,F8.2)			B3895
825	FORMAT (1H ,4I4,2E9.3)			B3900
830	FORMAT (1H1,39HDIFFUSE RECHARGE AND DISCHARGE (FT/SEC))			B3910
840	FORMAT (1H ,1P10E10.2)			B3920
845	FORMAT (1H ,4I4/3F10.4,3E10.2,I10,E10.2)			B3925
850	FORMAT (I2,3G10.2,I2)			B3930
860	FORMAT (1HO,7X,12,7X,1P1E10.3,4X,1P1E10.3)			B3940
865	FORMAT (1H ,3I4,1P3E10.3)			B3945
870	FORMAT (1HO,21X,20HEXECUTION PARAMETERS//13X,39HNITP (NO. OF ITE			B3950
	1R. PARAM - ADIP) = ,I4/13X,39HTOL (CONVERGENCE CRITERIA)			B3965
	2 = ,F9.4/13X,39HITMAX (MAX.NO.OF ITERATIONS) = ,I4/13X,3			B3975
	34HCELDISE (MAX.CELL DISTANCE PER MOVE/24X,28HOF PARTICLES - M.O.C.)			B3980
	4 = ,F8.3/13X,30HNPMAX (MAX. NO. OF PARTICLES),7X,2H= ,I4/12X,3			B3990
	52H NPTPND (NO. PARTICLES PER NODE),6X,3H= ,I4)			B4000
880	FORMAT (1HO,5X,47H*** WARNING *** NPTPND MUST EQUAL 4,5,8, OR 9.)			B4010
885	FORMAT (1HO,5X,38H*** WARNING *** NITP MUST BE POSITIVE)			B4015
890	FORMAT (1HO,23X,15HPROGRAM OPTIONS//13X,30HNPNT (TIME STEP INTER			B4020
	1VAL FOR/21X,18HCOMPLETE PRINTOUT),7X,3H= ,I4/13X,31HNPNTMV (MOVE			B4030
	2INTERVAL FOR CHEM./21X,28HCONCENTRATION PRINTOUT) = ,I4/13X,29HN			B4040
	3PNTVL (PRINT OPTION-VELOCITY/21X,24HO=NO; 1=FIRST TIME STEP;/21X,1			B4050
	47H2=ALL TIME STEPS),8X,3H= ,I4/13X,31HNPNTD (PRINT OPTION-DISP.C			B4060
	5DEF./21X,24HO=NO; 1=FIRST TIME STEP;/21X,17H2=ALL TIME STEPS),8X,3			B4070
	6H= ,I4/13X,32HNUMOBS (NO. OF OBSERVATION WELLS/21X,28HFOR HYDROGR			B4080
	7APH PRINTOUT) = ,I4/13X,35HNREC (NO. OF PUMPING WELLS) = ,I5			B4090
	8/13X,24HNCODES (FOR NODE IDENT.),9X,2H= ,I5/13X,25HNPNCNV (PUNCH V			B4100
	9VELOCITIES),8X,2H= ,I5/13X,36HNPDEL (PRINT OPT.-CONC. CHANGE) = ,			B4110
	\$I4)			B4120
895	FORMAT (1H ,F9.4,3I4)			B4125
900	FORMAT (1HO,10X,29HLOCATION OF OBSERVATION WELLS//17X,3HNO.,5X,1HX			B4130
	1,5X,1HY//)			B4140
910	FORMAT (1HO,10X,28HLOCATION OF PUMPING WELLS//11X,28HX Y RA			B4150
	1TE(IN CFS) CONC./)			B4160
920	FORMAT (1HO,5X,37HNO. OF NODE IDENT. CODES SPECIFIED = ,I2)			B4170
930	FORMAT (1HO,10X,41HTHE FOLLOWING ASSIGNMENTS HAVE BEEN MADE:/5X,5I			B4180
	1HCODE NO. LEAKANCE SOURCE CONC. RECHARGE)			B4190
935	FORMAT (1H ,5X,42H*** WARNING *** RECH.GT.O.O AT NODE IX = ,I4,			B4191
	1 6H, IY = ,I4)			B4192

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940 FORMAT (1H ,5X,61H*** WARNING *** THCK.EQ.O.O AND TMRX(X).GT.O.O B4200
1 AT NODE IX =,I4,6H, IY =,I4) B4210
945 FORMAT (1H ,5X,42H*** WARNING *** THCK.LT.O.O AT NODE IX =,I4, B4212
1 6H, IY =,I4) B4214
950 FORMAT (1H ,5X,61H*** WARNING *** THCK.EQ.O.O AND TMRX(Y).GT.O.O B4220
1 AT NODE IX =,I4,6H, IY =,I4) B4230
960 FORMAT (1H ,5X,61H*** WARNING *** THCK.EQ.O.O AND NODEID.GT.O.O B4240
1 AT NODE IX =,I4,6H, IY =,I4) B4250
970 FORMAT (1H ,5X,56H*** WARNING *** THCK.EQ.O.O AND WT.NE.O.O AT N B4260
1ODE IX =,I4,6H, IY =,I4) B4270
980 FORMAT (1H ,5X,58H*** WARNING *** THCK.EQ.O.O AND RECH.NE.O.O AT B4280
1 NODE IX =,I4,6H, IY =,I4) B4290
990 FORMAT (1H ,5X,58H*** WARNING *** THCK.EQ.O.O AND REC.NE.O.O AT B4300
1 NODE IX =,I4,6H, IY =,I4) B4310
1000 FORMAT (1H ,5X,61H*** WARNING *** PERM.EQ.O.O AND NODEID.GT.O.O B4320
1 AT NODE IX =,I4,6H, IY =,I4) B4330
1010 FORMAT (1H ,5X,56H*** WARNING *** PERM.EQ.O.O AND WT.NE.O.O AT N B4340
1ODE IX =,I4,6H, IY =,I4) B4350
1020 FORMAT (1H ,5X,58H*** WARNING *** PERM.EQ.O.O AND RECH.NE.O.O AT B4360
1 NODE IX =,I4,6H, IY =,I4) B4370
1030 FORMAT (1H ,5X,58H*** WARNING *** PERM.EQ.O.O AND REC.NE.O.O AT B4380
1 NODE IX =,I4,6H, IY =,I4) B4390
1040 FORMAT (1H ,5X,58H*** WARNING *** PERM.EQ.O.O AND THCK.GT.O.O AT B4400
1 NODE IX =,I4,6H, IY =,I4) B4410
1050 FORMAT (1H0,5X,45H*** WARNING *** ANFCTR WAS SPECIFIED AS O.O/23 B4420
1X,34HDEFAULT ACTION: RESET ANFCTR = 1.0) B4430
1060 FORMAT (I1) B4440
1070 FORMAT (10I4,3G5.O) B4450
1080 FORMAT (1H1,5X,25HSTART PUMPING PERIOD NO. ,I2//2X,75HTHE FOLLOWIN B4460
1G TIME STEP, PUMPAGE, AND PRINT PARAMETERS HAVE BEEN REDEFINED:/) B4470
1090 FORMAT (1H0,14X,9HNTIM = ,I4/15X,9HNPNT = ,I4/15X,9HNITP = , B4480
1I4/15X,9HITMAX = ,I4/15X,9HNREC = ,I4/15X,9HNPNTMV = ,I4/15X,9H B4490
2NPNTVL = ,I4/15X,9HNPNTD = ,I4/15X,9HNPDEL = ,I4/15X,9HNPCHV = B4500
3,I4/15X,9HPINT = ,F10.3/15X,9HTIMX = ,F10.3/15X,9HTINIT = ,F1 B4510
40.3/) B4520
1095 FORMAT (1H ,4I4,F11.3) B4525
1100 FORMAT (1H ,46X,1P1E10.3) B4530
1110 FORMAT (1H1,5X,25HSTART PUMPING PERIOD NO. ,I2//2X, B4532
1 23HND PARAMETERS REDEFINED/) B4533
END B4540-

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**** TSO FOREGROUND HARDCOPY ****
 DSNAME=U11236C.KONIMOD.CNTL

(ITERAT)

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C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER
C $NOFLOATCALLS
C $STORAGE:2
  SUBROUTINE ITERAT
  CHARACTER*8 TITLE
  REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT
  REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
  REAL*8 DXINV,DYINV,ARINV,PORINV
  REAL*8 HJ
  REAL*8 B,G,W,A,C,E,F,DR,DC,TBAR,TMK,COEF,BLH,BRK,CHK,QL,BRH
  INTEGER FCON
  COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO
  1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N
  2PNCHV,NPDELC,ICLK,FCON,IHEAD,ISOLV
  COMMON /PRMC/ NODEID(20,20),NPCELL(20,20),NPOLD(20,20),LIMBO(500),
  1XOBS(5),IYOBS(5)
  2,NDECAY,NSORB
  COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR
  1,THICK(20,20)
  COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20,
  120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T
  2ITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
  3,HJ(20,20)
  COMMON /BALM/ TOTLQ,TOTLQI,TPIN,TPOUT,TPQR
  COMMON /XINV/ DXINV,DYINV,ARINV,PORINV
  DIMENSION W(20),B(20),G(20)
  *****
  KOUNT=0
  PQIN = 0.0
  PQOUT = 0.0
  PQR = 0.0
  ---COMPUTE ROW AND COLUMN---
  ---CALL NEW ITERATION PARAMETER---
  10 REMN=MOD(KOUNT,NITP)
  IF (REMN.EQ.0) NTH=0
  NTH=NTH+1
  PARAM=AOPT(NTH)
  *****
  ---ROW COMPUTATIONS---
  TEST=0.0
  RHO=S/TIM(N)
  BRK=-RHO
  DO 50 IY=1,NY
  DO 20 M=1,NX
  W(M)=0.0
  B(M)=0.0
  G(M)=0.0
  20 CONTINUE
  DO 30 IX=1,NX
  IF (THCK(IX,IY).EQ.0.0) GO TO 30
  COEF=VPRM(IX,IY)
  QL=-COEF*WT(IX,IY)
  A=TMRX(IX-1,IY,1)*DXINV
  C=TMRX(IX,IY,1)*DXINV
  E=TMRX(IX,IY-1,2)*DYINV
  F=TMRX(IX,IY,2)*DYINV
  TBAR=A+C+E+F
  TMK=TBAR*PARAM
  BLH=-A-C-RHO-COEF-TMK
  IF (A.EQ.0.0.AND.C.EQ.0.0.AND.RHO.EQ.0.0.AND.COEF.EQ.0.0.AND.
  1 TMK.EQ.0.0) GO TO 30
  BRH=E+F-TMK
  
```

```

DR=BRH*HC(IX,IY)+BRK*HK(IX,IY)-E*HC(IX,IY-1)-F*HC(IX,IY+1)+QL+RECH C 490
1(IX,IY)+REC(IX,IY)*ARINV C 500
W(IX)=BLH-A*B(IX-1) C 510
B(IX)=C/W(IX) C 520
G(IX)=(DR-A*G(IX-1))/W(IX) C 530
30 CONTINUE C 540
C C 550
C ---BACK SUBSTITUTION--- C 560
DO 40 J=2,NX C 570
IJ=J-1 C 580
IS=NX-IJ C 590
HR(IS,IY)=G(IS)-B(IS)*HR(IS+1,IY) USNRC
40 IF (W(IS).EQ.O.O) HR(IS,IY) = HC(IS,IY) USNRC
50 CONTINUE C 610
C ***** C 620
C ---COLUMN COMPUTATIONS--- C 630
DO 90 IX=1,NX C 640
DO 60 M=1,NY C 650
W(M)=O.O C 660
B(M)=O.O C 670
60 G(M)=O.O C 680
DO 70 IY=1,NY C 690
IF (THCK(IX,IY).EQ.O.O) GO TO 70 C 700
COEF=VPRM(IX,IY) C 710
QL=-COEF*WT(IX,IY) C 720
A=TMRX(IX,IY-1,2)*DYINV C 730
C=TMRX(IX,IY,2)*DYINV C 740
E=TMRX(IX-1,IY,1)*DXINV C 750
F=TMRX(IX,IY,1)*DXINV C 760
TBAR=A+C+E+F C 770
TMK=TBAR*PARAM C 780
BLH=-A-C-RHO-COEF-TMK C 790
IF (A.EQ.O.O.AND.C.EQ.O.O.AND..RHO.EQ.O.O.AND.COEF.EQ.O.O.AND. USNRC
1 TMK.EQ.O.O) GO TO 70 USNRC
BRH=E+F-TMK C 800
DC=BRH*HR(IX,IY)+BRK*HK(IX,IY)-E*HR(IX-1,IY)-F*HR(IX+1,IY)+QL+RECH C 810
1(IX,IY)+REC(IX,IY)*ARINV C 820
W(IY)=BLH-A*B(IY-1) C 830
B(IY)=C/W(IY) C 840
G(IY)=(DC-A*G(IY-1))/W(IY) C 850
70 CONTINUE C 860
C C 870
C ---BACK SUBSTITUTION--- C 880
DO 80 J=2,NY C 890
IJ=J-1 C 900
IB=NY-IJ C 910
HC(IX,IB)=G(IB)-B(IB)*HC(IX,IB+1) C 920
IF (W(IB).EQ.O.O) HC(IX,IB) = HR(IX,IB) USNRC
IF (THCK(IX,IB).EQ.O.O) GO TO 80 C 930
CHK=DABS(HC(IX,IB)-HR(IX,IB)) C 940
IF (CHK.GT.TOL) TEST=1.O C 950
80 CONTINUE C 960
90 CONTINUE C 970
C ***** C 980
KOUNT=KOUNT+1 C 990
IF (TEST.EQ.O.O) GO TO 120 C1000
IF (KOUNT.GE.ITMAX) GO TO 100 C1010
GO TO 10 C1020
C ***** C1030
C ---TERMINATE PROGRAM -- ITMAX EXCEEDED--- C1040
100 WRITE (6,160) C1050
DO 110 IX=1,NX C1060
DO 110 IY=1,NY C1070
110 HK(IX,IY)=HC(IX,IY) C1080
CALL OUTPT C1090
STOP C1100

```

C	*****	C1110
C	---SET NEW HEAD (HK)---	C1120
120	DO 130 IY=1,NY	C1130
	DO 130 IX=1,NX	C1140
	IF (THCK(IX,IY).EQ.O.O) GO TO 130	C1150
	HR(IX,IY)=HK(IX,IY)	C1160
	HK(IX,IY)=HC(IX,IY)	C1170
C		C1180
C	---CUMULATIVE PUMPAGE AND RECHARGE FOR MASS BALANCE---	C1181
	IF (REC(IX,IY).GT.O.O) GO TO 32	C1182
	PQIN = PQIN + REC(IX,IY)	C1183
	GO TO 34	C1184
	32 PQOUT = PQOUT + REC(IX,IY)	C1185
	34 IF (RECH(IX,IY).GT.O.O) GO TO 36	C1186
	PQR = PQR + RECH(IX,IY)*AREA	C1187A
	GO TO 38	C1188
	36 PQOUT = PQOUT + RECH(IX,IY)*AREA	C1189
C	---COMPUTE LEAKAGE FOR MASS BALANCE---	C1190
	38 IF (VPRM(IX,IY).EQ.O.O) GO TO 130	C1201
	DELQ=-VPRM(IX,IY)*AREA*(WT(IX,IY)-HK(IX,IY))	C1211
	IF (DELQ.LE.O.O) GO TO 125	C1216
	TOTLQ=TOTLQ+DELQ*TIM(N)	C1220
	GO TO 130	C1222
	125 TOTLQI=TOTLQI+DELQ*TIM(N)	C1224
	130 CONTINUE	C1230
	TPIN = TPIN + PQIN*TIM(N)	C1232
	TPQR = TPQR + PQR*TIM(N)	C1232A
	TPOUT = TPOUT + PQOUT*TIM(N)	C1233
C		C1240
	WRITE (6,140) N	C1250
	WRITE (6,150) KOUNT	C1260
C	*****	C1270
	RETURN	C1280
C	*****	C1290
C		C1300
C		C1310
C		C1320
	140 FORMAT (1H0//3X,4HN = ,1I4)	C1330
	150 FORMAT (1H ,2X,23HNUMBER OF ITERATIONS = ,1I4)	C1340
	160 FORMAT (1H0,5X,64H*** EXECUTION TERMINATED -- MAX. NO. ITERATION	C1350
	1S EXCEEDED ***/26X,21HFINAL OUTPUT FOLLOWS:)	C1360
	END	C1370-

**** TSO FOREGROUND HARDCOPY ****
DSNAME=U11236C.KONIMOD.CNTL

(GENPT)

```
C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER
C $NOFLOATCALLS
C $STORAGE:2
SUBROUTINE GENPT D 10
CHARACTER*8 TITLE D 11
REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT D 20
REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR D 30
REAL*8 HJ D 34
INTEGER PTID D 35
INTEGER FCON D 36
COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO D 40
1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N D 50
2PNCHV,NPDEL,ICLK,FCON,IHEAD,ISOLV D 62
COMMON /PRMC/ NODEID(20,20),NPCELL(20,20),NPOLD(20,20),LIMBO(500), D 65
1IXOBS(5),IYOBS(5) D 66
2,NDECAY,NSORB USNRC
COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR D 90
1,THICK(20,20) D 91
COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20, D 100
120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T D 110
2ITITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR D 120
3,HJ(20,20) D 125
COMMON /CHMA/ PART(3,3200),CONC(20,20),TMCN(5,50),VX(20,20),VY(20, D 130
120),CONINT(20,20),CNRECH(20,20),POROS,SUMTCH,BETA,TIMV,STORM,STORM D 140
2I,CMSIN,CMSOUT,FLMIN,FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM D 150
3,DCYLAM,BLKDEN,SRBRAT,SRBSAT,SRBALF,VOLDCY,VOLSRB,SRBDCY USNRC
COMMON /CHMP/ PTID(3200) D 155
DIMENSION RP(8),RN(8),IPT(8) D 160
***** D 170
C F1=0.30 D 180
F2=1.0/3.0 D 190
IF (NPTPND.EQ.4) F1=0.25 D 200
IF (NPTPND.EQ.9) F1=1.0/3.0 D 210
IF (NPTPND.EQ.8) F2=0.25 D 220
NCHK=NPTPND D 230
IF (NPTPND.EQ.5.OR.NPTPND.EQ.9) NCHK=NPTPND-1 D 240
IF (TEST.GT.98.) GO TO 10 D 250
***** D 260
C ---INITIALIZE VALUES--- D 270
STORM=0.0 D 280
CMSIN=0.0 D 290
CMSOUT=0.0 D 300
FLMIN=0.0 D 310
FLMOT=0.0 D 320
SUMIO=0.0 D 330
***** D 340
C 10 DO 20 IN=1,NPMAX D 345
PTID(IN)=0 D 355
DO 20 ID=1,3 D 365
20 PART(ID,IN)=0.0 D 370
DO 30 IA=1,8 D 380
RP(IA)=0.0 D 390
RN(IA)=0.0 D 400
30 IPT(IA)=0 D 410
C ---SET UP LIMBO ARRAY--- D 420
DO 40 IN=1,500 D 430
40 LIMBO(IN)=0.0 D 440
IND=1 D 450
DO 50 IL=1,500,2 D 460
LIMBO(IL)=IND D 470
50 IND=IND+1 D 480
***** D 490
C
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C	--- <td>D 500</td>	D 500
	DO 410 IX=1,NX	D 510
	DO 410 IY=1,NY	D 520
	IF (THCK(IX,IY).EQ.O.O) GO TO 410	D 530
	KR=O	D 540
	TEST2=O.O	D 550
	METH=1	D 560
	NPCELL(IX,IY)=O	D 570
	NPOLD(IX,IY)=NPTPND	D 575
	C1=CONC(IX,IY)	D 580
	IF (C1.LE.1.OE-05) TEST2=1.O	D 590
	IF (VPRM(IX,IY).GT.O.O9) TEST2=1.O	D 600
	IF (REC(IX,IY).NE.O.O) TEST2=1.O	D 610
	IF (THCK(IX+1,IY+1).EQ.O.O.OR.THCK(IX+1,IY-1).EQ.O.O.OR.THCK(IX-1,	D 620
	1IY+1).EQ.O.O.OR.THCK(IX-1,IY-1).EQ.O.O) TEST2=1.O	D 630
	IF ((THCK(IX,IY+1).EQ.O.O.OR.THCK(IX,IY-1).EQ.O.O.OR.THCK(IX+1,IY)	D 640
	1.EQ.O.O.OR.THCK(IX-1,IY).EQ.O.O).AND.NPTPND.GT.5) TEST2=1.O	D 650
	CNODE=C1*(1.O-F1)	D 660
	IF (TEST.LT.98.O.OR.TEST2.GT.O.O) GO TO 70	D 670
	SUMC=CONC(IX+1,IY)+CONC(IX-1,IY)+CONC(IX,IY+1)+CONC(IX,IY-1)	D 680
	IF (NCHK.EQ.4) GO TO 60	D 690
	SUMC=SUMC+CONC(IX+1,IY+1)+CONC(IX+1,IY-1)+CONC(IX-1,IY+1)+CONC(IX-	D 700
	11,IY-1)	D 710
	60 AVC=SUMC/NCHK	D 720
	IF (AVC.GT.C1) METH=2	D 730
C		D 740
C	--- <td>D 750</td>	D 750
	70 DO 140 IT=1,2	D 760
	EVET=(-1.O)**IT	D 770
	DO 140 IS=1,2	D 780
	EVES=(-1.O)**IS	D 790
	PART(1,IND)=IX+F1*EVET	D 800
	PART(2,IND)=IY+F1*EVES	D 810
	PART(2,IND)=-PART(2,IND)	D 820
	PART(3,IND)=C1	D 830
	KR=KR+1	D 832
	PTID(IND)=KR	D 834
	IF (TEST.LT.98.O.OR.TEST2.GT.O.O) GO TO 130	D 840
	IXD=IX+EVET	D 850
	IYD=IY+EVES	D 860
	IPT(KR)=IND	D 880
	IF (METH.EQ.2) GO TO 80	D 890
	PART(3,IND)=CNODE+CONC(IXD,IYD)*F1	D 900
	GO TO 90	D 910
	80 PART(3,IND)=2.O*C1*CONC(IXD,IYD)/(C1+CONC(IXD,IYD))	D 920
	90 IF (C1-CONC(IXD,IYD)) 100,110,120	D 930
	100 RP(KR)=CONC(IXD,IYD)-PART(3,IND)	D 940
	RN(KR)=C1-PART(3,IND)	D 950
	GO TO 130	D 960
	110 RP(KR)=O.O	D 970
	RN(KR)=O.O	D 980
	GO TO 130	D 990
	120 RP(KR)=C1-PART(3,IND)	D1000
	RN(KR)=CONC(IXD,IYD)-PART(3,IND)	D1010
	130 IND=IND+1	D1020
	140 CONTINUE	D1030
C		D1040
	IF (NPTPND.EQ.5.OR.NPTPND.EQ.9) GO TO 150	D1050
	GO TO 160	D1060
C	--- <td>D1070</td>	D1070
	150 PART(1,IND)=IX	D1075
	PART(2,IND)=-IY	D1090
	PART(3,IND)=C1	D1100
	PTID(IND)=5	D1105
	IND=IND+1	D1110
C	--- <td>D1120</td>	D1120

160	IF (NPTPND.LT.8) GO TO 290	D1130
	CNODE=C1*(1.0-F2)	D1140
	DO 280 IT=1,2	D1150
	EVET=(-1.0)**IT	D1160
	PART(1,IND)=IX+F2*EVET	D1170
	PART(2,IND)=-IY	D1180
	PART(3,IND)=C1	D1190
	IF (EVET.LT.0) PTID(IND)=6	D1192
	IF (EVET.GT.0) PTID(IND)=8	D1194
	IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 220	D1200
	IXD=IX+EVET	D1210
	KR=KR+1	D1220
	IPT(KR)=IND	D1230
	IF (METH.EQ.2) GO TO 170	D1240
	PART(3,IND)=CNODE+CONC(IXD,IY)*F2	D1250
	GO TO 180	D1260
170	PART(3,IND)=2.0*C1*CONC(IXD,IY)/(C1+CONC(IXD,IY))	D1270
180	IF (C1-CONC(IXD,IY)) 190,200,210	D1280
190	RP(KR)=CONC(IXD,IY)-PART(3,IND)	D1290
	RN(KR)=C1-PART(3,IND)	D1300
	GO TO 220	D1310
200	RP(KR)=0.0	D1320
	RN(KR)=0.0	D1330
	GO TO 220	D1340
210	RP(KR)=C1-PART(3,IND)	D1350
	RN(KR)=CONC(IXD,IY)-PART(3,IND)	D1360
	PART(1,IND)=IX	D1380
220	IND=IND+1	D1370
	PART(2,IND)=IY+F2*EVET	D1390
	PART(2,IND)=-PART(2,IND)	D1400
	PART(3,IND)=C1	D1410
	IF (EVET.LT.0) PTID(IND)=7	D1412
	IF (EVET.GT.0) PTID(IND)=9	D1414
	IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 280	D1420
	IYD=IY+EVET	D1430
	KR=KR+1	D1440
	IPT(KR)=IND	D1450
	IF (METH.EQ.2) GO TO 230	D1460
	PART(3,IND)=CNODE+CONC(IX,IYD)*F2	D1470
	GO TO 240	D1480
230	PART(3,IND)=2.0*C1*CONC(IX,IYD)/(C1+CONC(IX,IYD))	D1490
240	IF (C1-CONC(IX,IYD)) 250,260,270	D1500
250	RP(KR)=CONC(IX,IYD)-PART(3,IND)	D1510
	RN(KR)=C1-PART(3,IND)	D1520
	GO TO 280	D1530
260	RP(KR)=0.0	D1540
	RN(KR)=0.0	D1550
	GO TO 280	D1560
270	RP(KR)=C1-PART(3,IND)	D1570
	RN(KR)=CONC(IX,IYD)-PART(3,IND)	D1580
280	IND=IND+1	D1590
C		D1600
290	IF (TEST.LT.98.0.OR.TEST2.GT.0.0) GO TO 410	D1610
	SUMPT=0.0	D1620
C	---COMPUTE CONC. GRADIENT WITHIN CELL---	D1630
	DO 300 KPT=1,NCHK	D1640
	IK=IPT(KPT)	D1650
300	SUMPT=PART(3,IK)+SUMPT	D1660
	CBAR=SUMPT/NCHK	D1670
C	---CHECK MASS BALANCE WITHIN CELL AND ADJUST PT. CONCS.---	D1680
	SUMPT=0.0	D1690
	IF (CBAR-C1) 310,410,330	D1700
310	CRCT=1.0-(CBAR/C1)	D1710
	IF (METH.EQ.1) CRCT=CBAR/C1	D1720
	DO 320 KPT=1,NCHK	D1730
	IK=IPT(KPT)	D1740

	PART(3,IK)=PART(3,IK)+RP(KPT)*CRCT	D1750
320	SUMPT=SUMPT+PART(3,IK)	D1760
	CBARN=SUMPT/NCHK	D1770
	GO TO 350	D1780
330	CRCT=1.0-(C1/CBAR)	D1790
	IF (METH.EQ.1) CRCT=C1/CBAR	D1800
	DO 340 KPT=1,NCHK	D1810
	IK=IPT(KPT)	D1820
	PART(3,IK)=PART(3,IK)+RN(KPT)*CRCT	D1830
340	SUMPT=SUMPT+PART(3,IK)	D1840
	CBARN=SUMPT/NCHK	D1850
350	IF (CBARN.EQ.C1) GO TO 410	D1860
C	---CORRECT FOR OVERCOMPENSATION---	D1870
	CRCT=C1/CBARN	D1880
	DO 380 KPT=1,NCHK	D1890
	IK=IPT(KPT)	D1900
	PART(3,IK)=PART(3,IK)*CRCT	D1910
C	---CHECK CONSTRAINTS---	D1920
	IF (PART(3,IK)-C1) 360,380,370	D1930
360	CLIM=C1-RP(KPT)+RN(KPT)	D1940
	IF (PART(3,IK).LT.CLIM) GO TO 390	D1950
	GO TO 380	D1960
370	CLIM=C1+RP(KPT)-RN(KPT)	D1970
	IF (PART(3,IK).GT.CLIM) GO TO 390	D1980
380	CONTINUE	D1990
	GO TO 410	D2000
390	TEST2=1.0	D2010
	DO 400 KPT=1,NCHK	D2020
	IK=IPT(KPT)	D2030
400	PART(3,IK)=C1	D2040
410	CONTINUE	D2050
	NP=IND	D2060
	IF (INT.EQ.0) CALL CHMOT	D2070
C	*****	D2080
	RETURN	D2090
C	*****	D2100
	END	D2110-

**** TSO FOREGROUND HARDCOPY ****
DSNAME=U11236C.KONIMOD.CNTL

(VELO)

```
C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER
C $NOFLOATCALLS
C $STORAGE:2
  SUBROUTINE VELO E 10
  CHARACTER*8 TITLE E 11
  REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT E 30
  REAL*8 DXINV,DYINV,ARINV,PORINV E 35
  REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR E 40
  REAL*8 RATE,SLEAK,DIV E 50
  REAL*8 HJ E 55
  INTEGER FCON E 56
  COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO E 60
  1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N E 70
  2PNCHV,NPDEL,ICLK,FCON,IHEAD,ISOLV E 82
  COMMON /PRMC/ NODEID(20,20),NPCELL(20,20),NPOLD(20,20),LIMBO(500), E 85
  1IXOBS(5),IYOBS(5) E 86
  2,NDECAY,NSORB USNRC
  COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR E 110
  1,THICK(20,20) E 111
  COMMON /HEDE/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20, E 120
  120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T E 130
  2ITITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR E 140
  3,HJ(20,20) E 145
  COMMON /XINV/ DXINV,DYINV,ARINV,PORINV E 150
  COMMON /CHMA/ PART(3,3200),CONC(20,20),TMCN(5,50),VX(20,20),VY(20, E 160
  120),CONINT(20,20),CNRECH(20,20),POROS,SUMTCH,BETA,TIMV,STORM,STORM E 170
  2I,CMSIN,CMSOUT,FLMIN,FLMOT,SUMID,CELDIS,DLTRAT,CSTORM E 180
  3,DCYLAM,BLKDEN,SRBRAT,SRBSAT,SRBALF,VOLDCY,VOLSRB,SRBDCY USNRC
  COMMON /CHMC/ SUMC(20,20),VXBDY(20,20),VYBDY(20,20) E 190
  COMMON /DIFUS/ DISP(20,20,4) E 200
C ***** E 210
C ---COMPUTE VELOCITIES AND STORE--- E 220
  VMAX=1.OE-10 E 230
  VMAY=1.OE-10 E 240
  VMXBD=1.OE-10 E 250
  VMYBD=1.OE-10 E 260
  TMV = 1.OE5*TIM(N) E 275
  LIM=0 E 280
  MAXX = 0 E 284
  MAXY = 0 E 285
C E 290
  DO 20 IX=1,NX E 300
  DO 20 IY=1,NY E 310
  DO 10 IZ=1,4 E 320
  10 DISP(IX,IY,IZ)=0.0 E 330
C E 340
  IF (THCK(IX,IY).EQ.0.0) GO TO 20 E 350
  DIST = 0.0 USNRC
  IF (NSORB.LT.1) GO TO 6 USNRC
  IF (NSORB.GT.1) GO TO 3 USNRC
C*** *****LINEAR SORBTION***** USNRC
  DIST = SRBRAT*BLKDEN USNRC
  GO TO 6 USNRC
  3 IF (NSORB.GT.2) GO TO 4 USNRC
C*** *****LANGMUIR SORBTION***** USNRC
  DIST = BLKDEN*SRBRAT*SRBSAT/(1.0+SRBRAT*CONC(IX,IY))**2.0 USNRC
  GO TO 6 USNRC
  4 IF (SRBALF.EQ.0.0) GO TO 6 USNRC
C*** *****FREUNDLICH SORBTION***** USNRC
  LOGCON = -23.0 USNRC
  IF (CONC(IX,IY).GT.1.OE-10) LOGCON = ALOG(CONC(IX,IY)) USNRC
  5 SRBEXP = (SRBALF-1.0)*LOGCON USNRC
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IF (SRBEXP.GT.23.0) SRBEXP = 23.0
DIST = BLKDEN*SRBALF*SRBRAT*EXP(SRBEXP)
6 RETARD = 1.0/(1.0+DIST)
RATE=REC(IX,IY)/AREA
SLEAK=(HK(IX,IY)-WT(IX,IY))*VPRM(IX,IY)
DIV=RATE+SLEAK+RECH(IX,IY)
C
C      ---VELOCITIES AT NODES---
C      ---X-DIRECTION---
DHX=HK(IX-1,IY)-HK(IX+1,IY)
IF (THCK(IX-1,IY).EQ.0.0) DHX=HK(IX,IY)-HK(IX+1,IY)
IF (THCK(IX+1,IY).EQ.0.0) DHX=HK(IX-1,IY)-HK(IX,IY)
IF (THCK(IX-1,IY).EQ.0.0.AND.THCK(IX+1,IY).EQ.0.0) DHX=0.0
GRDX=DHX*DXINV*0.50
VX(IX,IY)=PERM(IX,IY)*GRDX*PORINV
1
1      *RETARD
ABVX=ABS(VX(IX,IY))
IF (ABVX.GT.VMAX) VMAX=ABVX
C
C      ---Y-DIRECTION---
DHY=HK(IX,IY-1)-HK(IX,IY+1)
IF (THCK(IX,IY-1).EQ.0.0) DHY=HK(IX,IY)-HK(IX,IY+1)
IF (THCK(IX,IY+1).EQ.0.0) DHY=HK(IX,IY-1)-HK(IX,IY)
IF (THCK(IX,IY-1).EQ.0.0.AND.THCK(IX,IY+1).EQ.0.0) DHY=0.0
GRDY=DHY*DYINV*0.50
VY(IX,IY)=PERM(IX,IY)*GRDY*PORINV*ANFCTR
1
1      *RETARD
ABVY=ABS(VY(IX,IY))
IF (ABVY.GT.VMAY) VMAY=ABVY
C
C      ---VELOCITIES AT CELL BOUNDARIES---
GRDX=(HK(IX,IY)-HK(IX+1,IY))*DXINV
PERMX=2.0*PERM(IX,IY)*PERM(IX+1,IY)/((PERM(IX,IY)+PERM(IX+1,IY)))
VXBDY(IX,IY)=PERMX*GRDX*PORINV
1
1      *RETARD
GRDY=(HK(IX,IY)-HK(IX,IY+1))*DYINV
PERMY=2.0*PERM(IX,IY)*PERM(IX,IY+1)/((PERM(IX,IY)+PERM(IX,IY+1)))
VYBDY(IX,IY)=PERMY*GRDY*PORINV*ANFCTR
1
1      *RETARD
ABVX=ABS(VXBDY(IX,IY))
ABVY=ABS(VYBDY(IX,IY))
IF (ABVX.GT.VMXBD) VMXBD=ABVX
IF (ABVY.GT.VMYBD) VMYBD=ABVY
C
C
IF (DIV.GE.0.0) GO TO 20
TDIV=(PORDS*THCK(IX,IY))/DABS(DIV)
IF (TDIV.GE.TMV) GO TO 20
TMV = TDIV
MAXX = IX
MAXY = IY
20 CONTINUE
C
C      *****
C      ---PRINT VELOCITIES---
IF (NPNTVL.EQ.0) GO TO 80
IF (NPNTVL.EQ.2) GO TO 30
IF (NPNTVL.EQ.1.AND.N.EQ.1) GO TO 30
GO TO 80
30 WRITE (6,320)
WRITE (6,330)
DO 40 IY=1,NY
40 WRITE (6,350) (VX(IX,IY),IX=1,NX)
WRITE (6,340)
DO 50 IY=1,NY
50 WRITE (6,350) (VXBDY(IX,IY),IX=1,NX)
WRITE (6,360)
WRITE (6,330)
DO 60 IY=1,NY

```

```

USNRC
USNRC
USNRC
E 360
E 370
E 380
E 390
E 400
E 410
E 421
E 431
E 441
E 451
E 455
E 460
USNRC
E 470
E 480
E 490
E 501
E 511
E 521
E 531
E 535
E 540
USNRC
E 550
E 560
E 570
E 580
E 590
E 600
E 610
USNRC
E 620
E 630
E 640
USNRC
E 650
E 660
E 670
E 680
E 690
E 700
E 710
E 722
E 724
E 725
E 726
E 730
E 740
E 750
E 760
E 770
E 780
E 790
E 800
E 810
E 820
E 830
E 840
E 850
E 860
E 870
E 880
E 890

```

60	WRITE (6,350) (VY(IX,IY),IX=1,NX)	E 900
	WRITE (6,340)	E 910
	DO 70 IY=1,NY	E 920
70	WRITE (6,350) (VYBDY(IX,IY),IX=1,NX)	E 930
C	---PUNCH VELOCITIES---	E 940
80	IF (NPNCHV.EQ.0) GO TO 110	E 950
	IF (NPNCHV.EQ.2) GO TO 90	E 960
	IF (NPNCHV.EQ.1.AND.N.EQ.1) GO TO 90	E 970
	GO TO 110	E 980
90	WRITE (7,510) NX,NY,XDEL,YDEL,VMAX,VMAY	E 990
	DO 100 IY=1,NY	E1000
	WRITE (7,520) (VX(IX,IY),IX=1,NX)	E1010
100	WRITE (7,520) (VY(IX,IY),IX=1,NX)	E1020
C	*****	E1030
C	---COMPUTE NEXT TIME STEP---	E1040
110	WRITE (6,390)	E1050
	WRITE (6,400) VMAX,VMAY	E1060
	WRITE (6,410) VMXBD,VMYBD	E1070
	TDELX=CELDIS*XDEL/VMAX	E1080
	TDELY=CELDIS*YDEL/VMAY	E1090
	TDELXB=CELDIS*XDEL/VMXBD	E1100
	TDELYB=CELDIS*YDEL/VMYBD	E1110
	TIMV=AMIN1(TDELX,TDELY,TDELXB,TDELYB)	E1120
	IF (AMAX1(VMAX,VMAY,VMXBD,VMYBD).LE.1.OE-10) WRITE(6,570)	E1125
	WRITE (6,310) TMV,TIMV	E1130
	IF (TMV.LT.TIMV) GO TO 120	E1140
	LIM=-1	E1150
	GO TO 130	E1160
120	TIMV=TMV	E1170
	LIM=1	E1180
130	NTIMV=TIM(N)/TIMV	E1190
	NMOV=NTIMV+1	E1200
	WRITE (6,420) TIMV,NTIMV,NMOV	E1210
	TIMV=TIM(N)/NMOV	E1220
	WRITE (6,370) TIM(N)	E1230
	WRITE (6,380) TIMV	E1240
C		E1250
	IF (BETA.EQ.0.0) GO TO 200	E1260
C	*****	E1270
C	---COMPUTE DISPERSION COEFFICIENTS---	E1280
	ALPHA=BETA	E1290
	ALNG=ALPHA	E1300
	TRAN=DLTRAT*ALPHA	E1310
	XX2=XDEL*XDEL	E1320
	YY2=YDEL*YDEL	E1330
	XY2=4.0*XDEL*YDEL	E1340
	DO 150 IX=2,NNX	E1350
	DO 150 IY=2,NNY	E1360
	IF (THCK(IX,IY).EQ.0.0) GO TO 150	E1370
	VXE=VXBDY(IX,IY)	E1380
	VYS=VYBDY(IX,IY)	E1390
	IF (THCK(IX+1,IY).EQ.0.0) GO TO 140	E1400
C	---FORWARD COEFFICIENTS: X-DIRECTION---	E1410
	VYE=(VYBDY(IX,IY-1)+VYBDY(IX+1,IY-1)+VYS+VYBDY(IX+1,IY))/4.0	E1420
	VXE2=VXE*VXE	E1430
	VYE2=VYE*VYE	E1440
	VMGE=SQRT(VXE2+VYE2)	E1450
	IF (VMGE.LT.1.OE-20) GO TO 140	E1460
	DALN=ALNG*VMGE	E1470
	DTRN=TRAN*VMGE	E1480
	VMGE2=VMGE*VMGE	E1490
C	---XX COEFFICIENT---	E1500
	DISP(IX,IY,1)=(DALN*VXE2+DTRN*VYE2)/(VMGE2*XX2)	E1510
C	---XY COEFFICIENT---	E1520
	DISP(IX,IY,3)=(DALN-DTRN)*VXE*VYE/(VMGE2*XY2)	E1530
C	---FORWARD COEFFICIENTS: Y-DIRECTION---	E1540

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140 IF (THCK(IX,IY+1).EQ.O.O) GO TO 150 E1550
VXS=(VXBDY(IX-1,IY)+VXE+VXBDY(IX-1,IY+1)+VXBDY(IX,IY+1))/4.O E1560
VYS2=VYS*VYS E1570
VXS2=VXS*VXS E1580
VMGS=SQRT(VXS2+VYS2) E1590
IF (VMGS.LT.1.OE-20) GO TO 150 E1600
DALN=ALNG*VMGS E1610
DTRN=TRAN*VMGS E1620
VMGS2=VMGS*VMGS E1630
C ---YY COEFFICIENT--- E1640
DISP(IX,IY,2)=(DALN*VYS2+DTRN*VXS2)/(VMGS2*YY2) E1650
C ---YX COEFFICIENT--- E1660
DISP(IX,IY,4)=(DALN-DTRN)*VXS*VYS/(VMGS2*XY2) E1670
150 CONTINUE E1680
C ***** E1690
C ---ADJUST CROSS-PRODUCT TERMS FOR ZERO THICKNESS--- E1700
DO 160 IX=2,NNX E1710
DO 160 IY=2,NNY E1720
IF (THCK(IX,IY+1).EQ.O.O.OR.THCK(IX+1,IY+1).EQ.O.O.OR.THCK(IX,IY-1 E1730
).EQ.O.O.OR.THCK(IX+1,IY-1).EQ.O.O) DISP(IX,IY,3)=O.O E1740
IF (THCK(IX+1,IY).EQ.O.O.OR.THCK(IX+1,IY+1).EQ.O.O.OR.THCK(IX-1,IY E1750
).EQ.O.O.OR.THCK(IX-1,IY+1).EQ.O.O) DISP(IX,IY,4)=O.O E1760
160 CONTINUE E1770
C ***** E1780
C ---CHECK FOR STABILITY OF EXPLICIT METHOD--- E1790
TIMDIS=O.O E1800
DO 170 IX=2,NNX E1810
DO 170 IY=2,NNY E1820
TDCO=DISP(IX,IY,1)+DISP(IX,IY,2) E1830
170 IF (TDCO.GT.TIMDIS) TIMDIS=TDCO E1840
TIMDC=O.5/TIMDIS E1850
WRITE (6,440) TIMDC E1860
NTIMD=TIM(N)/TIMDC E1870
NDISP=NTIMD+1 E1880
IF (NDISP.LE.NMOV) GO TO 180 E1890
NMOV=NDISP E1900
TIMV=TIM(N)/NMOV E1910
LIM=O E1920
180 WRITE (6,430) TIMV,NTIMD,NMOV E1930
C ***** E1940
C ---ADJUST DISP. EQUATION COEFFICIENTS FOR SATURATED THICKNESS--- E1950
DO 190 IX=2,NNX E1960
DO 190 IY=2,NNY E1970
IF (THCK(IX,IY).EQ.O.O) GO TO 190 E1972
BAVX=2.O*THCK(IX,IY)*THCK(IX+1,IY)/(THCK(IX,IY)+THCK(IX+1,IY)) E1974
BAVY=2.O*THCK(IX,IY)*THCK(IX,IY+1)/(THCK(IX,IY)+THCK(IX,IY+1)) E1976
DISP(IX,IY,1)=DISP(IX,IY,1)*BAVX E2000
DISP(IX,IY,2)=DISP(IX,IY,2)*BAVY E2010
DISP(IX,IY,3)=DISP(IX,IY,3)*BAVX E2020
DISP(IX,IY,4)=DISP(IX,IY,4)*BAVY E2032
190 CONTINUE E2034
C ***** E2040
200 IF (NMOV.LT.2) GO TO 235 E2052
IF (LIM) 210,220,230 E2054
210 WRITE (6,530) E2060
GO TO 240 E2070
220 WRITE (6,540) E2080
GO TO 240 E2090
230 WRITE (6,550) E2100
WRITE (6,560) MAXX,MAXY E2102
GO TO 240 E2104
235 WRITE (6,580) E2106
C ***** E2110
C ---PRINT DISPERSION EQUATION COEFFICIENTS--- E2120
240 IF (NPNTD.EQ.O) GO TO 300 E2130
IF (NPNTD.EQ.2) GO TO 250 E2140

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IF (NPNTD.EQ.1.AND.N.EQ.1) GO TO 250
GO TO 300
250 WRITE (6,450)
WRITE (6,460)
DO 260 IY=1,NY
260 WRITE (6,500) (DISP(IX,IY,1),IX=1,NX)
WRITE (6,470)
DO 270 IY=1,NY
270 WRITE (6,500) (DISP(IX,IY,2),IX=1,NX)
WRITE (6,480)
DO 280 IY=1,NY
280 WRITE (6,500) (DISP(IX,IY,3),IX=1,NX)
WRITE (6,490)
DO 290 IY=1,NY
290 WRITE (6,500) (DISP(IX,IY,4),IX=1,NX)
*****
C 300 RETURN
*****
C
C
C
310 FORMAT (1H ,19H TMV (MAX. INJ.) = ,G12.5/20H TIMV (CELDIS) = ,
11P1E12.5)
320 FORMAT (1H1,12HX VELOCITIES)
330 FORMAT (1H ,25X,8HAT NODES/)
340 FORMAT (1H0,25X,13HON BOUNDARIES/)
350 FORMAT (1H ,1P10E12.3)
360 FORMAT (1H1,12HY VELOCITIES)
370 FORMAT (3H ,11HTIM (N) = ,1P1E12.5)
380 FORMAT (3H ,11HTIMEVELO = ,1P1E12.5)
390 FORMAT (1H1,10X,29HSTABILITY CRITERIA --- M.O.C.//)
400 FORMAT (1H0,8H VMAX = ,1P1E9.2,5X,7HVMAX = ,1P1E9.2)
410 FORMAT (1H ,8H VMXBD= ,1P1E9.2,5X,7HVMBD= ,1P1E9.2)
420 FORMAT (1H0,8H TIMV = ,1P1E9.2,5X,8HNTIMV = ,I5,5X,7HNMOV = ,I5/)
430 FORMAT (1H0,8H TIMV = ,1P1E9.2,5X,8HNTIMD = ,I5,5X,7HNMOV = ,I5)
440 FORMAT (3H ,11HTIMEDISP = ,1P1E12.5)
450 FORMAT (1H1,32HDISPERSION EQUATION COEFFICIENTS,10X,25H=(D-IJ)*(B)
1/(GRID FACTOR))
460 FORMAT (1H ,35X,14HXX COEFFICIENT/)
470 FORMAT (1H ,35X,14HYY COEFFICIENT/)
480 FORMAT (1H ,35X,14HXY COEFFICIENT/)
490 FORMAT (1H ,35X,14HYX COEFFICIENT/)
500 FORMAT (1H ,1P10E8.1)
510 FORMAT (2I4,2F10.1,2F10.7)
520 FORMAT (8F10.7)
530 FORMAT (1H0,10X,42HTHE LIMITING STABILITY CRITERION IS CELDIS)
540 FORMAT (1H0,10X,40HTHE LIMITING STABILITY CRITERION IS BETA)
550 FORMAT (1H0,10X,58HTHE LIMITING STABILITY CRITERION IS MAXIMUM INJ
ECTION RATE)
560 FORMAT (1H ,15X,35H MAX. INJECTION OCCURS IN CELL IX = ,I3,6H IY =
1
,I3)
570 FORMAT (1H0,5X,47H*** WARNING *** DECREASE CRITERIA IN E 230-260)
580 FORMAT (1H0,10X,63H*TIME INCREMENT FOR SOLUTE TRANSPORT EQUALS TIM
1E STEP FOR FLOW*)
END
E2150
E2160
E2170
E2180
E2190
E2200
E2210
E2220
E2230
E2240
E2250
E2260
E2270
E2280
E2290
E2300
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E2500
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E2570
E2580
E2590
E2600
E2610
E2620
E2630
E2635
E2636
E2637
E2638
E2639
E2640-

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**** TSO FOREGROUND HARDCOPY ****
DSNAME=U11236C.KONIMOD.CNTL

(MOVE)

C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER
C \$NOFLOATCALLS
C \$STORAGE:2

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SUBROUTINE MOVE
CHARACTER*8 TITLE
REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT
REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
REAL*8 DXINV,DYINV,ARINV,PORINV
REAL*8 HJ
INTEGER PTID
INTEGER FCON
COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO
1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N
2PNCHV,NPDELC,ICLK,FCON,IHEAD,ISOLV
COMMON /PRMC/ NODEID(20,20),NPCELL(20,20),NPOLD(20,20),LIMBO(500),
1IXOBS(5),IYOBS(5)
2,NDECAY,NSORB
COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR
1,THICK(20,20)
COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20,
120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T
2TITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
3,HJ(20,20)
COMMON /XINV/ DXINV,DYINV,ARINV,PORINV
COMMON /CHMA/ PART(3,3200),CONC(20,20),TMCN(5,50),VX(20,20),VY(20,
120),CONINT(20,20),CNRECH(20,20),POROS,SUMTCH,BETA,TIMV,STORM,STORM
2I,CMSIN,CMSOUT,FLMIN,FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM
3,DCYLAM,BLKDEN,SRBRAT,SRBSAT,SRBALF,VOLDCY,VOLSRB,SRBDCY
COMMON /CHMC/ SUMC(20,20),VXBDY(20,20),VYBDY(20,20)
COMMON /CHMP/ PTID(3200)
*****
C WRITE (6,680) NMOV
SUMTCH=SUMT-TIM(N)
F1=0.30
F2=1.0/3.0
IF (NPTPND.EQ.4) F1=0.25
IF (NPTPND.EQ.9) F1=F2
IF (NPTPND.EQ.8) F2=0.25
CONST1=TIMV*DXINV
CONST2=TIMV*DYINV
C ---MOVE PARTICLES "NMOV" TIMES---
DO 650 IMOV=1,NMOV
10 NPTM=NP
C ---MOVE EACH PARTICLE---
DO 590 IN=1,NP
IF (PART(1,IN).EQ.0.0) GO TO 590
KFLAG=0
*****
C ---COMPUTE OLD LOCATION---
20 XOLD=PART(1,IN)
IX=XOLD+0.5
IFLAG=1
IF (PART(2,IN).GE.0.0) GO TO 30
IFLAG=-1
PART(2,IN)=-PART(2,IN)
30 YOLD=PART(2,IN)
IY=YOLD+0.5
IF (THCK(IX,IY).EQ.0.0) GO TO 590
*****
C ---COMPUTE NEW LOCATION AND LOCATE CLOSEST NODE---
C ---LOCATE NORTHWEST CORNER---
IVX=XOLD
```

	IVY=YOLD	F 530
	IXE=IVX+1	F 540
	IYS=IVY+1	F 550
C	*****	F 560
C	---LOCATE QUADRANT, VEL. AT 4 CORNERS, CHECK FOR BOUNDARIES---	F 570
	CELDX=XOLD-IX	F 580
	CELDY=YOLD-IY	F 590
	ICD=9	F 595
	IF (CELDX.EQ.O.O.AND.CELDY.EQ.O.O) GO TO 280	F 600
	IF (CELDX.GE.O.O.OR.CELDY.GE.O.O) GO TO 70	F 610
C	---PT. IN NW QUADRANT---	F 620
	VXNW=VXBDY(IVX,IVY)	F 630
	VXNE=VX(IXE,IVY)	F 640
	VXSW=VXBDY(IVX,IYS)	F 650
	VXSE=VX(IXE,IYS)	F 660
	VYNW=VYBDY(IVX,IVY)	F 670
	VYNE=VYBDY(IXE,IVY)	F 680
	VYSW=VY(IVX,IYS)	F 690
	VYSE=VY(IXE,IYS)	F 700
	ICD=1	F 705
	IF (THCK(IVX,IVY).EQ.O.O) GO TO 50	F 710
	IF (REC(IXE,IVY).EQ.O.O.AND.VPRM(IXE,IVY).LT.O.09) GO TO 40	F 720
	VXNE=VXNW	F 730
40	IF (REC(IVX,IYS).EQ.O.O.AND.VPRM(IVX,IYS).LT.O.09) GO TO 50	F 740
	VYSW=VYNW	F 750
50	IF (REC(IXE,IYS).EQ.O.O.AND.VPRM(IXE,IYS).LT.O.09) GO TO 270	F 760
	IF (THCK(IVX,IYS).EQ.O.O) GO TO 60	F 770
	IF (THCK(IXE+1,IYS).GT.O.O) VXSE=VXSW	F 782
60	IF (THCK(IXE,IVY).EQ.O.O) GO TO 270	F 790
	IF (THCK(IXE,IYS+1).GT.O.O) VYSE=VYNE	F 802
	GO TO 270	F 810
C		F 820
70	IF (CELDX.LE.O.O.OR.CELDY.GE.O.O) GO TO 130	F 830
C	---PT. IN NE QUADRANT---	F 840
80	VXNW=VX(IVX,IVY)	F 850
	VXNE=VXBDY(IVX,IVY)	F 860
	VXSW=VX(IVX,IYS)	F 870
	VXSE=VXBDY(IVX,IYS)	F 880
	VYNW=VYBDY(IVX,IVY)	F 890
	VYNE=VYBDY(IXE,IVY)	F 900
	VYSW=VY(IVX,IYS)	F 910
	VYSE=VY(IXE,IYS)	F 920
	ICD=2	F 925
	IF (CELDX.EQ.O.O) GO TO 120	F 930
	IF (THCK(IXE,IVY).EQ.O.O) GO TO 100	F 940
	IF (REC(IVX,IVY).EQ.O.O.AND.VPRM(IVX,IVY).LT.O.09) GO TO 90	F 950
	VXNW=VXNE	F 960
90	IF (REC(IXE,IYS).EQ.O.O.AND.VPRM(IXE,IYS).LT.O.09) GO TO 100	F 970
	VYSE=VYNE	F 980
100	IF (REC(IVX,IYS).EQ.O.O.AND.VPRM(IVX,IYS).LT.O.09) GO TO 270	F 990
	IF (THCK(IXE,IYS).EQ.O.O) GO TO 110	F1000
	IF (THCK(IVX-1,IYS).GT.O.O) VXSW=VXSE	F1012
110	IF (THCK(IVX,IVY).EQ.O.O) GO TO 270	F1020
	IF (THCK(IVX,IYS+1).GT.O.O) VYSW=VYNW	F1032
	GO TO 270	F1040
120	IF (REC(IVX,IYS).EQ.O.O.AND.VPRM(IVX,IYS).LE.O.09) GO TO 270	F1050
	IF (THCK(IVX,IVY).EQ.O.O) GO TO 270	F1060
	IF (THCK(IVX,IYS+1).GT.O.O) VYSW=VYNW	F1072
	GO TO 270	F1080
C		F1090
130	IF (CELDY.LE.O.O.OR.CELDX.GE.O.O) GO TO 190	F1100
C	---PT. IN SW QUADRANT---	F1110
140	VXNW=VXBDY(IVX,IVY)	F1120
	VXNE=VX(IXE,IVY)	F1130
	VXSW=VXBDY(IVX,IYS)	F1140
	VXSE=VX(IXE,IYS)	F1150

	VYNW=VY(IVX,IVY)	F1160
	VYNE=VY(IXE,IVY)	F1170
	VYSW=VYBDY(IVX,IVY)	F1180
	VYSE=VYBDY(IXE,IVY)	F1190
	ICD=3	F1195
	IF (CELDY.EQ.O.O) GO TO 180	F1200
	IF (THCK(IVX,IYS).EQ.O.O) GO TO 160	F1210
	IF (REC(IVX,IVY).EQ.O.O.AND.VPRM(IVX,IVY).LT.O.O9) GO TO 150	F1220
	VYNW=VYSW	F1230
150	IF (REC(IXE,IYS).EQ.O.O.AND.VPRM(IXE,IYS).LT.O.O9) GO TO 160	F1240
	VXSE=VXSW	F1250
160	IF (REC(IXE,IVY).EQ.O.O.AND.VPRM(IXE,IVY).LT.O.O9) GO TO 270	F1260
	IF (THCK(IVX,IVY).EQ.O.O) GO TO 170	F1270
	IF (THCK(IXE+1,IVY).GT.O.O) VXNE=VXNW	F1282
170	IF (THCK(IXE,IYS).EQ.O.O) GO TO 270	F1290
	IF (THCK(IXE,IVY-1).GT.O.O) VYNE=VYSE	F1302
	GO TO 270	F1310
180	IF (REC(IXE,IVY).EQ.O.O.AND.VPRM(IXE,IVY).LE.O.O9) GO TO 270	F1320
	IF (THCK(IVX,IVY).EQ.O.O) GO TO 270	F1330
	IF (THCK(IXE+1,IVY).GT.O.O) VXNE=VXNW	F1342
	GO TO 270	F1350
C		F1360
190	IF (CELDY.LE.O.O.OR.CELDX.LE.O.O) GO TO 260	F1370
C	---PT. IN SE QUADRANT---	F1380
200	VXNW=VX(IVX,IVY)	F1390
	VXNE=VXBDY(IVX,IVY)	F1400
	VXSW=VX(IVX,IYS)	F1410
	VXSE=VXBDY(IVX,IYS)	F1420
	VYNW=VY(IVX,IVY)	F1430
	VYNE=VY(IXE,IVY)	F1440
	VYSW=VYBDY(IVX,IVY)	F1450
	VYSE=VYBDY(IXE,IVY)	F1460
	ICD=4	F1465
	IF (CELDY.EQ.O.O) GO TO 240	F1470
	IF (CELDX.EQ.O.O) GO TO 250	F1480
	IF (THCK(IXE,IYS).EQ.O.O) GO TO 220	F1490
	IF (REC(IXE,IVY).EQ.O.O.AND.VPRM(IXE,IVY).LT.O.O9) GO TO 210	F1500
	VYNE=VYSE	F1510
210	IF (REC(IVX,IYS).EQ.O.O.AND.VPRM(IVX,IYS).LT.O.O9) GO TO 220	F1520
	VXSW=VXSE	F1530
220	IF (REC(IVX,IVY).EQ.O.O.AND.VPRM(IVX,IVY).LT.O.O9) GO TO 270	F1540
	IF (THCK(IXE,IVY).EQ.O.O) GO TO 230	F1550
	IF (THCK(IVX-1,IVY).GT.O.O) VXNW=VXNE	F1562
230	IF (THCK(IVX,IYS).EQ.O.O) GO TO 270	F1570
	IF (THCK(IVX,IVY-1).GT.O.O) VYNW=VYSW	F1582
	GO TO 270	F1590
240	IF (REC(IVX,IVY).EQ.O.O.AND.VPRM(IVX,IVY).LE.O.O9) GO TO 270	F1600
	IF (THCK(IXE,IVY).EQ.O.O) GO TO 270	F1610
	IF (THCK(IVX-1,IVY).GT.O.O) VXNW=VXNE	F1622
	GO TO 270	F1630
250	IF (REC(IVX,IVY).EQ.O.O.AND.VPRM(IVX,IVY).LE.O.O9) GO TO 270	F1640
	IF (THCK(IVX,IYS).EQ.O.O) GO TO 270	F1650
	IF (THCK(IVX,IVY-1).GT.O.O) VYNW=VYSW	F1662
	GO TO 270	F1670
C		F1680
260	IF (CELDX.EQ.O.O.AND.CELDY.LT.O.O) GO TO 80	F1690
	IF (CELDX.LT.O.O.AND.CELDY.EQ.O.O) GO TO 140	F1700
	IF (CELDX.GT.O.O.AND.CELDY.EQ.O.O) GO TO 200	F1710
	IF (CELDX.EQ.O.O.AND.CELDY.GT.O.O) GO TO 200	F1720
	WRITE (6,690) IN,IX,IY	F1730
270	CONTINUE	F1740
C	--- CHECK FOR ADJACENT NO-FLOW BOUNDARIES ---	F1741A
	GO TO (1270,1275,1280,1285,1290),ICD	F1741B
	GO TO 1290	F1741C
1270	IF (THCK(IXE,IVY).EQ.O.O) GO TO 1272	F1742A
	IF (THCK(IVX,IYS).EQ.O.O) GO TO 1273	F1742B

	IF (THCK(IVX,IVY).EQ.O.O) GO TO 1274	F1742C
	GO TO 1290	F1742D
1272	VXNE=VXSE	F1742E
	IF (THCK(IVX,IYS).GT.O.O) GO TO 1274	F1742F
1273	VYSW=VYSE	F1742G
1274	VXNW=VXSW	F1742H
	VYNW=VYNE	F1742I
	GO TO 1290	F1742J
1275	IF (THCK(IVX,IVY).EQ.O.O) GO TO 1277	F1744A
	IF (THCK(IXE,IYS).EQ.O.O) GO TO 1278	F1744B
	IF (THCK(IXE,IVY).EQ.O.O) GO TO 1279	F1744C
	GO TO 1290	F1742D
1277	VXNW=VXSW	F1744E
	IF (THCK(IXE,IYS).GT.O.O) GO TO 1279	F1744F
1278	VYSE=VYSW	F1744G
1279	VXNE=VXSE	F1744H
	VYNE=VYNW	F1744I
	GO TO 1290	F1744J
1280	IF (THCK(IXE,IYS).EQ.O.O) GO TO 1282	F1746A
	IF (THCK(IVX,IVY).EQ.O.O) GO TO 1283	F1746B
	IF (THCK(IVX,IYS).EQ.O.O) GO TO 1284	F1746C
	GO TO 1290	F1746D
1282	VXSE=VXNE	F1746E
	IF (THCK(IVX,IVY).GT.O.O) GO TO 1284	F1746F
1283	VYNW=VYNE	F1746G
1284	VXSW=VXNW	F1746H
	VYSW=VYSE	F1746I
	GO TO 1290	F1746J
1285	IF (THCK(IVX,IYS).EQ.O.O) GO TO 1287	F1748A
	IF (THCK(IXE,IVY).EQ.O.O) GO TO 1288	F1748B
	IF (THCK(IXE,IYS).EQ.O.O) GO TO 1289	F1748C
	GO TO 1290	F1748D
1287	VXSW=VXNW	F1748E
	IF (THCK(IXE,IVY).GT.O.O) GO TO 1289	F1748F
1288	VYNE=VYNW	F1748G
1289	VYSE=VYSW	F1748H
	VXSE=VXNE	F1748I
1290	CONTINUE	F1749A
C	*****	F1750
C	---BILINEAR INTERPOLATION---	F1760
	CELXD=XOLD-IVX	F1770
	CELDXH=AMOD(CELXD,0.5)	F1780
	CELDX=CELDXH*2.0	F1790
	CELDY=YOLD-IVY	F1800
C	*****	F1810
C	---X VELOCITY---	F1820
	VXN=VXNW*(1.0-CELDX)+VXNE*CELDX	F1830
	VXS=VXSW*(1.0-CELDX)+VXSE*CELDX	F1850
	XVEL=VXN*(1.0-CELDY)+VXS*CELDY	F1870
C	---Y VELOCITY---	F1900
	CELDYH=AMOD(CELDY,0.5)	F1910
	CELYD=CELDYH*2.0	F1921
	VYW=VYNW*(1.0-CELYD)+VYSW*CELYD	F1931
	VYE=VYNE*(1.0-CELYD)+VYSE*CELYD	F1951
	YVEL=VYW*(1.0-CELXD)+VYE*CELXD	F1970
C		F2000
	GO TO 290	F2010
280	XVEL=VX(IX,IY)	F2020
	YVEL=VY(IX,IY)	F2030
290	DISTX=XVEL*CONST1	F2040
	DISTY=YVEL*CONST2	F2050
C	*****	F2060
C	---BOUNDARY CONDITIONS---	F2070
	TEMPX=XOLD+DISTX	F2080
	TEMPY=YOLD+DISTY	F2090
	INX=TEMPX+0.5	F2100

	INV=TEMPY+0.5	F2110
	IF (THCK(INX,INY).GT.O.O) GO TO 330	F2120
C	*****	F2130
C	---X BOUNDARY---	F2140
	IF (THCK(INX,IY).EQ.O.O) GO TO 300	F2150
	PART(1,IN)=TEMPX	F2160
	GO TO 310	F2170
300	BEYON=TEMPX-IX	F2180
	IF (BEYON.LT.O.O) BEYON=BEYON+0.5	F2190
	IF (BEYON.GT.O.O) BEYON=BEYON-0.5	F2200
	PART(1,IN)=TEMPX-2.O*BEYON	F2210
	INX=PART(1,IN)+0.5	F2220
	TEMPX=PART(1,IN)	F2230
C	*****	F2240
C	---Y BOUNDARY---	F2250
310	IF (THCK(INX,INY).EQ.O.O) GO TO 320	F2260
	PART(2,IN)=TEMPY	F2270
	GO TO 340	F2280
C	*****	F2290
320	BEYON=TEMPY-IY	F2300
	IF (BEYON.LT.O.O) BEYON=BEYON+0.5	F2310
	IF (BEYON.GT.O.O) BEYON=BEYON-0.5	F2320
	PART(2,IN)=TEMPY-2.O*BEYON	F2330
	INY=PART(2,IN)+0.5	F2340
	TEMPY=PART(2,IN)	F2350
	GO TO 340	F2360
330	PART(1,IN)=TEMPX	F2370
	PART(2,IN)=TEMPY	F2380
340	CONTINUE	F2390
C	*****	F2400
C	---SUM CONCENTRATIONS AND COUNT PARTICLES---	F2410
	SUMC(INX,INY)=SUMC(INX,INY)+PART(3,IN)	F2420
	NPCELL(INX,INY)=NPCELL(INX,INY)+1	F2430
C	*****	F2440
C	---CHECK FOR CHANGE IN CELL LOCATION---	F2450
	IF (IX.EQ.INX.AND.IY.EQ.INY) GO TO 580	F2460
C	---CHECK FOR CONST.-HEAD BDY. OR SOURCE AT OLD LOCATION---	F2470
	IF (REC(IX,IY).LT.O.O) GO TO 350	F2480
	IF (REC(IX,IY).GT.O.O) GO TO 360	F2490
	IF (VPRM(IX,IY).LT.O.O9) GO TO 540	F2500
	IF (WT(IX,IY).GT.HK(IX,IY)) GO TO 350	F2510
	IF (WT(IX,IY).LT.HK(IX,IY)) GO TO 360	F2520
	GO TO 540	F2530
C	*****	F2540
C	---CREATE NEW PARTICLES AT BOUNDARIES---	F2550
350	IF (IFLAG.GT.O) GO TO 550	F2560
	KFLAG=1	F2570
360	DO 370 IL=1,500	F2580
	IF (LIMBO(IL).EQ.O) GO TO 370	F2590
	IP=LIMBO(IL)	F2600
	IF (IP.LT.IN) GO TO 380	F2610
370	CONTINUE	F2620
C	*****	F2630
C	---GENERATE NEW PARTICLE---	F2640
	IF (NPTM.EQ.NPMAX) GO TO 600	F2650
	NPTM=NPTM+1	F2660
	IP=NPTM	F2670
	GO TO 390	F2680
380	LIMBO(IL)=O	F2690
C	*****	F2700
390	IF (KFLAG.EQ.O) GO TO 398	F2705
	ITEM=PTID(IN)	F2845
	GO TO 399	F2855
398	SUMC(IX,IY)=SUMC(IX,IY)+CONC(IX,IY)	F2865
	NPCELL(IX,IY)=NPCELL(IX,IY)+1	F2875
	IF (NPOLD(IX,IY).GT.O) NPOLD(IX,IY)=NPOLD(IX,IY)-1	F2885

	IF (IFLAG.GT.O) GO TO 441	F2895
	IF (KFLAG.EQ.O) GO TO 441	F2899
399	GO TO (401,411,421,431,441,451,461,471,481).ITEM	F2905
	GO TO 441	F2915
401	PART(1,IP)=IX-F1	F2925
	PART(2,IP)=IY-F1	F2935
	PTID(IP)=1	F2935
	GO TO 530	F2955
411	PART(1,IP)=IX-F1	F2965
	PART(2,IP)=IY+F1	F2975
	PTID(IP)=2	F2985
	GO TO 530	F2995
421	PART(1,IP)=IX+F1	F3005
	PART(2,IP)=IY-F1	F3015
	PTID(IP)=3	F3025
	GO TO 530	F3035
431	PART(1,IP)=IX+F1	F3045
	PART(2,IP)=IY+F1	F3055
	PTID(IP)=4	F3065
	GO TO 530	F3075
441	PART(1,IP)=IX	F3085
	PART(2,IP)=IY	F3095
	PTID(IP)=5	F3105
	GO TO 530	F3115
451	PART(1,IP)=IX-F2	F3125
	PART(2,IP)=IY	F3135
	PTID(IP)=6	F3145
	GO TO 530	F3155
461	PART(1,IP)=IX	F3165
	PART(2,IP)=IY-F2	F3175
	PTID(IP)=7	F3185
	GO TO 530	F3195
471	PART(1,IP)=IX+F2	F3205
	PART(2,IP)=IY	F3215
	PTID(IP)=8	F3225
	GO TO 530	F3235
481	PART(1,IP)=IX	F3245
	PART(2,IP)=IY+F2	F3255
	PTID(IP)=9	F3265
C		F3510
530	PART(2,IP)=-PART(2,IP)	F3520
	PART(3,IP)=CONC(IX,IY)	F3530
C	*****	F3550
C	---CHECK FOR DISCHARGE BOUNDARY AT NEW LOCATION---	F3560
540	IFLAG=1.O	F3570
550	IF (VPRM(INX,INX).GT.O.O9.AND.WT(INX,INX).LT.HK(INX,INX)) GO TO 56	F3580
	10	F3590
	IF (REC(INX,INX).GT.O.O) GO TO 560	F3600
	GO TO 590	F3610
C	*****	F3620
C	---PUT PT. IN LIMBO IF PT. DENSITY NOT INCREASED---	F3625
560	IF (NPOLD(INX,INX).LE.O) GO TO 590	F3635
	PART(1,IN)=O.O	F3645
	PART(2,IN)=O.O	F3650
	PART(3,IN)=O.O	F3660
	SUMC(INX,INX)=SUMC(INX,INX)-CONC(INX,INX)	F3662
	NPCELL(INX,INX)=NPCELL(INX,INX)-1	F3664
	NPOLD(INX,INX)=NPOLD(INX,INX)-1	F3666
	DO 570 ID=1,500	F3670
	IF (LIMBO(ID).GT.O) GO TO 570	F3680
	LIMBO(ID)=IN	F3690
	GO TO 590	F3700
570	CONTINUE	F3710
C		F3720
580	IF (IFLAG.LT.O) PART(2,IN)=-TEMPY	F3730
590	CONTINUE	F3750

C	---END OF LOOP---	F3760
C	*****	F3770
	GO TO 620	F3780
C	---RESTART MOVE IF PT. LIMIT EXCEEDED---	F3790
600	WRITE (6,700) IMOV,IN	F3800
	TEST=100.0	F3810
	CALL GENPT	F3820
	DO 610 IX=1,NX	F3830
	DO 610 IY=1,NY	F3840
	SUMC(IX,IY)=0.0	F3850
610	NPCELL(IX,IY)=0	F3860
	TEST=0.0	F3870
	GO TO 10	F3880
C	*****	F3890
620	SUMTCH=SUMTCH+TIMV	F3900
C	---ADJUST NUMBER OF PARTICLES---	F3910
	NP=NPTM	F3920
	WRITE (6,670) NP,IMOV	F3930
C	*****	F3940
C	CALL CNCON	F3950
C	*****	F3960
C	---STORE OBS. WELL DATA FOR STEADY FLOW PROBLEMS---	F3970
	IF (S.GT.0.0) GO TO 640	F3980
	IF (NUMOBS.LE.0) GO TO 640	F3990
	J=MOD(IMOV,50)	F4000
	IF (J.EQ.0) J=50	F4010
	TMOBS(J)=SUMTCH	F4020
	DO 630 I=1,NUMOBS	F4030
	TMWL(I,J)=HK(IXOBS(I),IYOBS(I))	F4040
630	TMCN(I,J)=CONC(IXOBS(I),IYOBS(I))	F4050
C	---PRINT CHEMICAL OUTPUT---	F4060
	IF (MOD(IMOV,50).EQ.0) IPRNT = 1	F4065
640	IF (IMOV.GE.NMOV) GO TO 660	F4070
	IF (MOD(IMOV,NPNTMV).EQ.0) IPRNT = -1	F4082
650	IF (IPRNT.NE.0) CALL CHMOT	F4085
C	*****	F4090
660	RETURN	F4100
C	*****	F4110
C		F4120
C		F4130
C		F4140
670	FORMAT (1H0,2X,2HNP,7X,2H= ,8X,I4,10X,11HIMOV = ,8X,I4)	F4150
680	FORMAT (1H0,10X,61HNO. OF PARTICLE MOVES REQUIRED TO COMPLETE THIS	F4160
	1 TIME STEP = ,I4//)	F4170
690	FORMAT (1H0,5X,53H*** WARNING *** QUADRANT NOT LOCATED FOR PT.	F4180
	1 NO. ,I5,11H , IN CELL ,2I4)	F4190
700	FORMAT (1H0,5X,17H *** NOTE *** ,10X,23HNPTM.EQ.NPMAX --- IMOV=	F4200
	1,I4,5X,8HPT. NO. = ,I4,5X,10HCALL GENPT/)	F4210
	END	F4220-


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IF (REC(IX,IY).NE.O.O.OR.VPRM(IX,IY).GT.O.O9) GO TO 90          G 900
NZERO=NZERO+1                                                  G 910
GO TO 90                                                         G 920
80 CONC(IX,IY)=SUMC(IX,IY)/APC                                  G 930
90 CONTINUE                                                     G 940
C   ---CHECK NUMBER OF CELLS VOID OF PTS.---                   G 950
IF (NZERO.GT.O) WRITE (6,290) NZERO,IMOV                       G 960
IF (NZERO.LE.NZCRIT) GO TO 110                                  USNRC
TEST=99.O                                                       G 980
WRITE (6,300)                                                    G 990
WRITE (6,320)                                                    G1000
DO 100 IY=1,NY                                                  G1010
100 WRITE (6,330) (NPCELL(IX,IY),IX=1,NX)                       G1020
GO TO 110                                                        USNRC
C   *****                                                    G1040
C   ---CHANGE CONCENTRATIONS AT NODES---                        G1050
110 DO 130 IX=1,NX                                              G1060
DO 130 IY=1,NY                                                  G1070
IF (THCK(IX,IY).EQ.O.O) GO TO 120                               G1080
CONC(IX,IY)=CONC(IX,IY)+CNCNC(IX,IY)                           G1090
SUMC(IX,IY)=O.O                                                 G1110
IF (CONC(IX,IY).LE.O.O) GO TO 130                               G1120
CNCPC=CNCNC(IX,IY)/CONC(IX,IY)                                  G1130
SUMC(IX,IY)=CNCPC                                               G1140
GO TO 130                                                        G1150
120 IF (CONC(IX,IY).GT.O.O) WRITE (6,310) IX,IY,CONC(IX,IY)   G1160
CONC(IX,IY)=O.O                                                 G1170
130 CONTINUE                                                    G1180
C   *****                                                    G1190
C   ---CHANGE CONCENTRATION OF PARTICLES---                    G1200
DO 180 IN=1,NP                                                  G1210
IF (PART(1,IN).EQ.O.O) GO TO 180                                G1220
INX=ABS(PART(1,IN))+O.5                                          G1230
INY=ABS(PART(2,IN))+O.5                                          G1240
C   ---UPDATE CONC. OF PTS. IN SINK/SOURCE CELLS---          G1250
IF (REC(INX,INY).NE.O.O) GO TO 140                              G1260
IF (VPRM(INX,INY).LE.O.O9) GO TO 150                           G1270
140 PART(3,IN)=CONC(INX,INY)                                     G1280
GO TO 180                                                        G1290
150 IF (CNCNC(INX,INY).LT.O.O) GO TO 170                        G1300
160 PART(3,IN)=PART(3,IN)+CNCNC(INX,INY)                        G1310
GO TO 180                                                        G1320
170 IF (CONC(INX,INY).LE.O.O) GO TO 160                         G1330
IF (SUMC(INX,INY).LT.-1.O) GO TO 160                           G1340
PART(3,IN)=PART(3,IN)+PART(3,IN)*SUMC(INX,INY)                 G1350
180 CONTINUE                                                    G1360
WRITE (6,280) TIM(N),TIMV,SUMTCH                                 G1370
C   *****                                                    G1380
C   ---COMPUTE MASS BALANCE FOR SOLUTE---                      G1390
DO 270 IX=1,NX                                                  G1420
DO 270 IY=1,NY                                                  G1430
IF (THCK(IX,IY).EQ.O.O) GO TO 270                               G1440
SUMC(IX,IY)=O.O                                                 G1450
NPOLD(IX,IY)=NPCELL(IX,IY)                                      USNRC
NPCELL(IX,IY)=O                                                G1684
270 CONTINUE                                                    G1690
C   *****                                                    G1700
C   ---COMPUTE CHANGE IN MASS OF SOLUTE STORED---             G1710
CSTORM=STORM-STORMI                                             G1720
SUMIO=FLMIN+FLMOT-CMSIN-CMSOUT                                  G1730
C   *****                                                    G1740
C   ---REGENERATE PARTICLES IF "NZCRIT" EXCEEDED---          G1750
IF (TEST.GT.98.O) CALL GENPT                                    G1760
TEST=O.O                                                         G1770
IF (NSORB.GT.1) CALL VELNEW (CNOLD)                              USNRC
C   *****                                                    G1780

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	RETURN	G1790
C	*****	G1800
C		G1810
C		G1820
C		G1830
	280 FORMAT (3H ,11HTIM(N) = ,1P1E12.5,10X,11HTIMV = ,1P1E12.5,	G1840
	110X,9HSUMTCH = ,1P1E12.5)	G1850
	290 FORMAT (1H0,5X,40HNUMBER OF CELLS WITH ZERO PARTICLES = ,I4,5X,9	G1860
	1HIMOV = ,I4/)	G1870
	300 FORMAT (1H0,5X,44H*** NZCRIT EXCEEDED --- CALL GENPT ***/)	G1880
	310 FORMAT (1H ,5X,37H***CONC.GT.O.AND.THCK.EQ.O AT NODE = ,2I4,4X,7HC	G1890
	10NC = ,1P1E10.4,4H ***)	G1900
	320 FORMAT (1H0,2X,6HNPCCELL/)	G1910
	330 FORMAT (1H ,4X,20I3)	G1920
	END	G1930-

**** TSO FOREGROUND HARDCOPY ****
 DSNAME=U11236C.KONIMOD.CNTL

(OUTPT)

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C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER
C $NOFLOATCALLS
C $STORAGE:2
SUBROUTINE OUTPT H 10
CHARACTER*8 TITLE H 11
REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT H 20
REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR H 30
REAL*8 HJ H 35
INTEGER FCON H 36
COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO H 40
1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N H 50
2PNCHV,NPDEL,C,ICLK,FCON,IHEAD,ISOLV H 62
COMMON /PRMC/ NODEID(20,20),NPCELL(20,20),NPOLD(20,20),LIMBO(500), H 65
1IXOBS(5),IYOBS(5) H 66
2,NDECAY,NSORB USNRC
COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR H 90
1,THICK(20,20) H 91
COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20, H 100
120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T H 110
2TITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR H 120
3,HJ(20,20) H 125
COMMON /BALM/ TOTLQ,TOTLQI,TPIN,TPOUT,TPQR H 127
DIMENSION IH(20),TRANS(20) H 140
***** H 150
C TIMD=SUMT/86400. H 160
TIMY=SUMT/(86400.0*365.25) H 170
C ---PRINT HEAD VALUES--- H 180
WRITE (6,120) H 190
WRITE (6,130) N H 200
WRITE (6,140) SUMT H 210
WRITE (6,150) TIMD H 220
WRITE (6,160) TIMY H 230
WRITE (6,170) H 240
DO 10 IY=1,NY H 250
10 WRITE (6,180) (HK(IX,IY),IX=1,NX) H 260
IF (N.EQ.0) GO TO 110 H 270
***** H 280
C ---PRINT HEAD MAP--- H 290
WRITE (6,120) H 300
WRITE (6,130) N H 310
WRITE (6,140) SUMT H 320
WRITE (6,150) TIMD H 330
WRITE (6,160) TIMY H 340
WRITE (6,170) H 350
DO 30 IY=1,NY H 360
DO 20 IX=1,NX H 370
20 IH(IX)=HK(IX,IY)+0.5 H 380
30 WRITE (6,190) (IH(ID),ID=1,NX) H 390
***** H 400
C ---COMPUTE WATER BALANCE AND DRAWDOWN--- H 410
QSTR=0.0 H 420
PUMP=0.0 H 430
PQIN=0.0 H 432
PQOUT=0.0 H 434
TPUM=0.0 H 440
QIN=0.0 H 450
QOUT=0.0 H 460
QNET=0.0 H 470
DELQ=0.0 H 480
PCTERR=0.0 H 500
PQR = 0.0 H 501
WRITE (6,290) H 510

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C	DO 80 IY=1,NY	H 520
	DO 70 IX=1,NX	H 530
	IH(IX)=0.0	H 540
	IF (THCK(IX,IY).EQ.0.0) GO TO 70	H 550
	IF (REC(IX,IY).GT.0.0) GO TO 32	H 560
	PQIN=PQIN+REC(IX,IY)	H 562
	GO TO 34	H 564
	32 PQOUT=PQOUT+REC(IX,IY)	H 566
	34 IF (RECH(IX,IY).GT.0.0) GO TO 36	H 568
	PQR=PQR+RECH(IX,IY)*AREA	H 572
	GO TO 38	H 575
	36 PQOUT=PQOUT+RECH(IX,IY)*AREA	H 576
	38 IF (VPRM(IX,IY).EQ.0.0) GO TO 60	H 578
	DELO=VPRM(IX,IY)*AREA*(WT(IX,IY)-HK(IX,IY))	H 582
	IF (DELO.GT.0.0) GO TO 40	H 590
	QOUT=QOUT+DELO	H 600
	GO TO 50	H 610
	40 QIN=QIN+DELO	H 620
	50 QNET=QNET+DELO	H 630
	60 DDRW=HI(IX,IY)-HK(IX,IY)	H 640
	IH(IX)=DDRW+0.5	H 650
	QSTR=QSTR+DDRW*AREA*S	H 660
	70 CONTINUE	H 670
C	---PRINT DRAWDOWN MAP---	H 680
	WRITE (6,300) (IH(IX),IX=1,NX)	H 690
	80 CONTINUE	H 700
C	---PRINT THICKNESS MAP---	H 710
	IF (FCON.EQ.0) GO TO 75	H 711
	WRITE (6,310)	H 712
	DO 85 IY=1,NY	H 713
	WRITE (6,320) (THCK(IX,IY),IX=1,NX)	H 715
	85 CONTINUE	H 716A
C	---PRINT TRANSMISSIVITY MAP---	H 718
	WRITE (6,330)	H 719
	DO 90 IY=1,NY	H 720
	DO 95 IX=1,NX	H 722
	TRANS(IX)=PERM(IX,IY)*THCK(IX,IY)	H 723
	95 CONTINUE	H 724
	WRITE (6,340) (TRANS(IX),IX=1,NX)	H 725
	90 CONTINUE	H 726
	75 CONTINUE	H 728
	TPUM = PQIN + PQR + PQOUT	H 729
	PUMP = TPIN + TPQR + TPOUT	H 730
	TOTLON=TOTLQ+TOTLQI	H 740
	SRCS=QSTR-TPIN-TOTLQI-TPQR	H 745
	SINKS=TPOUT+TOTLQ	H 757
	ERRMB=SRCS-SINKS	H 766
	DENOM=(SRCS+SINKS)*0.5	H 775
	IF (DENOM.EQ.0.0) GO TO 100	H 785
	PCTERR=ERRMB*100.0/DENOM	H 795
C	---PRINT MASS BALANCE DATA FOR FLOW MODEL---	H 805
100	WRITE (6,240)	H 830
	WRITE (6,215) TPQR	H 840
	WRITE (6,211) TPIN	H 841
	WRITE (6,212) TPOUT	H 842
	WRITE (6,250) PUMP	H 844
	WRITE (6,230) QSTR	H 850
	WRITE (6,202) TOTLQI	H 860
	WRITE (6,203) TOTLQ	H 862
	WRITE (6,260) TOTLON	H 864
	WRITE (6,270) ERRMB	H 866
	WRITE (6,280) PCTERR	H 880
	WRITE (6,201)	H 883
	WRITE (6,215) PQR	H 886
	WRITE (6,202) QIN	H 887
		H 889

	WRITE (6.203) QOUT	H 892
	WRITE (6.204) QNET	H 895
	WRITE (6.211) PQIN	H 898
	WRITE (6.212) PQOUT	H 901
	WRITE (6.210) TPUM	H 910
	*****	H 940
C	110 RETURN	H 950
	*****	H 960
C		H 970
C		H 980
C		H 990
	120 FORMAT (1H1,23HHEAD DISTRIBUTION - ROW)	H1000
	130 FORMAT (1X,23HNUMBER OF TIME STEPS = ,1I5)	H1010
	140 FORMAT (8X,16HTIME(SECONDS) = ,1P1E12.5)	H1020
	150 FORMAT (8X,16HTIME(DAYS) = ,1P1E12.5)	H1030
	160 FORMAT (8X,16HTIME(YEARS) = ,1P1E12.5)	H1040
	170 FORMAT (1H)	H1050
	180 FORMAT (1HO,1OF12.7)	H1055
	190 FORMAT (1HO,2OI4)	H1070
	201 FORMAT (1HO,2X,33HRATE MASS BALANCE -- (IN C.F.S.) //)	H1073
	202 FORMAT (4X,29HLEAKAGE INTO AQUIFER = ,1P1E12.5)	H1076
	203 FORMAT (4X,29HLEAKAGE OUT OF AQUIFER = ,1P1E12.5)	H1083
	204 FORMAT (4X,29HNET LEAKAGE (QNET) = ,1P1E12.5)	H1086
	210 FORMAT (4X,29HNET WITHDRAWAL (TPUM) = ,1P1E12.5)	H1093
	211 FORMAT (4X,29HINJECTION = ,1P1E12.5)	H1095
	212 FORMAT (4X,29HPUMPAGE = ,1P1E12.5)	H1100
	215 FORMAT (4X,29HRECHARGE = ,1P1E12.5)	H1110
	230 FORMAT (4X,29HWATER RELEASE FROM STORAGE = ,1P1E12.5)	H1120
	240 FORMAT (1HO,2X,38HCUMULATIVE MASS BALANCE -- (IN FT**3) //)	H1125
	250 FORMAT (4X,29HCUMULATIVE NET PUMPAGE = ,1P1E12.5)	H1140
	260 FORMAT (4X,29HCUMULATIVE NET LEAKAGE = ,1P1E12.5)	H1150
	270 FORMAT (1HO,7X,25HMASS BALANCE RESIDUAL = ,1P1E12.5)	H1160
	280 FORMAT (1H ,7X,25HERROR (AS PERCENT) = ,1P1E12.5//)	H1170
	290 FORMAT (1H1,8HDRAWDOWN)	H1180
	300 FORMAT (3H ,2OI5)	H1190
	310 FORMAT (1H1,17HAQUIFER THICKNESS)	H1192
	320 FORMAT (3H ,2OF5.1)	H1194
	330 FORMAT (1H1,14HTRANSMISSIVITY)	H1196
	340 FORMAT (3H ,2OF5.2)	H1198
	END	H1200-

**** TSO FOREGROUND HARDCOPY ****

DSNAME=U11236C.KONIMOD.CNTL

(CHMOT)

C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER

C \$NOFLOATCALLS

C \$STORAGE:2

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SUBROUTINE CHMOT I 10
CHARACTER*8 TITLE I 11
REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT I 20
REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR I 30
REAL*8 HJ I 35
INTEGER FCON I 36
COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO I 40
1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N I 50
2PNCHV,NPDELC,ICLK,FCON,IHEAD,ISOLV I 62
COMMON /PRMC/ NDEID(20,20),NPCELL(20,20),NPOLD(20,20),LIMBO(500), I 65
1XOBS(5),IYBS(5) I 66
2,NDECAY,NSORB USNRC
COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR I 90
1,THICK(20,20) I 91
COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20, I 100
120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T I 110
2TITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR I 120
3,HJ(20,20) I 125
COMMON /CHMA/ PART(3,3200),CONC(20,20),TMCN(5,50),VX(20,20),VY(20, I 130
120),CONINT(20,20),CNRECH(20,20),POROS,SUMTCH,BETA,TIMV,STORM,STORM I 140
2I,CMSIN,CMSOUT,FLMIN,FLMOT,SUMID,CELDIS,DLTRAT,CSTORM I 150
3,DCYLAM,BLKDEN,SRBRAT,SRBSAT,SRBALF,VOLDCY,VOLSRB,SRBDCY USNRC
DIMENSION IC(20) I 160
***** I 170
C TMFY=86400.0*365.25 I 180
TMYR=SUMT/TMFY I 190
TCHD=SUMTCH/86400.0 I 200
TCHYR=SUMTCH/TMFY I 210
ERR1=0.0 I 212
ERR3=0.0 I 214
IF (IPRNT.GT.0) GO TO 100 I 220
***** I 230
C ---PRINT CONCENTRATIONS--- I 240
WRITE (6,160) I 250
WRITE (6,170) N I 260
IF (N.GT.0) WRITE (6,180) TIM(N) I 270
WRITE (6,190) SUMT I 280
WRITE (6,450) SUMTCH I 290
WRITE (6,200) TCHD I 300
WRITE (6,210) TMYR I 310
WRITE (6,460) TCHYR I 320
WRITE (6,380) IMOV I 330
WRITE (6,220) I 340
DO 5 IY=1,NY I 344
5 WRITE (6,245) (CONC(IX,IY),IX=1,NX) I 346
WRITE (6,160) I 347
WRITE (6,170) N I 348
WRITE (6,220) I 349
DO 20 IY=1,NY I 350
DO 10 IX=1,NX I 360
10 IC(IX)=CONC(IX,IY)+0.5 I 370
20 WRITE (6,240) (IC(IX),IX=1,NX) I 380
C ***** I 390
IF (N.EQ.0) GO TO 150 I 400
IF (NPDELC.EQ.0) GO TO 50 I 410
C I 420
C ---PRINT CHANGES IN CONCENTRATION--- I 430
WRITE (6,230) I 440
WRITE (6,170) N I 450
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WRITE (6,180) TIM(N) I 460
WRITE (6,190) SUMT I 470
WRITE (6,450) SUMTCH I 480
WRITE (6,200) TCHD I 490
WRITE (6,210) TMYR I 500
WRITE (6,460) TCHYR I 510
WRITE (6,380) IMOV I 520
WRITE (6,220) I 530
DO 40 IY=1,NY I 540
DO 30 IX=1,NX I 550
CNG=CONC(IX,IY)-CONINT(IX,IY) I 560
30 IC(IX)=CNG I 570
40 WRITE (6,240) (IC(IX),IX=1,NX) I 580
C ***** I 590
C ---PRINT MASS BALANCE DATA FOR SOLUTE--- I 600
50 RESID=SUMIO-CSTORM + VOLDCY - VOLSRB + SRBDCY USNRC
SUMIN=FLMIN-CMSIN I 615
IF (SUMIN.EQ.O.O) GO TO 60 I 625
ERR1=RESID*100.O/SUMIN I 635
60 IF (STORMI.EQ.O.O) GO TO 70 I 650
ERR3=-100.O*RESID/(STORMI-SUMIO) I 660
70 WRITE (6,220) I 670
WRITE (6,250) I 680
WRITE (6,220) I 690
WRITE (6,260) FLMIN I 700
WRITE (6,270) FLMOT I 710
RECIN=-CMSIN I 720
RECOUT=-CMSOUT I 730
WRITE (6,290) RECIN I 740
WRITE (6,280) RECOUT I 750
WRITE (6,300) SUMIO I 760
WRITE (6,310) STORMI I 770
WRITE (6,320) STORM I 780
WRITE (6,330) CSTORM I 790
IF (NDECAY.GT.O) WRITE (6,333) VOLDCY USNRC
IF (NSORB.GT.O) WRITE (6,335) VOLSRB USNRC
IF (NSORB.GT.O.AND.NDECAY.GT.O) WRITE (6,336) SRBDCY USNRC
WRITE (6,340) I 810
WRITE (6,350) RESID I 820
WRITE (6,360) ERR1 I 830
80 IF (STORMI.EQ.O.O) GO TO 90 I 840
WRITE (6,370) I 850
WRITE (6,360) ERR3 I 860
C ***** I 870
C ---PRINT HYDROGRAPHS AFTER 50 STEPS OR END OF SIMULATION--- I 880
90 IF (MOD(IMOV,50).EQ.O.AND.S.EQ.O.O) GO TO 100 I 890
IF (MOD(N,50).EQ.O.AND.S.GT.O.O) GO TO 100 I 900
IF (S.EQ.O.O.AND.N.LT.NTIM.AND.INT.GT.O) GO TO 100 I 905
GO TO 150 I 910
100 WRITE (6,390) TITLE I 920
IF (NUMOBS.LE.O) GO TO 150 I 930
WRITE (6,400) INT I 940
IF (S.GT.O.O) WRITE (6,410) I 950
IF (S.EQ.O.O) WRITE (6,420) I 960
C ---TABULATE HYDROGRAPH DATA--- I 970
MOZ=O I 980
IF (S.GT.O.O) GO TO 110 I 990
NTO=NMOV I 1000
IF (NMOV.GT.50) NTO=MOD(IMOV,50) I 1010
GO TO 120 I 1020
110 NTO=NTIM I 1030
IF (NTIM.GT.50) NTO=MOD(N,50) I 1040
120 IF (NTO.EQ.O) NTO=50 I 1050
DO 140 J=1,NUMOBS I 1060
TMYR=O.O I 1070
WRITE (6,430) J,IXOBS(J),IYOBS(J) I 1080

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WRITE (6,440) MOZ,WT(IXOBS(J),IYOBS(J)),CONINT(IXOBS(J),IYOBS(J)), I 1090
1TMYR I 1100
DO 130 M=1,NT0 I 1110
TMYR=TMOBS(M)/TMFY I 1120
WRITE (10,445) INT,N,J,M,TMWL(J,M),TMCN(J,M),TMYR I 1125
130 WRITE (6,440) M,TMWL(J,M),TMCN(J,M),TMYR I 1130
140 CONTINUE I 1140
C ***** I 1150
150 IPRNT = 0 I 1155
RETURN I 1165
C ***** I 1170
C I 1180
C I 1190
C I 1200
160 FORMAT (1H1,13HCONCENTRATION/) I 1210
170 FORMAT (1X,23HNUMBER OF TIME STEPS = ,I5) I 1220
180 FORMAT (8X,16HDELTA T = ,1P1E12.5) I 1230
190 FORMAT (8X,16HTIME(SECONDS) = ,1P1E12.5) I 1240
200 FORMAT (3X,21HCHEM.TIME(DAYS) = ,1P1E12.5) I 1250
210 FORMAT (8X,16HTIME(YEARS) = ,1P1E12.5) I 1260
220 FORMAT (1H ) I 1270
230 FORMAT (1H1,23HCHANGE IN CONCENTRATION/) I 1280
240 FORMAT (1H0,20I5) I 1290
245 FORMAT (1H0,10F10.4) I 1295
250 FORMAT (1H ,21HCHEMICAL MASS BALANCE) I 1300
260 FORMAT (8X,25HMASS IN BOUNDARIES = ,1P1E12.5) I 1310
270 FORMAT (8X,25HMASS OUT BOUNDARIES = ,1P1E12.5) I 1320
280 FORMAT (8X,25HMASS PUMPED OUT = ,1P1E12.5) I 1330
290 FORMAT (8X,25HMASS PUMPED IN = ,1P1E12.5) I 1340
300 FORMAT (8X,25HINFLOW MINUS OUTFLOW = ,1P1E12.5) I 1350
310 FORMAT (8X,25HINITIAL MASS STORED = ,1P1E12.5) I 1360
320 FORMAT (8X,25HPRESENT MASS STORED = ,1P1E12.5) I 1370
330 FORMAT (8X,25HCHANGE MASS STORED = ,1P1E12.5) I 1380
333 FORMAT (8X,25HDECAY OF SOLUTE MASS = ,1P1E12.5) USNRC
335 FORMAT (8X,25HSORPTION STORAGE (S) = ,1P1E12.5) USNRC
336 FORMAT (8X,25HSORPTION DECAY (S) = ,1P1E12.5) USNRC
340 FORMAT (1H ,5X,53HCOMPARE RESIDUAL WITH NET FLUX AND MASS ACCUMULA I 1390
TION:) I 1400
350 FORMAT (8X,25HMASS BALANCE RESIDUAL = ,1P1E12.5) I 1410
360 FORMAT (8X,25HERROR (AS PERCENT) = ,1P1E12.5) I 1420
370 FORMAT (1H ,5X,55HCOMPARE INITIAL MASS STORED WITH CHANGE IN MASS I 1430
STORED:) I 1440
380 FORMAT (1X,23H NO. MOVES COMPLETED = ,I5) I 1450
390 FORMAT (1H1,10A8//) I 1460
400 FORMAT (1H0,5X,65HTIME VERSUS HEAD AND CONCENTRATION AT SELECTED O I 1470
BSERVATION POINTS//15X,19HPUMPING PERIOD NO. ,I4////) I 1480
410 FORMAT (1H0,16X,19HTRANSIENT SOLUTION////) I 1490
420 FORMAT (1H0,15X,21HSTEADY-STATE SOLUTION////) I 1500
430 FORMAT (1H0,20X,22HOBS.WELL NO. X Y,17X,1HN,6X,40HHEAD (FT) I 1510
1 CONC.(MG/L) TIME (YEARS)//17X,I3,9X,I2,3X,I2//) I 1520
440 FORMAT (1H ,58X,I2,6X,F7.1,8X,F7.1,8X,F7.3) I 1531
445 FORMAT (1H ,4I4,3F7.3) I 1535
450 FORMAT (1H ,2X,21HCHEM.TIME(SECONDS) = ,1P1E12.5) I 1540
460 FORMAT (1H ,2X,21HCHEM.TIME(YEARS) = ,1P1E12.5) I 1550
END I 1560-

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**** TSD FOREGROUND HARDCOPY ****

DSNAME=U11236C.KONIMOD.CNTL

(VELNEW)

C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER

C \$NOFLOATCALLS

C \$STORAGE:2

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SUBROUTINE VELNEW (CNOLD)
CHARACTER*8 TITLE
REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT
REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
REAL*8 RATE,SLEAK,DIV
REAL*8 HJ
INTEGER FCON
COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO
1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N
2PNCHV,NPDEL,ICLK,FCON,IHEAD,ISQV
COMMON /PRMC/ NODEID(20,20),NPCELL(20,20),NPOLD(20,20),LIMBO(50),
1IXOBS(5),IYOBS(5)
2,NDECAY,NSORB
COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR
1,THICK(20,20)
COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20,
120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T
2ITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
3,HJ(20,20)
COMMON /XINV/ DXINV,DYINV,ARINV,PORINV
COMMON /CHMA/ PART(3,3200),CONC(20,20),TMCN(5,50),VX(20,20),VY(20,
120),CONINT(20,20),CNRECH(20,20),POROS,SUMTCH,BETA,TIMV,STORM,STORM
2I,CMSIN,CMSOUT,FLMIN,FLMOT,SUMID,CELDIS,DLTRAT,CSTORM
3,DCYLAM,BLKDEN,SRBRAT,SRBSAT,SRBALF,VOLDCY,VOLSRB,SRBDCY
COMMON /CHMC/ SUMC(20,20),VXBDY(20,20),VYBDY(20,20)
COMMON /DIFUS/ DISP(20,20,4)
DIMENSION CNOLD(20,20)
*****
C -----UPDATE VELOCITIES AND STORE-----
C
VMAX = 0.0
TDIV = 0.0
TDIS = 0.0
IXQMAX = 0
IYQMAX = 0
IF (IMOV.LT.2) ELPTIM = 0.0
ELPTIM = ELPTIM + TIMV
TIMREM = TIM(N) - ELPTIM
RATIOT = TIMREM/TIM(N)
IF (RATIOT.GT.1.0E-07) GO TO 10
NMOV = IMOV
RETURN
10 DO 50 IX=1,NX
DO 50 IY=1,NY
DO 20 IZ=1,4
20 DISP(IX,IY,IZ)=0.0
IF (THCK(IX,IY).EQ.0.0) GO TO 50
DISTN = 0.0
DISTO = 0.0
IF (NSORB.GT.2) GO TO 30
C*** *****LANGMUIR SORBTION*****
DISTN = BLKDEN*SRBRAT*SRBSAT/(1.0+SRBRAT*CONC(IX,IY))**2.0
DISTO = BLKDEN*SRBRAT*SRBSAT/(1.0+SRBRAT*CNOLD(IX,IY))**2.0
GO TO 40
30 IF (SRBALF.EQ.0.0) GO TO 40
C*** *****FREUNDLICH SORBTION*****
DIST = BLKDEN*SRBRAT*SRBALF
LOGCON = -23.0
IF (CONC(IX,IY).GT.1.0E-10) LOGCON = ALOG(CONC(IX,IY))
SRBEXP = (SRBALF-1.0)*LOGCON
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IF (SRBEXP.GT.23.0) SRBEXP = 23.0 J 550
DISTN = DIST*EXP(SRBEXP) J 560
LOGCON = -23.0 J 570
IF (CNOLD(IX,IY).GT.1.0E-10) LOGCON = ALOG(CNOLD(IX,IY)) J 580
SRBEXP = (SRBALF-1.0)*LOGCON J 590
IF (SRBEXP.GT.23.0) SRBEXP = 23.0 J 610
DISTO = DIST*EXP(SRBEXP) J 620
40 RETARD = (1.0+DISTO)/(1.0+DISTN) J 630
C J 640
C ---UPDATE VELOCITIES AT NODES--- J 650
C ---X-DIRECTION--- J 660
VX(IX,IY) = VX(IX,IY)*RETARD J 670
VX2 = VX(IX,IY)*VX(IX,IY) J 680
IF (VX2.GT.VMAX) VMAX = VX2 J 690
C ---Y-DIRECTION--- J 700
VY(IX,IY) = VY(IX,IY)*RETARD J 710
VY2 = VY(IX,IY)*VY(IX,IY) J 720
IF (VY2.GT.VMAX) VMAX = VY2 J 730
C -----VELOCITIES AT CELL BOUNDARIES----- J 740
VXBDY(IX,IY) = VXBDY(IX,IY)*RETARD J 750
VX2 = VXBDY(IX,IY)*VXBDY(IX,IY) J 760
IF (VX2.GT.VMAX) VMAX = VX2 J 770
VYBDY(IX,IY) = VYBDY(IX,IY)*RETARD J 780
VY2 = VYBDY(IX,IY)*VYBDY(IX,IY) J 790
IF (VY2.GT.VMAX) VMAX = VY2 J 800
RATE = -REC(IX,IY)/AREA J 810
SLEAK = (WT(IX,IY)-HK(IX,IY))*VPRM(IX,IY) J 820
DIV = RATE+SLEAK-RECH(IX,IY) J 830
IF (DIV.LE.0.0) GO TO 50 J 840
RTDIV = DIV/(POROS*THCK(IX,IY)) J 850
IF (RTDIV.LT.TDIV) GO TO 50 J 860
TDIV = RTDIV J 870
IXQMAX = IX J 880
IYQMAX = IY J 890
50 CONTINUE J 900
IF (BETA.EQ.0.0) GO TO 100 J 910
C ***** J 920
C ---COMPUTE DISPERSION COEFFICIENTS--- J 930
ALPHA=BETA J 940
ALNG=ALPHA J 950
TRAN=DLTRAT*ALPHA J 960
XX2=XDEL*XDEL J 970
YY2=YDEL*YDEL J 980
XY2=4.0*XDEL*YDEL J 990
DO 70 IX=2,NNX J1000
DO 70 IY=2,NNY J1010
IF (THCK(IX,IY).EQ.0.0) GO TO 70 J1020
VXE=VXBDY(IX,IY) J1030
VYS=VYBDY(IX,IY) J1040
IF (THCK(IX+1,IY).EQ.0.0) GO TO 60 J1050
C ---FORWARD COEFFICIENTS: X-DIRECTION--- J1060
VYE=(VYBDY(IX,IY-1)+VYBDY(IX+1,IY-1)+VYS+VYBDY(IX+1,IY))/4.0 J1070
VXE2=VXE*VXE J1080
VYE2=VYE*VYE J1090
VMGE=SQRT(VXE2+VYE2) J1100
IF (VMGE.LT.1.0E-20) GO TO 60 J1110
DALN=ALNG*VMGE J1120
DTRN=TRAN*VMGE J1130
VMGE2=VMGE*VMGE J1140
C ---XX COEFFICIENT--- J1150
DISP(IX,IY,1)=(DALN*VXE2+DTRN*VYE2)/(VMGE2*XX2) J1160
C ---XY COEFFICIENT--- J1170
DISP(IX,IY,3)=(DALN-DTRN)*VXE*VYE/(VMGE2*XY2) J1180
C ---FORWARD COEFFICIENTS: Y-DIRECTION--- J1190
60 IF (THCK(IX,IY+1).EQ.0.0) GO TO 70 J1200
VXS=(VXBDY(IX-1,IY)+VXE+VXBDY(IX-1,IY+1)+VXBDY(IX,IY+1))/4.0 J1210

```

```

VYS2=VYS*VYS
VXS2=VXS*VXS
VMGS=SQRT(VXS2+VYS2)
IF (VMGS.LT.1.OE-20) GO TO 70
DALN=ALNG*VMGS
DTRN=TRAN*VMGS
VMGS2=VMGS*VMGS
C      ---YY COEFFICIENT---
DISP (IX,IY,2)=(DALN*VYS2+DTRN*VXS2)/(VMGS2*YY2)
C      ---YX COEFFICIENT---
DISP (IX,IY,4)=(DALN-DTRN)*VXS*VYS/(VMGS2*XY2)
70 CONTINUE
C      *****
C      ---ADJUST CROSS-PRODUCT TERMS FOR ZERO THICKNESS---
DO 80 IX=2,NNX
DO 80 IY=2,NNY
IF (THCK (IX,IY+1).EQ.O.O.OR.THCK (IX+1,IY+1).EQ.O.O.OR.THCK (IX,IY-1
1).EQ.O.O.OR.THCK (IX+1,IY-1).EQ.O.O) DISP (IX,IY,3)=O.O
IF (THCK (IX+1,IY).EQ.O.O.OR.THCK (IX+1,IY+1).EQ.O.O.OR.THCK (IX-1,IY
1).EQ.O.O.OR.THCK (IX-1,IY+1).EQ.O.O) DISP (IX,IY,4)=O.O
C      *****
C      ---CHECK FOR STABILITY OF EXPLICIT METHOD---
TDISP = DISP (IX,IY,1)+DISP (IX,IY,2)
80 IF (TDISP.GT.TDIS) TDIS = TDISP
C      *****
C      ---ADJUST DISP. EQUATION COEFFICIENTS FOR SATURATED THICKNESS---
DO 90 IX=2,NNX
DO 90 IY=2,NNY
IF (THCK (IX,IY).EQ.O.O) GO TO 90
BAVX=2.O*THCK (IX,IY)*THCK (IX+1,IY)/(THCK (IX,IY)+THCK (IX+1,IY))
BAVY=2.O*THCK (IX,IY)*THCK (IX,IY+1)/(THCK (IX,IY)+THCK (IX,IY+1))
DISP (IX,IY,1)=DISP (IX,IY,1)*BAVX
DISP (IX,IY,2)=DISP (IX,IY,2)*BAVY
DISP (IX,IY,3)=DISP (IX,IY,3)*BAVX
DISP (IX,IY,4)=DISP (IX,IY,4)*BAVY
90 CONTINUE
C      *****
C      ---COMPUTE NEXT TIME STEP---
100 VMAX = SQRT (VMAX)
RTADV = VMAX/(CELDIS*XDEL)
TDIS = 2.O*TDIS
RTMAX = AMAX1 (RTADV,TDIV,TDIS)
TIMV = 1.O/RTMAX
NMOVRM = TIMREM/TIMV + 1
TIMV = TIMREM/(1.O*NMOVRM)
NMOV = IMDV + NMOVRM
WRITE (6,6000) NMOVRM,N
IF (RTMAX.EQ.RTADV) WRITE (6,6010)
IF (RTMAX.EQ.TDIS) WRITE (6,6020)
IF (RTMAX.EQ.TDIV) WRITE (6,6030) IXQMAX,IYQMAX
RETURN
C      *****
C      -----OUTPUT FORMATS-----
C      *****
6000 FORMAT (1H1,10X,38HSTABILITY CRITERIA --- M.O.C. REQUIRES,I3,
154HADDITIONAL PARTICLE MOVES TO COMPLETE FLOW TIME STEP =,I3)
6010 FORMAT (1H1,10X,42HTHE LIMITING STABILITY CRITERION IS CELDIS)
6020 FORMAT (1H1,10X,40HTHE LIMITING STABILITY CRITERION IS BETA)
6030 FORMAT (1H1,10X,58HTHE LIMITING STABILITY CRITERION IS MAXIMUM INJ
1ECTION RATE//15X,35H MAX. INJECTION OCCURS IN CELL IX = ,I3,
2 6H IY = ,I3)
END

```

```

J1220
J1230
J1240
J1250
J1260
J1270
J1280
J1290
J1300
J1310
J1320
J1330
J1340
J1350
J1360
J1370
J1380
J1390
J1400
J1410
J1420
J1430
J1440
J1450
J1460
J1470
J1480
J1490
J1500
J1510
J1520
J1530
J1540
J1550
J1560
J1570
J1580
J1590
J1600
J1610
J1620
J1630
J1640
J1650
J1660
J1670
J1680
J1690
J1700
J1710
J1720
J1730
J1740
J1750
J1760
J1770
J1780
J1790
J1800
J1810
J1820
J1830-

```


**** TSO FOREGROUND HARDCOPY ****
 DSNAME=U11236C.KONIMOD.CNTL

(ISIP)

```

C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER
C $NOFLOATCALLS
C $STORAGE:2
  SUBROUTINE ISIP
  DOUBLE PRECISION DMIN1,DABS,XI
  CHARACTER*8 TITLE
  REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT
  REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
  REAL*8 DXINV,DYINV,ARINV,PORINV
  REAL*8 HJ
  REAL*8 A,C,E,F,D,TBAR,COEF,CHK,QL,CH,GH,EH,HH,ALF,BET,GAM,W
  INTEGER FCON
  COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO
1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N
2PNCHV,NPDEL,ICLK,FCON,IHEAD,ISOLV
  COMMON /PRMC/ NODEID(20,20),NPCELL(20,20),NPOLD(20,20),LIMBO(500),
1IXOBS(5),IYOBS(5)
  2,NDECAY,NSORB
  COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR
1,THICK(20,20)
  COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20,
120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T
2ITITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
3,HJ(20,20)
  COMMON /BALM/ TOTLQ,TOTLQI,TPIN,TPOUT,TPQR
  COMMON /XINV/ DXINV,DYINV,ARINV,PORINV
  DIMENSION DEL(20,20),ETA(20,20),XI(20,20),V(20,20)
C *****
  LENGTH=10
  KOUNT=0
  PQIN = 0.0
  PQOUT = 0.0
  PQR = 0.0
  I2=NX-2
  J2=NY-2
  DO 35 I=1,NX
  DO 35 J=1,NY
  35 HJ(I,J)=HK(I,J)
C *****
C ---TERMINATE PROGRAM -- ITMAX EXCEEDED---
  40 IF (KOUNT.LE.ITMAX) GO TO 50
  WRITE (6,360)
  DO 45 J=1,NY
  DO 45 I=1,NX
  45 HK(I,J)=HJ(I,J)
  CALL OUTPT
  STOP
C *****
C ---INITIALIZE DATA FOR A NEW ITERATION---
  50 IF (MOD(KOUNT,LENGTH)) 60,60,70
  60 NTH=0
  70 NTH=NTH+1
  W=AOPT(NTH)
  BIGI=0.0
  TEST=0.0
C *****
C ---INITIALIZE SIP PARAMETERS---
  DO 80 I=1,NX
  DO 80 J=1,NY
  DEL(I,J)=0.
  ETA(I,J)=0.
  V(I,J)=0.

```

```

80 XI(I,J)=0. K 560
   KOUNT=KOUNT+1 K 570
   RHO=S/TIM(N) K 580
C ***** K 590
C ---CHOOSE SIP NORMAL OR REVERSE ALGORITHM--- K 600
   IF (MOD(KOUNT,2)) 100,240,100 K 610
100 DO 210 J=2,NNY K 620
   DO 210 I=2,NNX K 630
   IF (THCK(I,J).EQ.O.) GO TO 210 K 640
   COEF=VPRM(I,J) K 650
   QL=-COEF*WT(I,J) K 660
   A=TMRX(I-1,J,1)*DXINV K 670
   C=TMRX(I,J,1)*DXINV K 680
   E=TMRX(I,J-1,2)*DYINV K 690
   F=TMRX(I,J,2)*DYINV K 700
   TBAR=-E-A-C-F-RHO-COEF K 710
   HH=DEL(I,J-1)*E/(1.+W*DEL(I,J-1)) K 720
   GH=ETA(I-1,J)*A/(1.+W*ETA(I-1,J)) K 730
   EH=E-W*HH K 740
   AH=A-W*GH K 750
   TBARH=TBAR+W*HH+W*GH K 760
   CH=C-W*HH K 770
   FH=F-W*GH K 780
   ALF=EH K 790
   BET=AH K 800
   GAM=TBARH-ALF*ETA(I,J-1)-BET*DEL(I-1,J) K 810
   DEL(I,J)=CH/GAM K 820
   ETA(I,J)=FH/GAM K 830
   D=-A*HJ(I-1,J)-C*HJ(I+1,J)-F*HJ(I,J+1)-E*HJ(I,J-1)-TBAR*HJ(I,J)- K 840
1   RHO*HK(I,J)+QL+RECH(I,J)+REC(I,J)*ARINV K 850
   V(I,J)=(D*1.OO-ALF*V(I,J-1)-BET*V(I-1,J))/GAM K 860
210 CONTINUE K 870
C ***** K 880
C ---BACK SUBSTITUTION FOR VECTOR XI--- K 890
   DO 220 I=1,I2 K 900
   I3=NX-I K 910
   DO 220 J=1,J2 K 920
   J3=NY-J K 930
   IF (THCK(I3,J3).EQ.O.O) GO TO 220 K 940
   XI(I3,J3)=V(I3,J3)-(DEL(I3,J3)*XI(I3+1,J3)+ETA(I3,J3)*XI(I3,J3+1)) K 950
220 CONTINUE K 960
C ***** K 970
C ---COMPUTE MAGNITUDE OF CHANGE WITH CLOSURE CRITERION--- K 980
   DO 230 J=2,NNY K 990
   DO 230 I=2,NNX K 1000
   CHK=DABS(XI(I,J)) K 1010
   IF (CHK.GT.BIGI) BIGI=CHK K 1020
   IF (BIGI.GT.TOL) TEST=1. K 1030
230 HJ(I,J)=HJ(I,J)+XI(I,J) K 1040
   IF (TEST.EQ.1.O.AND.KOUNT.LT.ITMAX)GO TO 40 K 1050
   GO TO 280 K 1060
C ***** K 1070
C ---SIP REVERSE ALGORITHM--- K 1080
240 DO 250 JJ=1,J2 K 1090
   J=NY-JJ K 1100
   DO 250 I=2,NNX K 1110
   IF (THCK(I,J).EQ.O.O)GO TO 250 K 1120
   COEF=VPRM(I,J) K 1130
   QL=-COEF*WT(I,J) K 1140
   A=TMRX(I-1,J,1)*DXINV K 1150
   C=TMRX(I,J,1)*DXINV K 1160
   E=TMRX(I,J-1,2)*DYINV K 1170
   F=TMRX(I,J,2)*DYINV K 1180
C ***** K 1190
C ---COMPUTE INTERMEDIATE VECTORS-FORWARD SUBSTITUTION--- K 1200
   TBAR=-E-A-C-F-RHO-COEF K 1210

```

```

HH=DEL(I,J+1)*F/(1.+W*DEL(I,J+1))
GH=ETA(I-1,J)*A/(1.+W*ETA(I-1,J))
EH=F-W*HH
AH=A-W*GH
TBARH=TBAR+W*HH+W*GH
CH=C-W*HH
FH=E-W*GH
ALF=EH
BET=AH
GAM=TBARH-ALF*ETA(I,J+1)-BET*DEL(I-1,J)
DEL(I,J)=CH/GAM
ETA(I,J)=FH/GAM
D=-A*HJ(I-1,J)-C*HJ(I+1,J)-F*HJ(I,J+1)-E*HJ(I,J-1)-TBAR*HJ(I,J)-
1 RHO*HK(I,J)+QL+RECH(I,J)+REC(I,J)*ARINV
V(I,J)=(D*1.00-ALF*V(I,J+1)-BET*V(I-1,J))/GAM
250 CONTINUE
C *****
C ---BACKWARD SUBSTITUTION FOR VECTOR XI---
DO 260 J3=2,NNY
DO 260 I=1,I2
I3=NX-I
XI(I3,J3)=V(I3,J3)-(DEL(I3,J3)*XI(I3+1,J3)+ETA(I3,J3)*XI(I3,J3-1))
260 CONTINUE
C *****
C ---COMPARE MAGNITUDE OF CHANGE WITH CLOSURE CRITERION---
DO 270 J=2,NNY
DO 270 I=2,NNX
CHK=DABS(XI(I,J))
IF (CHK.GT.BIGI) BIGI=CHK
270 HJ(I,J)=HJ(I,J)+XI(I,J)
IF (BIGI.GT.TOL) TEST=1.
IF (TEST.EQ.1.O.AND.KOUNT.LT.ITMAX) GO TO 40
280 CONTINUE
DO 300 J=1,NY
DO 300 I=1,NX
IF (THCK(I,J).EQ.O.O) GO TO 300
HK(I,J)=HJ(I,J)
IF (REC(I,J).GT.O.O) GO TO 232
PQIN=PQIN+REC(I,J)
GO TO 234
232 PQOUT=PQOUT+REC(I,J)
234 IF (RECH(I,J).GT.O.O) GO TO 236
PQR=PQR + RECH(I,J)*AREA
GO TO 238
236 PQOUT=PQOUT+RECH(I,J)*AREA
238 CONTINUE
C *****
C ---COMPUTE LEAKANCE FOR MASS BALANCE---
IF (VPRM(I,J).EQ.O.O) GO TO 300
DELQ=-VPRM(I,J)*AREA*(WT(I,J)-HK(I,J))
IF (DELQ.LE.O.O) GO TO 290
TOTLQ=TOTLQ+DELQ*TIM(N)
GO TO 300
290 TOTLQI=TOTLQI+DELQ*TIM(N)
300 CONTINUE
TPIN=TPIN+PQIN*TIM(N)
TPQR= TPQR+PQR*TIM(N)
TPOUT=TPOUT+PQOUT*TIM(N)
C *****
WRITE (6,370) N
WRITE (6,390) KOUNT
C *****
RETURN
C *****
360 FORMAT (1H0,5X,64H*** EXECUTION TERMINATED -- MAX. NO. ITERATION
1S EXCEEDED ***/26X,21HFINAL OUTPUT FOLLOWS:)

```

```
370 FORMAT(1H0//3X,4HN = ,1I4)
390 FORMAT (1H ,2X,23HNUMBER OF ITERATIONS = ,1I4)
400 FORMAT (1H0,10E12.7)
END
```

```
K1880
K1890
K1900
K1910-
```

**** TSO FOREGROUND HARDCOPY ****
 DSNAME=U11236C.KONIMOD.CNTL

(GRPH)

```

C USE META COMMANDS (BELOW) WHEN COMPILED ON MICROCOMPUTER
C $NOFLOATCALLS
C $STORAGE:2
  SUBROUTINE GRPH
  CHARACTER*8 TITLE
  REAL*8 TMRX,VPRM,HI,HR,HC,HK,WT,REC,RECH,TIM,AOPT
  REAL*8 XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
  REAL*8 HJ
  INTEGER FCON
  COMMON /PRMI/ NTIM,NPMP,NPNT,NITP,N,NX,NY,NP,NREC,INT,NNX,NNY,NUMO
1BS,NMOV,IMOV,NPMAX,ITMAX,NZCRIT,IPRNT,NPTPND,NPNTMV,NPNTVL,NPNTD,N
2PNCHV,NPDEL,C,ICLK,FCON,IHEAD,ISOLV
  COMMON /HEDA/ THCK(20,20),PERM(20,20),TMWL(5,50),TMOBS(50),ANFCTR
1,THICK(20,20)
  COMMON /HEDB/ TMRX(20,20,2),VPRM(20,20),HI(20,20),HR(20,20),HC(20,
120),HK(20,20),WT(20,20),REC(20,20),RECH(20,20),TIM(100),AOPT(20),T
2ITITLE(10),XDEL,YDEL,S,AREA,SUMT,RHO,PARAM,TEST,TOL,PINT,HMIN,PYR
3,HJ(20,20)
  COMMON /CHMA/ PART(3,3200),CONC(20,20),TMCN(5,50),VX(20,20),VY(20,
120),CONINT(20,20),CNRECH(20,20),PORDS,SUMTCH,BETA,TIMV,STORM,STORM
2I,CMSIN,CMSOUT,FLMIN,FLMOT,SUMIO,CELDIS,DLTRAT,CSTORM
3,DCYLAM,BLKDEN,SRBRAT,SRBSAT,SRBALF,VOLDCY,VOLSRB,SRBDCY
  REAL*8 IH(20)
  DIMENSION TRANS(20)
  *****
C TIMD=SUMT/86400.
  TIMY=SUMT/(86400.0*365.25)
C ---PRINT HEAD MAP---
  WRITE (10,200) INT,N
  WRITE (10,210) INT,N,SUMT,TIMD,TIMY
  DO 20 IY=1,NY
  DO 20 IX=1,NX
  IH(IX)=HI(IX,IY) - HK(IX,IY) + 0.5
  TRANS(IX)=PERM(IX,IY)*THCK(IX,IY)
  20 WRITE (10,220) INT,N,IX,IY,
  1 HK(IX,IY),IH(IX),THCK(IX,IY),TRANS(IX),CONC(IX,IY)
C *****
  RETURN
C *****
  200 FORMAT (1H ,2I4)
  210 FORMAT (1H ,2I4,1P3E12.5)
  220 FORMAT (1H ,4I4,3F10.4,E10.2,F10.4)
  END
  L 10
  L 11
  L 20
  L 30
  L 40
  L 41
  L 50
  L 60
  L 70
  L 80
  L 90
  L 100
  L 110
  L 120
  L 130
  L 140
  L 150
  L 160
  L 170
  L 171
  L 180
  L 190
  L 200
  L 210
  L 220
  L 230
  L 240
  L 250
  L 260
  L 270
  L 280
  L 290
  L 300
  L 310
  L 320
  L 330
  L 340
  L 350
  L 360
  L 370-

```

APPENDIX II
FORTRAN IV PROGRAM CHANGES

APPENDIX II-A
GLOBAL DECLARATIONS AND
NAMED COMMON BLOCKS

Delete and insert the following Fortran statements to implement the modifications described in this report.

Global Declarations

Insert the following Fortran statements:

REAL*8 HJ

as lines:

A 117	D 34	G 45	J 45
B 61	E 55	H 35	
C 46	F 33	I 35	

CHARACTER*8 TITLE

as lines:

A 71	D 11	G 11	J 11
B 21	E 11	H 11	
C 11	F 11	I 11	

INTEGER FCON

as lines:

A 118	D 36	G 46	J 46
B 68	E 56	H 36	
C 51	F 36	I 36	

Named Common, PRMI

Delete:

A 141	D 61	G 71	J 70
B 91	E 81	H 61	
C 81	F 61	I 61	

Insert the Fortran statement:

2PNCHV, NPDELC, ICHK, FCON, IHEAD, ISOLV

as lines:

A 142	D 62	G 72	J 71
B 92	E 82	H 62	
C 82	F 62	I 62	

Named Common, HEDA

No deletions.

Insert the Fortran statement:

1, THICK(60, 60)

as lines:

A 171	D 91	G 101	J 111
B 121	E 111	H 91	
C 111	F 91	I 91	

Named Common, HEDB

No deletions.

Insert the statement:

3, HJ(60, 60)

as lines:

A 205	D 125	G 135	J 145
B 155	E 145	H 125	
C 145	F 125	I 125	

Named Common, BALM

Delete:

B 186	C 146	H 126
-------	-------	-------

Insert the statement:

COMMON /BALM/ TOTLQ, TOTLQI, TPIN, TPOUT, TPQR

as lines:

B 187	C 147	H 127
-------	-------	-------

APPENDIX II-8
STRONGLY IMPLICIT PROCEDURE

Main Program

To implement the subroutine ISIP the following lines were added to the Main program.

Insert:

A 436-A 439

Subroutine PARLOD

To add the subroutine ISIP, modifications to the subroutine PARLOD are indicated below.

Delete:

B2960 B3960-B3970

Insert:

B 211	B 585	B2902	B3891B
B 212	B 586	B2951A-B2968B	B3965-B3975
B 465	B2872	B3891A	

SIP iteration parameters are calculated in lines B2952B through B2968B. Line B465 reads the values for all of the integer flags that have been added to implement the modifications described in this report.

APPENDIX II-C
TRANSMISSIVITY

Main Program

In this part of the program, updating of the transmissivities (for an unconfined aquifer) after every time step is performed by the changes indicated below.

Insert:

A 441A-A 450C

Subroutine PARLOD

Line B65 is replaced with line B67 to facilitate the declaration of flag TP as an integer. TP dictates whether the input is transmissivity or hydraulic conductivity. TP and FCON are also read in line B465 as stated in Appendix II-B.

All lines that have been deleted and added in subroutine PARLOD to incorporate transmissivity updating and either transmissivity or hydraulic conductivity input options are listed below.

Delete:

B 65	B2010	B2050-B2170	B2250
B1631-B1910			

Insert:

B 67	B 971	B2011	B2271 -B2276
B 465	B1491	B2021	B2351A-B2359C
B 588	B1611	B2252	B3891D-B3891E
B 589	B1632	B2254	

Subroutine OUTPT

This subroutine was modified as illustrated below to print the updated transmissivity and saturated thickness when an unconfined aquifer is being modeled.

Insert:

H 711-H 729 H1192-H1198

APPENDIX II-D
HYDRAULIC HEAD SIMULATION

Main Program

The changes made to the main program are indicated below.

Delete:

A 280 A 680

Insert:

A 281 A 452 A 615 A 681

Subroutine PARLOD

The flag IHEAD is read in line B465 as stated in Appendix II-B. Other changes are listed below.

Insert:

B 587 B3891C

APPENDIX II-E

MASS BALANCE

Subroutine PARLOD

Insert:

B 301

Subroutine ITERAT /

The changes to this subroutine are listed below.

Delete:

C1187 C1210 C1215

Insert:

C 194 C1211 C1216 C1232A
C1187A

Subroutine OUTPT

The modifications made to in this subroutine for mass balance modifications are listed below.

Delete:

H 574 H 721 H1096 H1103
H 716 H 755

Insert:

H 501 H 740 H 766 H 887
H 575 H 757 H 841 H1095-H1110
H 730

APPENDIX II-F
SATURATED THICKNESS

Subroutine PARLOD

Line B65 is replaced with line B67 (as previously described in Appendix II-C) to facilitate the declaration of the integer flag BTM. BTM is also read in line B465 as stated in Appendix II-B. All changes made to PARLOD to incorporate the input of either saturated thickness or bottom elevation for an unconfined aquifer are listed below.

Delete:

B65	B1940	B2630-B2750
-----	-------	-------------

Insert:

B 67	B1942-B1944	B3162-B3168	B3891F
B465	B2041-B2146	B3435	B4212 -B4214
B589A			

APPENDIX II-G
ADDITIONAL MODIFICATIONS

Main Program

To implement the subroutine GRPH, the following lines were added to the main program.

Insert:

A 266	A 620	A 662-A 664	A 725
A 321			

Subroutine PARLOD

Delete:

B2270	B3590	B3810	B3895
B3460			

Insert:

B 212A	B1235	B3461	B3900
B 265	B1395	B3591	B3925
B 564-B 565	B2022	B3685	B3945
B 640	B2256	B3811	B4125
B 700	B2585	B3815	B4191-4192
B 755	B2761-B2764	B3895	B4525
B 962-B 964	B3151		

Subroutine CHMOT

Insert:

I 344-I 349	I1125	I1295	I1535
-------------	-------	-------	-------

APPENDIX III

DEFINITION OF SELECTED FORTRAN IV PROGRAM VARIABLES

BTM An integer flag used to indicate low saturated thickness is input. For input of saturated thickness, BTM must equal zero. For input of bottom elevation, BTM must equal 1. BTM equals zero if FCON equals zero.

DEL Two dimensional array used in the SIP normal and reverse algorithms for forward substitution.

ETA Two dimensional array used in the SIP normal and reverse algorithms for forward substitution.

FCON An integer flag used to indicate the option of simulating confined or unconfined aquifer. For confined aquifer simulation, FCON must be equal to zero and for an unconfined aquifer simulation, FCON must be equal to 1.

HJ A two dimensional array used for temporary storage of hydraulic head in subroutine ISIP (ft).

IHEAD An integer flag used to indicate whether the simulation is only for hydraulic head or for solute transport. For only the hydraulic head simulation, IHEAD must be equal to 1 and for solute transport simulation, IHEAD must be equal to zero.

IORDER Vector that indicates the order of the iteration parameters used in the SIP algorithm.

ISOLV This is an integer flag used to implement the option for different solution algorithms for flow equation. To use ADIP algorithm, ISOLV must be equal to zero and for SIP algorithm, ISOLV must be equal to 1.

LENGTH Number of iteration parameters in SIP algorithm.

PQR Rate of recharge from the distributed source to the aquifer (ft³/sec).

TEMP Vector for arranging the SIP iteration parameters in geometric sequence.

THICK A two dimensional array used in the main program to update aquifer thickness for unconfined aquifer (ft).

TP TP is an integer flag to indicate the option of inputting the hydraulic conductivity or transmissivity as an input variable. For transmissivity, TP must be equal to zero and for hydraulic conductivity, TP must be equal to 1.

TPQR Total amount of recharge to the aquifer from distributed sources during the simulation period (ft³).

V Two dimensional array used in SIP normal and reverse algorithms for forward substitution.

- XI** Two dimensional array containing incremental head values in SIP solution, during backward substitution. If XI is less than or equal to the prespecified value for convergence, the iteration process will be stopped and the convergence is achieved (ft).
- W** Iteration parameter used in SIP algorithm.

APPENDIX IV
ADDITIONAL DATA REQUIREMENTS

Five variables have been added for the modifications made to the NRC version of the USGS Solute Transport Model. These variables allow for (a) the choice of the iterative techniques to be used when solving the groundwater equation, (b) the type of simulation (transport or head only), (c) the type of aquifer, (d) the input of either transmissivity or hydraulic conductivity, and (e) the input of either saturated thickness or bottom elevation for an unconfined aquifer. The data is contained on Data Card 5; the input formats are given in Appendix IV, page IV-5. The definition of the variables are:

ISOLV = 0 ADIP -- Alternating-Direction Implicit Procedure
 = 1 SIP -- Strongly Implicit Procedure

IHEAD = 0 Transport simulation
 = 1 Head only simulation

FCOM = 0 Confined aquifer
 = 1 Unconfined aquifer

TP = 0 Transmissivity input
 = 1 Hydraulic Conductivity input

BTM = 0 Saturated Thickness input
 = 1 Bottom Elevation input

APPENDIX V
DATA DEFINITIONS AND INPUT FORMATS

Card Image	Column	Format	Variable	Definition
1	1-80	10A8	TITLE	Description of problem
2	1- 4	I4	NTIM	Maximum number of time steps in a pumping period (limit=100)*.
	5- 8	I4	NPMP	Number of pumping periods. Note that if NPMP>1, then data set 10 must be completed. (limit=20)*.
	9-12	I4	NX	Number of nodes in x direction (limit=20)*.
	13-16	I4	NY	Number of nodes in y direction (limit=20)*.
	17-20	I4	NPMAX	Maximum number of particles (limit=3200)*.
	21-24	I4	NPNT	Time-step interval for printing hydraulic and chemical output data.
	25-28	I4	NITP	Number of iteration parameters (usually 4<=NITP<=7).
	29-32	I4	NUMOBS	Number of observation points to be specified in a following data set (limit=5)*.
	33-36	I4	ITMAX	Maximum allowable number of iterations in ADIP or SIP (usually 100 <=ITMAX<=200).
	37-40	I4	NREC	Number of pumping or injection wells to be specified in a following data set (limit=50)*.
	41-44	I4	NPTPND	Initial number of particles per node (options=4,5,8,9).
	45-48	I4	NCODES	Number of node identification codes to be specified in a following data set (limit=10)*.

Card Image	Column	Format	Variable	Definition
	49-52	I4	NPNTMV	Particle movement interval (IMOV) for printing chemical output data. (Specify 0 to print only at end of time steps).
	53-56	I4	NPNTVL	Option for printing computed velocities (0=do not print; 1=print for first time step; 2=print for all time steps).
	57-60	I4	NPNTD	Option for printing computed dispersion equation coefficients (option definition same as for NPNTVL).
	61-64	I4	NPDELC	Option for printing computed changes in concentration (0=do not print; 1=print).
	65-68	I4	NPNCHV	Option to punch velocity data (option definition same as for NPNTVL). When specified, program will punch on unit 7 the velocities at nodes.
3	1- 5	G5.0	PINT	Pumping period in years.
	6-10	G5.0	TOL	Convergence criteria in ADIP (usually $TOL \leq 0.01$).
	11-15	G5.0	POROS	Effective porosity.
	16-20	G5.0	BETA	Characteristic length, in feet (=longitudinal dispersivity).
	21-25	G5.0	S	Storage coefficient (set S=0 for steady flow problems).
	26-30	G5.0	TIMX	Time increment multiplier for transient flow problems. TIMX is disregarded if S=0.
	31-35	G5.0	TINIT	Size of initial time step in seconds. TINIT is disregarded if S=0.

Card Image	Column	Format	Variable	Definition
	36-40	G5.0	XDEL	Width of finite-difference cell in x direction, in feet.
	41-45	G5.0	YDEL	Width in finite-difference cell in y direction, in feet.
	46-50	G5.0	DLTRAT	Ratio of transverse to longitudinal dispersivity.
	51-55	G5.0	CELDIS	Maximum cell distance per particle move (value between 0 and 1.0).
	56-60	G5.0	ANFCTR	Ratio of Transmissivity tensors for anisotropic site (T(yy) to T(xx)).
4	1- 5	I5	NDECAY	If NDECAY=1 decay will be simulated, if NDECAY=0 decay will not be simulated.
	6-10	I5	NSORB	If NSORB=1 sorption will be simulated using a linear solver, if NSORB=2 sorption will be simulated using the Langmuir solver, if NSORB=3 sorption will be simulated using the Freundlich solver, if NSORB=0 sorption will not be simulated.
	11-20	F10.0	DCYTIN	If NDECAY=1, DCYTIN=decay half life, in years. If NDECAY=0, DCYTIN=0.
	21-30	F10.0	DENROCK	If NSORB=1,2, or 3, DENROCK=density of aquifer in gm/cm ³ . If NSORB=0, DENROC=0.
	31-40	F10.0	SORBQR	If NSORB=1,2, OR 3, SORBQR is the value of Kd, in ml/g. If NSORB=0, SORBQR=0.
	41-50	F10.0	SORBST	If NSORB=2, SORBST is the sorbtion saturation value for the Langmuir solver. If NSORB=0, 1, or 3, SORBST=0.

Card Image	Column	Format	Variable	Definition
	51-60	F10.0	SORBAL	If NSORB=3, SORBAL is the value of alpha for the Freundlich isotherm, if NSORB=0,1, or 2, SORBAL=0.
5	1- 4	I4	ISOLV	ISOLV=0 for ADIP algorithm and ISOLV=1 for SIP algorithm.
	5- 8	I4	IHEAD	IHEAD=0 for solute transport simulation. IHEAD=1 for only head simulation.
	9-12	I4	FCON	FCON=0 for confined aquifer simulation. FCON=1 for unconfined aquifer simulation.
	13-16	I4	TP	TP=1 for hydraulic conductivity input. TP=0 for transmissivity input.
	17-20	I4	BTM	BTM=1 for bottom elevation input (unconfined aquifer simulation). BTM=0 for saturated thickness input. (BTM=0 if FCON=0.)

See footnotes at end of table.

Data set	Number of card images	Format	Variable	Definition
1	Value of NUMOBS (limit=5)*	2I2	IXOBS, IYOBS	x and y coordinates of observation points. This data set is eliminated if NUMOBS is specified as =0.
2	Value of NREC (limit=50)*	2I2, 2G8.2	IX, IY, REC, CNRECH	x and y coordinates of pumping (+) or injection (-) wells, rate in ft ³ /s, and if an injection well, the concentration of injected water. This data set is eliminated if NREC=0.
3	a.1 b. Value of NY times the ceiling of NX/20 (limit=20)*	I1, G10.0 20G4.1	INPUT, FCTR ** VPRM	Parameter card for transmissivity or hydraulic conductivity. If TP=0, array for temporary storage of transmissivity data, in ft ² /s. If TP=1, array for temporary storage of hydraulic conductivity data, in ft/s. For an anisotropic aquifer, read in values of T(xx) and the program will adjust for anisotropy by multiplying T(yy) by ANFCTR.

Data set	Number of card images	Format	Variable	Definition
4	a.1 b. Value of NY times the ceiling of NX/26 (limit=20)*	I1, G10.0 26G3.0	INPUT, FCTR ** THCK	Parameter card for THICK. Saturated thickness or bottom elevation of aquifer, in feet. If BTM=0, array for storage of saturated thickness. If BTM=1, array for temporary storage of bottom elevation.
5	a.1 b. Value of NY times the ceiling of NX/20 (limit=20)*	I1, G10.0 20G4.0	INPUT, FCTR ** WT	Parameter card for WT. Initial water-table or potentiometric elevation, or constant head in stream or source bed.
6	a.1 b. Value of NY times the ceiling of NX/20 (limit=20)*	I1, G10.0 20G4.1	INPUT, FCTR ** RECH	Parameter card for RECH. Diffuse recharge (-) or discharge (+), in ft/s.
7	a.1 b. Value of NY (limit=20)*	I1, G10.0 60I1	INPUT, FCTR ** NODEID	Parameter card for NODEID. Node identification matrix (used to define constant-head nodes or other boundary conditions and stresses).

Data set	Number of card images	Format	Variable	Definition
8	Value of NCODES (limit=10)*	I2, 3G10.2 I2	ICODE, FCTR1, FCTR2, FCTR3, OVERRD	Instructions for using NODEID array. When NODEID=ICODE, program sets leakance=FCTR1, CNRECH=FCTR2, and if OVERRD is nonzero, RECH=FCTR3. Set OVERRD=0 to preserve values of RECH specified in data set 5.
9	a.1 b. Value of NY times the ceiling of NX/20 (limit=20)*	I1, G10.0 20G4.0	INPUT, FCTR ** CONC	Parameter card for CONC. Initial concentration in aquifer.
10				This data set allows time step parameters, print options, and pumpage data to be revised for each pumping period of the simulation. Data set 10 is only used if NPMP >1. The sequence of cards in data set 10 must be repeated (NPMP -1) times (that is, data set 10 is required for each pumping period after the first).

Data set	Number of card images	Format	Variable	Definition
a.1		I1	ICLK	Parameter to check whether any revisions are desired. Set ICHK=1 if data are to be revised, and then complete data set 10b and c. Set ICHK=0 if data are not to be revised for the next pumping period, and skip rest of data set 10.
b.1		10I4, 3G5.0	NTIM, NPNT, NITP, ITMAX, NREC, NPNTMV, NPNTVL, NPNTD, NPNDEL, NPNCHV, PINT, TIMX, TINIT	Thirteen parameters to be revised for next pumping period; the parameters were previously defined in the description of data cards 2 and 3. Only include this card if ICHK=1 in previous part a.
c. Value of NREC ++ (limit=50)*		2I2, 2G8.2	IX, IY, REC, CNRECH	Revision of previously defined data set 2. Include part c only if ICHK=1 in previous part a and if NREC>0 in previous part b.

- *These limits can be modified if necessary by changing the corresponding array dimensions in the COMMON statements of the program.
- **Any wells set during one pumping period continue pumping and injecting during subsequent pumping periods unless the rates are explicitly reset in those subsequent periods.
- **The parameter card must be the first card of the indicated data sets. It is used to specify whether the parameter is constant and uniform, and can be defined by one value, or whether it varies in space and must be defined at each node. If INPUT=0, the data set has a constant value, which is defined by FCTR. If INPUT=1, the data set is read from cards as described by part b. Then FCTR is a multiplication factor for the values read in the data set.

APPENDIX VI
UNITS SUMMARY TABLE

<u>VARIABLE</u>	<u>FIELD UNITS</u>	<u>CONVERSION</u>	<u>MODEL UNITS</u>
NTIM	-	-	(limit=100)+
NPMP	-	-	-
NX	-	-	(limit=60)+
NY	-	-	(limit=60)+
NPMAX	-	-	(limit=9850)+
NPNT	-	-	-
NITP	-	-	-
NUMOBS	-	-	(limit=5)+
ITMAX	-	-	-
NREC	-	-	-
NPTPND	-	-	-
NCODES	-	-	-
NPNTMV	-	-	-
NPNTVL	-	-	-
NPNTD	-	-	-
NPDEL	-	-	-
NPCHV	-	-	-
PINT	yrs	-	yrs
TOL	-	-	-
POROS	-	-	-
BETA	-	-	-
S	percent	-	percent
TIMX	-	-	-
TINIT	sec	-	sec
XDEL	ft	-	ft
YDEL	ft	-	ft
DLTRAT	ratio	-	ratio
CELDIS	-	-	betw 0 & 1.0
ANFCTR	ratio	-	ratio
DCYTIM	yrs	-	yrs
DENROCK	gm/cm3	-	gm/cm3
SORBOR	ml/g	-	ml/g
SORBST	-	-	-
SORBAL	-	-	-
ISOLV	-	-	-
IHEAD	-	-	-
FCOM	-	-	-
TP	-	-	-
IXOBS	-	-	-
IYOBS	-	-	-
IX	-	-	-
IY	-	-	-
REC	af/y	.001400463	ft3/s
CNRECH	mg/l	-	mg/l
VPRM	-	-	-
TRANS	gpd/ft	1.54723 E-6	ft2/s
or PERM	gpd/ft2	1.54723 E-6	ft/s
THCK	ft	-	ft
WT	ft	-	ft

<u>VARIABLE</u>	<u>FIELD</u> <u>UNITS</u>	*	<u>CONVERSION</u>	=	<u>MODEL</u> <u>UNITS</u>
RECH	in/yr		26.7918 E-10		ft/s
NODEID	-		-		-
FCTR1	(gpd/ft ²)/ft		1.54723 E-6		(ft/s)/ft
FCTR2	mg/l		-		mg/l
FCTR3	in/yr		26.7918 E-10		ft/s
OVERRD	-		-		-
CONC	mg/l		-		mg/l

+These limits may be modified by changing the corresponding array dimensions in the COMMON statements of the program.

APPENDIX VII

INPUT AND SELECTED OUTPUT FOR TEST PROBLEM 2

**** TSO FOREGROUND HARDCOPY ****
DSNAME=U11236D.EX3KB.CNTL

//M11236D JOB (?????,TSO-TR-KONI),KONIKOWRUN,
// TIME=(0,40),CLASS=A,
// MSGCLASS=X,NOTIFY=**
/*PASSWORD ????
/*JOBPARM ROOM=L
/*

//KONI EXEC PGM=KONI60G,REGION=1500K
//STEPLIB DD DISP=SHR,DSN=U11236D.KONI.LOAD
//FT06FOO1 DD DSN=U11236D.EX3KB.OUTLIST,UNIT=STORAGE,
// SPACE=(TRK,(10,10)),DISP=(MOD,CATLG),
// DCB=(RECFM=VBA,LRECL=133,BLKSIZE=7448)
//FT10FOO1 DD DSN=U11236D.EX3KB.GRAPH,UNIT=STORAGE,
// SPACE=(TRK,(10,10)),DISP=(MOD,CATLG),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=7440)
//FT07FOO1 DD SYSOUT=B
//FT05FOO1 DD *

TEST PROBLEM 2 FOR TRANSIENT SIMULATION WITH SIP OPTION

10	1	9	103200	1	10	2	100	1	9	2	10	1	0	0	0
2.5	0.01	.3	100.	.005		179.E5	900.	900.	.3	.5	1.				
0	0	0.		0.		0.		0.	0.		0.				

1 0 0 0 0
5 4
5 7
4 7 1. 0.0
0 0.1
0 20.
1 1

0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	100.	100.	100.	100.	100.	100.	100.	100.	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	75.	75.	75.	75.	75.	75.	75.	75.	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

0 0.
1 1
00000000
022111220
00000000
00000000
00000000
00000000
00000000
00000000
022222220
00000000

2	1.	0.	0. 0
1	1.	100.	0. 0
0	0		

U.S.G.S. METHOD-OF-CHARACTERISTICS MODEL FOR SOLUTE TRANSPORT IN GROUND WATER
 TEST PROBLEM 2 FOR TRANSIENT SIMULATION WITH SIP OPTION

INPUT DATA

GRID DESCRIPTORS

NX (NUMBER OF COLUMNS) = 9
 NY (NUMBER OF ROWS) = 10
 XDEL (X-DISTANCE IN FEET) = 300.0
 YDEL (Y-DISTANCE IN FEET) = 300.0

TIME PARAMETERS

NTIM (MAX. NO. OF TIME STEPS) = 10
 NPMP (NO. OF PUMPING PERIODS) = 1
 PINT (PUMPING PERIOD IN YEARS) = 2.500
 TIME (TIME INCREMENT MULTIPLIER) = 1.00
 TINIT (INITIAL TIME STEP IN SEC.) = 0.79E+07

HYDROLOGIC AND CHEMICAL PARAMETERS

S (STORAGE COEFFICIENT) = 0.005000
 POROS (EFFECTIVE POROSITY) = 0.30
 BETA (CHARACTERISTIC LENGTH) = 100.0
 DLTRAT (RATIO OF TRANSVERSE TO LONGITUDINAL DISPERSIVITY) = 0.30
 ANFCR (RATIO OF T-YY TO T-XX) = 1.000000

NON-DECAYING SPECIES

NON-SORBING SPECIES

SIP USED

CONFINED AQUIFER

EXECUTION PARAMETERS

NITP (NO. OF ITERATION PARAMETERS) = 10
 TOL (CONVERGENCE CRITERIA - ADIP) = 0.0100
 ITMAX (MAX. NO. OF ITERATIONS - ADIP) = 100
 CELDIS (MAX. CELL DISTANCE PER MOVE OF PARTICLES - M.O.C.) = 0.500
 NPMAX (MAX. NO. OF PARTICLES) = 3200
 NPTRND (NO. PARTICLES PER NODE) = 8

PROGRAM OPTIONS

NPNT (TIME STEP INTERVAL FOR COMPLETE PRINTOUT) = 1
 NPNTMV (MOVE INTERVAL FOR CHEM. CONCENTRATION PRINTOUT) = 10
 NPNTVL (PRINT OPTION-VELOCITY) = 1
 0=NO; 1=FIRST TIME STEP; 2=ALL TIME STEPS
 NPNTD (PRINT OPTION-DISP. COEF.) = 0
 0=NO; 1=FIRST TIME STEP; 2=ALL TIME STEPS
 NUMOBS (NO. OF OBSERVATION WELLS FOR HYDROGRAPH PRINTOUT) = 2
 NREC (NO. OF PUMPING WELLS) = 1
 NCODES (FOR NODE IDENT.) = 2
 NPNCHV (PUNCH VELOCITIES) = 0
 NPDEL (PRINT OPT.-CONC. CHANGE) = 0

TIME INTERVALS (IN SECONDS)

0.79000E+07 0.79000E+07 0.79000E+07 0.79000E+07 0.79000E+07 0.79000E+07 0.79000E+07 0.79000E+07 0.79000E+07 0.79000E+07
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00

LOCATION OF OBSERVATION WELLS

NO.	X	Y
1	5	4
2	5	7

LOCATION OF PUMPING WELLS

X	Y	RATE (IN CPS)	CONC.
6	7	0.100E+01	0.00

AREA OF ONE CELL = 8.1000E+05

X-Y SPACING:
 300.00
 300.00

NODE IDENTIFICATION MAP

0	0	0	0	0	0	0	0	0
0	2	2	1	1	1	2	2	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	2	2	2	2	2	2	2	0
0	0	0	0	0	0	0	0	0

NO. OF NODE IDENT. CODES SPECIFIED : 2

THE FOLLOWING ASSIGNMENTS HAVE BEEN MADE:

CODE NO.	LEAKANCE	SOURCE CONC.	RECHARGE
2	1.000E+00	0.000E+00	
1	1.000E+00	1.000E+02	

VERTICAL PERMEABILITY/THICKNESS [FT/(FT*SEC)]

0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	0.00E+00
0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
0.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	1.00E+00	0.00E+00
0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

HEAD DISTRIBUTION - ROW

NUMBER OF TIME STEPS : 0
 TIME(SECONDS) : 0.00000E+00
 TIME(DAYS) : 0.00000E+00
 TIME(YEARS) : 0.00000E+00

0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
0.00000000	100.00000000	100.00000000	100.00000000	100.00000000	100.00000000	100.00000000	100.00000000	0.00000000
0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
0.00000000	75.00000000	75.00000000	75.00000000	75.00000000	75.00000000	75.00000000	75.00000000	0.00000000
0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000

ITERATION PARAMETERS

9.823E-01	9.823E-01	9.815E-01	9.816E-01	8.870E-01	8.870E-01	8.253E-01	8.253E-01	0.000E+00	0.000E+00
0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

CONCENTRATION

NUMBER OF TIME STEPS : 0
TIME(SECONDS) : 0.00000E+00
CHEM.TIME(SECONDS) : 0.00000E+00
CHEM.TIME(DAYS) : 0.00000E+00
TIME(YEARS) : 0.00000E+00
CHEM.TIME(YEARS) : 0.00000E+00
NO. MOVES COMPLETED : 0

0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

CONCENTRATION

NUMBER OF TIME STEPS : 0

0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0

N : 1
NUMBER OF ITERATIONS : 5

HEAD DISTRIBUTION - ROW

NUMBER OF TIME STEPS : 1
TIME(SECONDS) : 7.90000E+06
TIME(DAYS) : 9.14352E+01
TIME(YEARS) : 2.50336E-01

0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	89.8999993	89.9999993	89.9999993	89.9999993	89.9999993	89.9999993	89.9999994	89.9999994	0.0000000
0.0000000	94.9999993	94.9999993	94.9999993	94.9999993	94.9999993	94.9999993	94.9999994	94.9999994	0.0000000
0.0000000	89.9999993	89.9999993	89.9999993	89.9999993	89.9999993	89.9999993	89.9999994	89.9999994	0.0000000
0.0000000	85.9999993	85.9999993	85.9999993	85.9999993	85.9999993	85.9999993	85.9999994	85.9999994	0.0000000
0.0000000	81.9999993	81.9999993	81.9999993	81.9999993	81.9999993	81.9999993	81.9999994	81.9999994	0.0000000
0.0000000	77.9999993	77.9999993	77.9999993	77.9999993	77.9999993	77.9999993	77.9999994	77.9999994	0.0000000
0.0000000	73.9999993	73.9999993	73.9999993	73.9999993	73.9999993	73.9999993	73.9999994	73.9999994	0.0000000
0.0000000	69.9999993	69.9999993	69.9999993	69.9999993	69.9999993	69.9999993	69.9999994	69.9999994	0.0000000
0.0000000	65.9999993	65.9999993	65.9999993	65.9999993	65.9999993	65.9999993	65.9999994	65.9999994	0.0000000

HEAD DISTRIBUTION - ROW
 NUMBER OF TIME STEPS : 1
 TIME(SECONDS) : 7.90000E+06
 TIME(DAYS) : 9.14382E+01
 TIME(YEARS) : 2.50338E-01

0	0	0	0	0	0	0	0	0
0	100	100	100	100	100	100	100	0
0	88	88	88	88	88	88	88	0
0	90	90	90	90	90	90	90	0
0	88	88	88	88	88	88	88	0
0	81	81	81	81	82	82	82	0
0	78	78	78	78	79	79	79	0
0	78	78	78	78	77	77	77	0
0	78	78	78	78	78	78	78	0
0	0	0	0	0	0	0	0	0

DRAWDOWN

0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	-84	-84	-84	-84	-84	-84	-84	0
0	-88	-88	-88	-88	-88	-88	-88	0
0	-84	-84	-84	-84	-85	-85	-85	0
0	-80	-80	-80	-80	-81	-81	-81	0
0	-77	-77	-74	-77	-78	-78	-78	0
0	-78	-78	-74	-78	-78	-78	-78	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0

CUMULATIVE MASS BALANCE -- (IN FT**3)

RECHARGE : 0.00000E+00
 INJECTION : 0.00000E+00
 PUMPAGE : 7.90000E+06
 CUMULATIVE NET PUMPAGE : 7.90000E+06
 WATER RELEASE FROM STORAGE : -1.42380E+07
 LEAKAGE INTO AQUIFER : -2.84414E+07
 LEAKAGE OUT OF AQUIFER : 7.20111E+06
 CUMULATIVE NET LEAKAGE : -2.22403E+07
 MASS BALANCE RESIDUAL : 1.28800E+03
 ERROR (AS PERCENT) : 8.58178E-03

RATE MASS BALANCE -- (IN C.F.S.)

RECHARGE : 0.00000E+00
 LEAKAGE INTO AQUIFER : 3.72877E+00
 LEAKAGE OUT OF AQUIFER : -9.11833E-01
 NET LEAKAGE (QNET) : 2.81823E+00
 INJECTION : 0.00000E+00
 PUMPAGE : 1.00000E+00
 NET WITHDRAWAL (TPUM) : 1.00000E+00

CONCENTRATION

NUMBER OF TIME STEPS : 1
 DELTA T : 7.90000E+06
 TIME(SECONDS) : 7.90000E+06
 CHEM. TIME(SECONDS) : 7.90000E+06
 CHEM. TIME(DAYS) : 9.14382E+01
 CHEM. TIME(YEARS) : 2.50338E-01
 NO. MOVES COMPLETED : 2

0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.3207	88.7791	88.8828	88.8817	0.3078	0.0000	0.0000
0.0000	0.0000	0.2208	31.7841	31.8823	24.7013	0.1578	0.0000	0.0000
0.0000	0.0000	-0.0000	0.7088	0.8842	0.8082	-0.0037	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

CONCENTRATION

NUMBER OF TIME STEPS = 1

0	0	0	0	0	0	0	0	0
0	0	0	87	87	86	0	0	0
0	0	0	32	32	26	0	0	0
0	0	0	1	1	1	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0

CHEMICAL MASS BALANCE

MASS IN BOUNDARIES = 1.25808E+09
 MASS OUT BOUNDARIES = 0.00000E+00
 MASS PUMPED IN = 0.00000E+00
 MASS PUMPED OUT = 0.00000E+00
 INFLOW MINUS OUTFLOW = 1.25808E+09
 INITIAL MASS STORED = 0.00000E+00
 PRESENT MASS STORED = 1.41025E+09
 CHANGE MASS STORED = 1.41025E+09
 COMPARE RESIDUAL WITH NET FLUX AND MASS ACCUMULATION:
 MASS BALANCE RESIDUAL = -1.44182E+08
 ERROR (AS PERCENT) = -1.13670E+01

N = 10
NUMBER OF ITERATIONS = 1

HEAD DISTRIBUTION - ROW

NUMBER OF TIME STEPS = 10
 TIME(SECONDS) = 7.45940E+07
 TIME(DAYS) = 9.13125E+02
 TIME(YEARS) = 2.50000E+00

0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	88.9999995	88.9999995	88.9999995	88.9999995	88.9999995	88.9999995	88.9999995	88.9999995
0.0000000	85.9387927	85.9347080	85.9486781	85.9558858	85.9611524	85.1171439	85.1482955	0.0000000
0.0000000	81.8818727	81.8531537	81.8589210	81.8755133	82.1315802	82.2691261	82.3277433	0.0000000
0.0000000	87.8830717	87.7393191	87.8621388	87.8178663	88.2306270	88.4600448	88.5758063	0.0000000
0.0000000	83.9382272	83.5988993	83.0948932	83.8124888	84.4128187	84.7747183	84.9398306	0.0000000
0.0000000	80.3827136	79.6233888	77.3180916	78.8248072	80.8338389	81.2883809	81.4882872	0.0000000
0.0000000	77.8285238	77.2188578	78.7175182	77.3381158	77.8101386	78.0889025	78.1790900	0.0000000
0.0000000	75.0000003	75.0000003	75.0000002	75.0000003	75.0000003	75.0000004	75.0000004	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000

HEAD DISTRIBUTION - ROW

NUMBER OF TIME STEPS = 10
 TIME(SECONDS) = 7.45940E+07
 TIME(DAYS) = 9.13125E+02
 TIME(YEARS) = 2.50000E+00

0	0	0	0	0	0	0	0	0
0	100	100	100	100	100	100	100	0
0	96	86	88	88	86	95	95	0
0	92	92	92	92	92	92	92	0
0	88	88	88	88	88	88	88	0
0	84	84	83	84	84	85	85	0
0	80	80	77	80	81	81	81	0
0	78	77	77	77	76	76	76	0
0	75	75	75	75	75	75	75	0
0	0	0	0	0	0	0	0	0

DRAWDOWN

0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	-95	-85	-85	-85	-85	-85	-85	-85
0	-91	-81	-81	-81	-81	-81	-81	-81
0	-87	-87	-87	-87	-87	-87	-87	-87
0	-83	-83	-82	-83	-83	-84	-84	-84
0	-79	-79	-78	-79	-80	-80	-80	-80
0	-77	-75	-75	-75	-77	-77	-77	-77
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0

CUMULATIVE MASS BALANCE -- (IN FT**3)

RECHARGE	=	0.00000E+00
INJECTION	=	0.00000E+00
PUMPAGE	=	7.88840E+07
CUMULATIVE NET PUMPAGE	=	7.88840E+07
WATER RELEASE FROM STORAGE	=	-1.46812E+07
LEAKAGE INTO AQUIFER	=	-2.27383E+08
LEAKAGE OUT OF AQUIFER	=	1.33788E+08
CUMULATIVE NET LEAKAGE	=	-9.35883E+07

MASS BALANCE RESIDUAL	=	1.30240E+04
ERROR (AS PERCENT)	=	5.12320E-03

RATE MASS BALANCE -- (IN C.F.S.)

RECHARGE	=	0.00000E+00
LEAKAGE INTO AQUIFER	=	2.78871E+00
LEAKAGE OUT OF AQUIFER	=	-1.78871E+00
NET LEAKAGE (ONET)	=	8.88888E-01
INJECTION	=	0.00000E+00
PUMPAGE	=	1.00000E+00
NET WITHDRAWAL (TPUM)	=	1.00000E+00

CONCENTRATION

NUMBER OF TIME STEPS	=	10
DELTA T	=	7.78400E+06
TIME(SECONDS)	=	7.88840E+07
CHEM. TIME(SECONDS)	=	7.88840E+07
CHEM. TIME(DAYS)	=	9.13128E+02
TIME(YEARS)	=	2.50000E+00
CHEM. TIME(YEARS)	=	2.50000E+00
NO. MOVES COMPLETED	=	2

0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0338	1.7405	86.1823	98.8874	88.2215	1.7882	0.0341	0.0000
0.0000	0.1000	3.8902	86.0981	99.8332	96.8284	3.3182	0.0902	0.0000
0.0000	0.2534	6.3141	83.0406	98.9330	93.4149	6.4627	0.2830	0.0000
0.0000	0.4882	8.9286	88.1229	98.8711	88.8627	8.8421	0.5082	0.0000
0.0000	0.7073	10.7781	83.2844	90.4337	88.7808	9.8289	0.8730	0.0000
0.0000	0.7472	8.0419	86.2821	74.8078	40.4178	8.3884	0.8589	0.0000
0.0000	0.4182	3.3815	28.9020	41.8722	22.8643	4.8626	0.3821	0.0000
0.0000	0.0848	0.2858	1.8877	6.8878	6.5283	0.7113	0.0785	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

CONCENTRATION

NUMBER OF TIME STEPS = 10

0	0	0	0	0	0	0	0	0
0	0	2	88	100	98	2	0	0
0	0	4	86	100	97	3	0	0
0	0	6	83	99	93	6	0	0
0	0	8	88	97	89	8	1	0
0	1	11	83	80	70	10	1	0
0	1	8	86	78	40	8	1	0
0	0	3	27	42	23	5	0	0
0	0	0	2	7	7	1	0	0
0	0	0	0	0	0	0	0	0

CHEMICAL MASS BALANCE

MASS IN BOUNDARIES = 8.78987E+08
 MASS OUT BOUNDARIES = -3.08348E+07
 MASS PUMPED IN = 0.00000E+00
 MASS PUMPED OUT = -1.34451E+08
 INFLOW MINUS OUTFLOW = 8.41482E+08
 INITIAL MASS STORED = 0.00000E+00
 PRESENT MASS STORED = 8.58800E+09
 CHANGE MASS STORED = 8.58800E+09
 COMPARE RESIDUAL WITH NET FLUX AND MASS ACCUMULATION:
 MASS BALANCE RESIDUAL = -1.52178E+08
 ERROR [AS PERCENT] = -1.86488E+00

TEST PROBLEM 2 FOR TRANSIENT SIMULATION WITH SIP OPTION

TIME VERSUS HEAD AND CONCENTRATION AT SELECTED OBSERVATION POINTS

PUMPING PERIOD NO. 1

TRANSIENT SOLUTION

OBS.WELL NO.	X	Y	N	HEAD (FT)	CONC. (MG/L)	TIME (YEARS)
1	5	4				
0				0.0	0.0	0.000
1				88.8	0.7	0.250
2				81.8	3.2	0.501
3				82.0	40.4	0.751
4				82.0	70.7	1.001
5				82.0	81.2	1.252
6				82.0	91.1	1.502
7				82.0	96.8	1.752
8				82.0	98.8	2.003
9				82.0	98.1	2.253
10				82.0	98.8	2.500
OBS.WELL NO.	X	Y	N	HEAD (FT)	CONC. (MG/L)	TIME (YEARS)
2	5	7				
0				0.0	0.0	0.000
1				77.7	0.0	0.250
2				78.8	0.0	0.501
3				78.8	0.0	0.751
4				78.8	0.3	1.001
5				78.8	2.0	1.252
6				78.8	7.7	1.502
7				78.8	23.8	1.752
8				78.8	43.9	2.003
9				78.8	64.7	2.253
10				78.8	74.8	2.500

APPENDIX VIII

INPUT AND SELECTED OUTPUT FOR TEST PROBLEM 3

**** TSD FOREGROUND HARDCOPY ****
DSNAME=U11236D.EXNRC.CNTL

//M11236D JOB (? ,TSO-TR-KONI),KONIKOWRUN,
// TIME=(0,40),CLASS=A,
// MSGCLASS=X,NOTIFY=*
/*PASSWORD ????
/*JOBPARM ROOM=L

//*
//KONI EXEC PGM=KONI60G,REGION=1500K
//STEPLIB DD DISP=SHR,DSN=U11236C.KONI.LOAD
//FTO6FOO1 DD DSN=U11236C.EXNRC.OUTLIST,UNIT=STORAGE,
// SPACE=(TRK,(10,10)),DISP=(MOD,CATLG),
// DCB=(RECFM=VBA,LRECL=133,BLKSIZE=7448)
//FT10FOO1 DD DSN=U11236C.EXNRC.GRAPH,UNIT=STORAGE,
// SPACE=(TRK,(10,10)),DISP=(MOD,CATLG),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=7440)
//FTO7FOO1 DD SYSOUT=B
//FTO5FOO1 DD *

TEST PROBLEM 3 FOR TRANSIENT SIMULATION WITH SIP OPTION

10	1	20	33200	2	10	2	100	2	9	1	10	1	0	0	0
4.	0.01	0.1	100.	.0005	113.E6	30.	30.	.3	.2	1					
1	1		33.		2.404		10.								
1	0	0	0	0											
4	2														
6	2														
3	2	-.0075	500.												
17	2	0.0075	0.0												
1		1													
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1		1													
0.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
0.0	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50	.00
0.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
1		1													
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	14.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0		.00													
1		1													
00000000000000000000															
0100000000000000000010															
00000000000000000000															
1		0.3		.00			0.0								
0		0													

U.S.G.S. METHOD-OF-CHARACTERISTICS MODEL FOR SOLUTE TRANSPORT IN GROUND WATER

TEST PROBLEM 3 FOR TRANSIENT SIMULATION WITH SIP OPTION

INPUT DATA

GRID DESCRIPTORS

NX (NUMBER OF COLUMNS) = 20
 NY (NUMBER OF ROWS) = 3
 XDEL (X-DISTANCE IN FEET) = 30.0
 YDEL (Y-DISTANCE IN FEET) = 30.0

TIME PARAMETERS

NTIM (MAX. NO. OF TIME STEPS) = 10
 NPMP (NO. OF PUMPING PERIODS) = 1
 PINT (PUMPING PERIOD IN YEARS) = 4.000
 TIMX (TIME INCREMENT MULTIPLIER) = 1.00
 TINT (INITIAL TIME STEP IN SEC.) = 0.12E+08

HYDROLOGIC AND CHEMICAL PARAMETERS

S (STORAGE COEFFICIENT) = 0.000500
 POROS (EFFECTIVE POROSITY) = 0.10
 SETS (CHARACTERISTIC LENGTH) = 100.0
 OLTRAT (RATIO OF TRANSVERSE TO LONGITUDINAL DISPERSIVITY) = 0.30
 ANPCTR (RATIO OF T-VY TO T-XX) = 1.000000

SPECIES HALF LIFE (YEARS) = 3.300E+01 OR DECAY CONSTANT (1/SECS) = 6.666E-10

ROCK DENSITY (GRM/CM**3) = 2.404E+00 BULK DENSITY/POROSITY = 2.184E+01

LINEAR SORPTION DISTRIBUTION CONSTANT (KD) = 1.000E+01

SIP USED

CONFINED AQUIFER

EXECUTION PARAMETERS

NITP (NO. OF ITERATION PARAMETERS) = 10
 TOL (CONVERGENCE CRITERIA - ADIP) = 0.0100
 ITMAX (MAX. NO. OF ITERATIONS - ADIP) = 100
 CELDIS (MAX. CELL DISTANCE PER MOVE OF PARTICLES - N.C.C.) = 0.200
 NPMPX (MAX. NO. OF PARTICLES) = 3200
 NPMPND (NO. PARTICLES PER NODE) = 8

PROGRAM OPTIONS

NPNT (TIME STEP INTERVAL FOR COMPLETE PRINTOUT) = 2
 NPNTMV (MOVE INTERVAL FOR CHEM. CONCENTRATION PRINTOUT) = 10
 NPNTVL (PRINT OPTION-VELOCITY) = 1
 0=NO; 1=FIRST TIME STEP; 2=ALL TIME STEPS
 NPNTD (PRINT OPTION-DISP. COEF.) = 1
 0=NO; 1=FIRST TIME STEP; 2=ALL TIME STEPS
 NUMOBS (NO. OF OBSERVATION WELLS) = 0
 NRECF (FOR HYDROGRAPH PRINTOUT) = 2
 NRCDE (NO. OF PUMPING WELLS) = 2
 NRCDEE (FOR NODE IDENT.) = 1
 NPNCVY (PUNCH VELOCITIES) = 0
 NPDEL (PRINT OPT.-CONC. CHANGE) = 0

TIME INTERVALS (IN SECONDS)

0.12000E+08 0.13000E+08 0.13000E+08 0.13000E+08 0.13000E+08 0.13000E+08 0.13000E+08 0.13000E+08 0.13000E+08 0.13000E+08
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00

LOCATION OF OBSERVATION WELLS

NO.	X	Y
1	4	2
2	8	2

LOCATION OF PUMPING WELLS

X	Y	RATE (IN CFS)	EDNC.
3	2	-0.750E-02	500.00
17	2	0.750E-02	0.00

AREA OF ONE CELL = 9.0000E+02

N-Y SPACING:
 30.000
 30.000

AQUIFER THICKNESS (FT)
 0.0
 0.0
 0.0

WATER TABLE
 0.
 0. 14. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 10. 0.
 0.

TRANSMISSIVITY MAP (FT*FT/SEC)
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02
 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02 3.00E-02
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00

PERMEABILITY MAP (FT/SEC)
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04
 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04 8.00E-04
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00

NO. OF FINITE-DIFFERENCE CELLS IN AQUIFER = 18
 AREA OF AQUIFER IN MODEL = 1.82000E+04 SQ. FT.

NZCRIT (MAX. NO. OF CELLS THAT CAN BE VOID OF PARTICLES; IF EXCEEDED, PARTICLES ARE REGENERATED) = 0

DIFFUSE RECHARGE AND DISCHARGE (FT/SEC)
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00

NODE IDENTIFICATION MAP

0
 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0
 0

NO. OF NODE IDENT. CODES SPECIFIED = 1

THE FOLLOWING ASSIGNMENTS HAVE BEEN MADE:
 CODE NO. LEAKANCE SOURCE CONC. RECHARGE
 1 3.000E-01 0.000E+00

VERTICAL PERMEABILITY/THICKNESS (FT/(FT*SEC))
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 3.00E-01 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 3.00E-01 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00
 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00

HEAD DISTRIBUTION - ROW

NUMBER OF TIME STEPS : 0
TIME(SECONDS) : 0.00000E+00
TIME(DAYS) : 0.00000E+00
TIME(YEARS) : 0.00000E+00

0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	14.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	10.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000

ITERATION PARAMETERS

8.328E-01 8.328E-01 8.780E-01 8.780E-01 8.215E-01 8.215E-01 7.188E-01 7.188E-01 0.000E+00 0.000E+00
0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

CONCENTRATION

NUMBER OF TIME STEPS : 0
TIME(SECONDS) : 0.00000E+00
CHEM.TIME(SECONDS) : 0.00000E+00
CHEM.TIME(DAYS) : 0.00000E+00
TIME(YEARS) : 0.00000E+00
CHEM.TIME(YEARS) : 0.00000E+00
NO. MOVES COMPLETED : 0

0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

CONCENTRATION

NUMBER OF TIME STEPS : 0

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

N : 2
NUMBER OF ITERATIONS : 1

HEAD DISTRIBUTION - ROW

NUMBER OF TIME STEPS : 2
TIME(SECONDS) : 2.00000E+07
TIME(DAYS) : 3.00828E+02
TIME(YEARS) : 8.23890E-01

0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	13.8888887	13.8708883	12.8811740	12.4117628	13.1323812	12.8828388	12.8738288	12.2841171	12.0147087	0.0000000
11.7382843	11.4888888	11.1784718	10.8870802	10.8178488	10.3382374	10.0888288	10.0284148	10.0000033	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000

HEAD DISTRIBUTION - ROW

NUMBER OF TIME STEPS : 2
 TIME(SECONDS) : 2.80000E+07
 TIME(DAYS) : 3.00826E+02
 TIME(YEARS) : 8.23880E-01

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	14	14	14	13	12	12	12	12	11	11	11	11	10	10	10	10	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

DRAWDOWN

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	-13	-13	-12	-12	-12	-12	-11	-11	-11	-10	-10	-10	-8	-8	-8	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CUMULATIVE MASS BALANCE -- (IN FT**3)

RECHARGE : 0.00000E+00
 INJECTION : -1.95000E+05
 PUMPAGE : 1.95000E+05
 CUMULATIVE NET PUMPAGE : 0.00000E+00
 WATER RELEASE FROM STORAGE : -8.58124E+01
 LEAKAGE INTO AQUIFER : -2.29851E+04
 LEAKAGE OUT OF AQUIFER : 2.29005E+04
 CUMULATIVE NET LEAKAGE : -8.8084E+01
 MASS BALANCE RESIDUAL : 0.00000E+00
 ERROR (AS PERCENT) : 0.00000E+00

RATE MASS BALANCE -- (IN C.F.S.)

RECHARGE : 0.00000E+00
 LEAKAGE INTO AQUIFER : 8.82341E-04
 LEAKAGE OUT OF AQUIFER : -8.82341E-04
 NET LEAKAGE (ONET) : 0.00000E+00
 INJECTION : -7.50000E-03
 PUMPAGE : 7.50000E-03
 NET WITHDRAWAL (TPUM) : 0.00000E+00

CONCENTRATION

NUMBER OF TIME STEPS : 2
 DELTA T : 1.30000E+07
 TIME(SECONDS) : 2.80000E+07
 CHEM.TIME(SECONDS) : 2.59988E+07
 CHEM.TIME(DAYS) : 3.00823E+02
 TIME(YEARS) : 8.23880E-01
 CHEM.TIME(YEARS) : 8.23884E-01
 NO. MOVES COMPLETED : 22

0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	2.5077	59.0890	31.0170	9.0285	1.8241	0.2818	0.0351	0.0037	0.0003	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

CONCENTRATION

NUMBER OF TIME STEPS : 2

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	3	59	31	9	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CHEMICAL MASS BALANCE

MASS IN BOUNDARIES : 0.00000E+00
 MASS OUT BOUNDARIES : -3.88375E-15
 MASS PUMPED IN : 8.74888E+07
 MASS PUMPED OUT : -3.48514E+08
 INFLOW MINUS OUTFLOW : 8.74888E+07
 INITIAL MASS STORED : 0.00000E+00
 PRESENT MASS STORED : 5.13437E+05
 CHANGE MASS STORED : 5.13437E+05
 DECAY OF SOLUTE MASS : -4.03855E+03
 ADSORPTION STORAGE (S) : 1.11085E+08
 ADSORPTION DECAY (S) : -8.73775E+05
 COMPARE RESIDUAL WITH NET FLUX AND MASS ACCUMULATION:
 MASS BALANCE RESIDUAL : -1.49787E+07
 ERROR (AS PERCENT) : -1.53608E+01

N = 10
 NUMBER OF ITERATIONS = 1

HEAD DISTRIBUTION - ROW
 NUMBER OF TIME STEPS = 10
 TIME(SECONDS) = 1.28230E+08
 TIME(DAYS) = 1.48100E+03
 TIME(YEARS) = 4.00000E+00

0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	13.8888887	13.8705254	13.8511740	13.4117628	13.1223512	12.8528398	12.5735285	12.2841171	12.0147057
11.7152043	11.4858828	11.1784718	10.8970802	10.5178488	10.3382374	10.0588250	10.0284148	10.0000033	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000

HEAD DISTRIBUTION - ROW
 NUMBER OF TIME STEPS = 10
 TIME(SECONDS) = 1.28230E+08
 TIME(DAYS) = 1.48100E+03
 TIME(YEARS) = 4.00000E+00

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	14	14	13	13	13	12	12	12	11	11	11	11	10	10	10	10	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

DRAWDOWN

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	-13	-13	-12	-12	-12	-12	-11	-11	-11	-11	-10	-10	-10	-9	-9	-9	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CUMULATIVE MASS BALANCE -- (IN FT³)

RECHARGE = 0.00000E+00
 INJECTION = -8.48727E+05
 PUMPAGE = 8.48727E+05
 CUMULATIVE NET PUMPAGE = 0.00000E+00
 WATER RELEASE FROM STORAGE = -8.35124E+01
 LEAKAGE INTO AQUIFER = -1.11423E+05
 LEAKAGE OUT OF AQUIFER = 1.11338E+05
 CUMULATIVE NET LEAKAGE = -8.58828E+01

MASS BALANCE RESIDUAL = 0.00000E+00
 ERROR (AS PERCENT) = 0.00000E+00

RATE MASS BALANCE -- (IN C.F.S.)

RECHARGE = 0.00000E+00
 LEAKAGE INTO AQUIFER = 8.82341E-04
 LEAKAGE OUT OF AQUIFER = -8.82341E-04
 NET LEAKAGE (QNET) = 0.00000E+00
 INJECTION = -7.50000E-03
 PUMPAGE = 7.50000E-03
 NET WITHDRAWAL (TPUM) = 0.00000E+00

CONCENTRATION

NUMBER OF TIME STEPS = 10
 DELTA T = 8.23040E+08
 TIME(SECONDS) = 1.28230E+08
 CHEM. TIME(DAYS) = 1.28230E+08
 CHEM. TIME(YEARS) = 1.48100E+03
 CHEM. TIME(YEARS) = 4.00000E+00
 NO. MOVES COMPLETED = 16

0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	34.1468	171.5018	119.3772	88.8855	38.2258	21.1563	10.4521	4.5588	1.8014	0.0000
0.7118	0.2484	0.0781	0.0238	0.0088	0.0017	0.0008	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

CONCENTRATION

NUMBER OF TIME STEPS = 10

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	34	172	118	70	39	21	10	5	2	1	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CHEMICAL MASS BALANCE

MASS IN BOUNDARIES = 0.00000E+00
 MASS OUT BOUNDARIES = -3.48473E-03
 MASS PUMPED IN = 4.73243E+08
 MASS PUMPED OUT = -4.42187E+01
 INFLOW MINUS OUTFLOW = 4.73243E+08
 INITIAL MASS STORED = 0.00000E+00
 PRESENT MASS STORED = 2.12887E+08
 CHANGE MASS STORED = 2.12887E+08
 DECAY OF SOLUTE MASS = -8.37876E+04
 SORPTION STORAGE (S) = 4.80481E+08
 SORPTION DECAY (S) = -2.02826E+07
 COMPARE RESIDUAL WITH NET FLUX AND MASS ACCUMULATION:
 MASS BALANCE RESIDUAL = -8.63429E+06
 ERROR (AS PERCENT) = -2.03637E+00

TEST PROBLEM 3 FOR TRANSIENT SIMULATION WITH SIP OPTION

TIME VERSUS HEAD AND CONCENTRATION AT SELECTED OBSERVATION POINTS

PUMPING PERIOD NO. 1

TRANSIENT SOLUTION

OBS.WELL NO.	X	Y	N	HEAD (FT)	CONC. (MG/L)	TIME (YEARS)
1	4	2				
			0	0.0	0.0	0.000
			1	13.7	6.2	0.412
			2	13.7	31.0	0.824
			3	13.7	54.1	1.236
			4	13.7	87.0	1.648
			5	13.7	119.1	2.060
			6	13.7	151.1	2.472
			7	13.7	183.8	2.884
			8	13.7	216.1	3.296
			9	13.7	248.9	3.708
			10	13.7	281.4	4.000
2	6	2				
			0	0.0	0.0	0.000
			1	13.1	0.1	0.412
			2	13.1	1.6	0.824
			3	13.1	4.1	1.236
			4	13.1	7.4	1.648
			5	13.1	12.9	2.060
			6	13.1	17.3	2.472
			7	13.1	21.8	2.884
			8	13.1	26.8	3.296
			9	13.1	31.4	3.708
			10	13.1	36.2	4.000